PROPERTIES OF GRAPHENE NANORIBBONS
OBTAINED BY CHEMICAL VAPOR DEPOSITION

BY

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THESIS
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ABSTRACT

We use chemical vapor deposition (CVD) to synthesize graphene films on copper foil. After transferring the graphene to SiO$_2$/Si substrates, we pattern the film into graphene nanoribbons (GNRs) of width $< \sim 50$ nm and length $< \sim 700$ nm with Ti/Au contacts. We perform low-bias, high-bias, and temperature-dependent electrical measurements. CVD-grown GNRs have mobility values from 100 to 500 cm$^2$V$^{-1}$s$^{-1}$ and current densities up to $\sim$3 mA/µm, suggesting that polycrystalline graphene grain boundaries play a limited role in the CVD-GNR electrical properties. CVD-GNR Raman spectra are comparable to lithographically patterned GNRs from exfoliated graphene. We fit our experimental data using a self-consistent model that includes GNR fringing capacitance and observe a weak temperature dependence of CVD-GNR mobility. We find a square root dependence of maximum current density on GNR resistance, implying that breakdown is primarily due to Joule heating. The electrical characteristics of CVD-GNRs illustrate the promise of wafer-scale graphene integration while revealing variability, contacts, and impurities as future challenges for improving performance.
To my wife Emily for her love and support
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CHAPTER 1
INTRODUCTION

1.1 Introduction to Graphene

Silicon transistors have been the fundamental building blocks of the semiconductor industry for several decades. Improvements in fabrication techniques and technologies allowed device designers to iteratively shrink silicon transistor dimensions, resulting in faster and cheaper electronics. In turn, these powerful and cheap transistors spawned a spectrum of silicon-based electronics, enabling technical, economic, and social improvements. However, silicon transistor scaling trends are approaching the physical limits of silicon. With the future of the semiconductor industry in limbo, forward-thinking researchers in industry and academia have been searching for new materials with better electronic properties to supplement or replace silicon. Graphene is one such material.

Graphene, a two-dimensional sheet of hexagonally arranged carbon atoms, was first isolated and electrically measured in 2004 by scientists at the University of Manchester. Realizing that graphite is simply stacked layers of graphene, the scientists (now Nobel laureates) devised a method dubbed “mechanical exfoliation” to obtain single layer graphene. In general, mechanical exfoliation uses a type of adhesive tape (e.g. Scotch™ tape) to peel away layers of graphite with the hope that enough peeling will thin some of the graphite down to only a few layers. The graphite flakes are then transferred to a substrate; in our lab we simply press the Scotch tape against a substrate and then slowly peel it off, leaving some of the graphite behind. After transferring the graphite to a substrate, one must undertake the monumental task of finding single layer graphene (Fig. 1.1(a)) (placed at end of chapter) in the midst of a graphite mess (Fig. 1.1(b)). Monolayer graphene is only one atom thick, yet it produces a slight change in optical contrast if
the underlying substrate is a particular thickness. Therefore, with the right substrate, a good microscope, and patience, one can find single layers graphene up to ~50 μm in size.

After graphene was successfully isolated, its electrical properties were explored. Experiments revealed an ambipolar electric field effect in graphene (Fig 1.2(a)), which means that conduction can occur via electrons, holes, or a combination of both (Fig 1.2(b)). Charge carrier concentrations as high as $10^{13}$ cm$^{-2}$ with mobility values $\mu > 15,000$ cm$^2$ V$^{-1}$ s$^{-1}$ were reported. Because mobility is a measure of how quickly charge carriers can move through a material, the high mobility of graphene is desirable for high-frequency applications. High-speed graphene transistors were fabricated and intrinsic cutoff frequencies over 100 GHz were demonstrated. In addition to desirable electronic properties, the atomically thin planar structure of graphene is suitable for modern integrated circuit manufacturing processes. A thin MOSFET channel suppresses short-channel effects in semiconducting transistors. Graphene promises manufacturable transistor technology that can be scaled to the ultimate thickness limit (single atom) while operating at very high frequencies and large current densities.

Though it has many desirable properties for electronic applications, graphene also has some important shortcomings. First and foremost, graphene lacks an energy band gap, which is necessary for the operation of low-power, high-fidelity digital circuits with large $I_{\text{ON}}/I_{\text{OFF}}$ ratios > $10^4$ at (and above) room temperature. Without a band gap, the on/off ratio of graphene is only modulated by the density of states and is typically only $10 \sim 100$. In digital applications with billions of transistors, leaky graphene devices would consume a prohibitive amount of power. Secondly, fabricated devices behave differently than ideal graphene; many devices have asymmetric conduction, varying minimum conductivity (Dirac) voltages $V_0$, and hysteretic curves (Fig 1.3). Therefore, an open research problem is to fabricate graphene transistors with repeatable charac-
teristics, a Dirac voltage $V_0 = 0$ Volts, and a high $I_{ON}/I_{OFF}$ ratio. Regardless of its shortcomings, the discovery of such a promising electronic material has had an enormous impact on the direction of semiconductor research.\(^4\)

1.2 Graphene Nanoribbon Field-Effect Transistors

Initial graphene experiments were on micrometer-sized graphene. However, state-of-the-art silicon field-effect transistors (FETs) for digital applications have minimum feature sizes on the order of tens of nanometers.\(^1\) Therefore, a reasonable question is whether nanometer graphene will have the same excellent electrical properties as micrometer graphene. To answer this, researchers began studying the properties of graphene strips with widths less than 100 nm. Such small structures are called graphene nanoribbons (GNRs). Early theoretical studies determined that GNRs with zigzag edges (Fig. 1.4(a)) behave as metallic conductors, while GNRs with armchair edges (Fig 1.4(b)) are semiconductors.\(^11\) Another theoretical study revealed an inverse relationship between armchair GNR width and band gap magnitude.\(^12\) In 2007, a team from Columbia University experimentally confirmed this inverse relationship by lithographically patterning GNRs and measuring their conductance at low temperatures (Fig 1.5).\(^13\) We note that such experimental GNR edges have a combination of zigzag and armchair segments, most likely terminated by H or O atoms.\(^14\) Further experimental studies used alternative methods\(^15-17\) to create narrow ($<$10 nm) GNRs with finite transport or energy band gaps and room temperature $I_{ON}/I_{OFF}$ ratios up to $10^7$.

While these experiments demonstrate that it is possible to engineer a band gap for GNRs, several challenges still remain. The Columbia study used mechanical exfoliation to obtain graphene, which is not a scalable fabrication technique. Alternative fabrication methods suffer from
low yield, result in a random distribution of GNR sizes, and are unable to precisely position the GNRs.\textsuperscript{15-17} All GNRs suffer from edge scattering and therefore have mobility values much lower than micron-scale graphene,\textsuperscript{18} sometimes even lower than silicon. Because experimental data reveal gaps much larger than theoretical predictions, it has been suggested that the observed transport gap is actually dominated by localized states from edge roughness and disorder.\textsuperscript{19} Future work is needed to understand the cause of the transport gap. Nevertheless, it is clear that energy gaps appear in graphene nanoribbons and provide the band gap necessary for GNRs to be a viable material for digital FETs.

### 1.3 Graphene Nanoribbon Interconnects

As silicon FET dimensions are shrinking, so are the conductive wires used to connect FET terminals.\textsuperscript{20} These interconnects need to have low resistivity, high current capability, resistance to electromigration, high mobility, and the ability to be defined using conventional fabrication methods.\textsuperscript{21} Mechanically exfoliated GNRs have been shown to have resistivity comparable to copper interconnects,\textsuperscript{22} breakdown current density $>10^8$ A/cm$^2$,\textsuperscript{22} immunity to electromigration,\textsuperscript{23} and can be defined using standard lithography and etching techniques.\textsuperscript{22} In addition, with a thermal conductivity comparable to or higher than that of copper,\textsuperscript{24} GNR interconnects could double as heat dissipaters to combat the growing interconnect Joule heating problem.\textsuperscript{20} These desirable properties have generated interest in using GNRs as interconnects in hybrid graphene-Si circuits\textsuperscript{25} and all graphene circuits.\textsuperscript{26}

### 1.4 Chemical Vapor Deposition of Graphene

While mechanical exfoliation is a suitable method for obtaining high-quality flakes of graphene for laboratory experiments, it is not capable of scaling for wafer-scale applications. In-
stead, large-area graphene films are needed. Graphene films were first synthesized by epitaxy,\textsuperscript{27} which produces graphene on an insulating SiC substrate. However, this method requires extremely high temperatures (over 1500 °C), ultra-low pressures, and expensive ultra-high vacuum equipment. A cheaper, lower temperature, higher pressure method of growing predominantly monolayer graphene uses chemical vapor deposition (CVD) of carbon-containing gases on a metallic substrate. A promising method of growing graphene on copper (Cu) foil was developed in 2009 by a group at the University of Texas at Austin.\textsuperscript{28}

CVD synthesis of graphene on Cu begins by loading a 25 µm thick Cu foil into a hot wall CVD furnace. Next, the foil is heated to 1000 °C under a 2 sccm H\textsubscript{2} flow at a pressure of 40 mTorr. When the system reaches 1000 °C, 35 sccm of CH\textsubscript{4} is introduced to begin the graphene growth. During this key step of the process, methane molecules crack on the hot Cu surface. Carbon atoms from the methane chemically adsorb to the Cu at nucleation sites while the hydrogen atoms from the methane float away. As the carbon atoms cluster to the nucleation sites, individual graphene domains are created (Fig. 1.6). The growth rate of each graphene domain is a function of the underlying Cu substrate crystallography.\textsuperscript{29} This surface catalyzed growth is self-limited, resulting in graphene films with over 90% monolayer coverage\textsuperscript{28} (the rest is multilayer). The synthesized graphene grows on both sides of the copper, and the dimensions are only limited by the size of foil.

CVD graphene has its share of imperfections. It contains resistive grain boundaries (GBs) at the intersection of graphene domains.\textsuperscript{30} The difference in thermal expansion between Cu and graphene creates wrinkles in the graphene film. Finally, the CVD graphene must be removed from the copper foil and transferred to a more suitable substrate for electronic applications, which requires significant handling and chemical processing. These problems are known to de-
crease the mobility of micron-scale graphene. Regardless, large-area CVD graphene has already been used by Samsung to create graphene-based touch panels and 30 inch graphene films (Fig. 1.7).³¹

Graphene films synthesized by chemical vapor deposition are very useful for future wafer-scale nanoelectronics that use GNRs as interconnects or transistors. It is well known that micron-scale exfoliated graphene has better electrical properties than CVD graphene. However, very little CVD GNR data exists today. GNRs made from CVD-grown graphene could be comparable to or smaller than the average graphene grain size, and therefore have few or no grain boundaries, few or no wrinkles, and fewer impurities than large-area CVD graphene. In this case, the electrical characteristics of CVD GNRs and exfoliated GNRs may be quite similar, enabling large-scale integration of high-quality CVD GNR transistors or interconnects.

In this thesis we present a comprehensive analysis of CVD GNRs. We perform low-bias, high-bias, and temperature-dependent measurements on GNRs with various dimensions. The mobility, current density, and Raman spectra of CVD-grown GNRs are comparable to exfoliated and chemically derived GNRs, suggesting that polycrystalline grain boundaries play a limited role in the CVD GNR electrical properties. We fit the data using a self-consistent model that includes GNR fringing capacitance. Our model reveals a weak temperature dependence of CVD GNR mobility. Square root power dependence of maximum current density on the resistance of the GNRs implies that breakdown is mainly due to Joule heating. The electrical characteristics of CVD GNRs illustrate the promise of wafer scale graphene integration while revealing variability, contacts, and impurities as future challenges for improving performance.
1.5 Figures

Figure 1.1(a) A large piece of single-layer exfoliated graphene on a 90 nm SiO$_2$/Si++ substrate. The bottom left corner is thick graphite. The slight difference in optical contrast of the atomically thin graphene makes it very difficult to find graphene flakes. This picture is taken with a 50x microscope lens. (b) A 5x image of exfoliated graphite. The arrow points to the graphite which the graphene is located near.
Figure 1.2(a) The ambipolar electric field effect in graphene. A positive (negative) gate voltage $V_G$ induces electrons (holes) in the graphene. (b) A MATLAB analysis of charge carrier density in graphene as a function of gate voltage for a graphene FET on 90 nm SiO$_2$ at room temperature. Holes are the majority carriers for $V_G-V_0 < 0$, electrons are majority carriers for $V_G-V_0 > 0$, and near $V_0$ holes and electrons are similar in density.
**Figure 1.3** $R$-$V_G$ curve in air at room temperature for an exfoliated monolayer graphene FET on SiO$_2$/Si with width $W = 14\ \mu$m, length $L = 21\ \mu$m on 90 nm SiO$_2$. The drain voltage $V_{DS} = 20$ mV. $V_G$ was swept from 0 to +20, down to -20, and back to 0 in 200 mV increments. The Dirac voltage of this device is $V_0 = 13$–16 V, with the uncertainty due to hysteresis. $I_{ON}/I_{OFF}$ of this device is ~5 and hole mobility is $\mu_p \sim 1500$ cm$^2$V$^{-1}$s$^{-1}$. Inset, borrowed from Liao,$^{32}$ is a schematic of the graphene FET.

**Figure 1.4** (a) Semiconducting GNRs have a band gap that depends on ribbon width and length,$^{12,33}$ while (b) zigzag GNRs are metallic.$^{34}$
Figure 1.5 Experimental results from a Columbia University study demonstrating the inverse relationship between band gap and GNR width.\textsuperscript{13} We observe that GNRs with widths $W > 25$ nm have band gaps smaller than the room temperature thermal excitation energy ($k_B T / q$, ~26 millielectron volt, where $k_B$ is the Boltzmann constant and $T$ is the absolute temperature).

\begin{figure}[h]
\centering
\includegraphics[width=0.5\textwidth]{figure1.5.png}
\caption{Experimental results from a Columbia University study demonstrating the inverse relationship between band gap and GNR width. We observe that GNRs with widths $W > 25$ nm have band gaps smaller than the room temperature thermal excitation energy ($k_B T / q$, ~26 millielectron volt, where $k_B$ is the Boltzmann constant and $T$ is the absolute temperature).}
\end{figure}

Figure 1.6 Scanning electron microscope (SEM) image of graphene on Cu foil after a one minute partial growth.\textsuperscript{28} The graphene domains begin at a nucleation site and fan outward as time progresses. The intersections of graphene domains are called grain boundaries.

\begin{figure}[h]
\centering
\includegraphics[width=0.5\textwidth]{figure1.6.png}
\caption{Scanning electron microscope (SEM) image of graphene on Cu foil after a one minute partial growth. The graphene domains begin at a nucleation site and fan outward as time progresses. The intersections of graphene domains are called grain boundaries.}
\end{figure}
Figure 1.7 Researchers from Samsung have demonstrated (a) a graphene-based touch screen and (b) a 30 inch graphene film.31
CHAPTER 2
EXPERIMENTAL PROCEDURES

2.1 Graphene Growth and Transfer

Our CVD graphene growth and GNR device process steps are illustrated in Fig. 2.1. We begin by loading 1 mil copper foil (~99.9% purity, Basic Copper, Carbondale, IL) into an Atome-CVD system. The foil is cut into a rectangle and wrapped around a quartz boat. We load the boat with Cu foil into a quartz tube. This tube is dedicated to growing graphene in an effort prevent cross contamination with other CVD processes. The Cu foil is kept as smooth as possible during these steps to minimize wrinkles and tears in the synthesized graphene. The temperature is ramped to 1000 °C under H₂/Ar flow and the Cu foil is kept at 1000 °C under H₂/Ar flow for one hour to increase Cu foil grain size. Graphene growth is performed by flowing 100 sccm CH₄ at 1000°C and 500 mTorr chamber pressure for 30 minutes, which results primarily in monolayer graphene growth on both sides of the Cu foil (Fig. 2.1(a)). The system was cooled at a rate of ~20 °C under H₂/Ar flow.

We remove the foil from the quartz tube and prepare the graphene for transfer from the foil to an SiO₂/Si++ substrate. The foil with graphene on it is gently cut into squares roughly the size of the substrates used (22 mm x 22 mm). One side of the foil is covered with ~250 nm thick layer of polymethyl methacrylate (PMMA) to protect the graphene, while the other side is left exposed. We remove the graphene from the exposed side of the Cu foil with a 20 sccm O₂ plasma reactive ion etch (RIE) for 10 seconds (Fig. 2.1(b)). It is worth noting that we use the graphene from the side of the foil that was in contact with the quartz boat because it tended to have better Raman spectra (smaller D peak) than graphene from the opposite side of the foil. After RIE, the remaining Cu foil/graphene/PMMA stack is placed in a beaker of aqueous FeCl₃ overnight to
etch away the Cu (Fig. 2.1(c)). After the foil is completely etched, we are left with the graphene/PMMA film floating on the surface of the FeCl$_3$. The PMMA/graphene film is transferred via a glass slide to an HCl bath to functionalize Cu particle contamination$^{35}$ and then to two separate deionized water baths to wash away the HCl (Fig. 2.1(d)). After the film is clean, it is transferred to an SiO$_2$ (90 nm ± 5 nm) on Si (N doped 5 mΩ⋅cm) substrate and left overnight to dry (Fig. 2.1(e)). The PMMA is removed by submerging the substrate in a 1:1 mixture of methylene chloride and methanol for one hour. Finally, the graphene is annealed with a one hour Ar/H$_2$ anneal at 400 °C at atmospheric pressure to remove the PMMA and other organic residue$^{36}$ (Fig. 2.1(f)). This step does not completely remove the PMMA residue (Fig. 2.2), preventing metal electrodes from completely contacting the graphene and leading to a higher contact resistance. Improving GNR contacts is a very important challenge that must still be addressed to increase GNR performance while reducing variability.

2.2 GNR Fabrication

GNR devices are fabricated by defining large Ti/Au (0.5/40 nm) probing contacts using optical lithography and electron-beam (e-beam) evaporation (Fig 2.2). An additional step of e-beam lithography and evaporation is performed to create smaller finger contacts defining the length of the devices in the nanometer regime (Fig. 2.3(a)). We use a bilayer resist (495 PMMA A2 & 950 PMMA A4 from MicroChem) to help with metal liftoff for all e-beam lithography steps. The width of the GNR is defined with a second e-beam lithography step, and after the PMMA is developed, 1 to 2 nm of Al is deposited using e-beam evaporation. The thin evaporated Al film oxidizes when the chip is removed from the low-pressure e-beam evaporation chamber.$^{37}$ PMMA liftoff leaves behind an AlO$_x$ nanoribbon covering the graphene and stretching between finger electrodes (Fig. 2.3(a)). Because liftoff of a 1-2 nm evaporated Al film can be surprisingly diffi-
cult (Fig. 2.4), one may opt to evaporate a thicker (e.g. 20 nm) metal mask for etching the CVD graphene into ribbons.\textsuperscript{38} A 10 second $O_2$ plasma RIE at 40 Watts and 40 mTorr removes all unprotected graphene and leaves a GNR under the etch mask (Fig. 2.1(g)). The etch parameters can be tuned during this step to laterally etch the protected GNR at the edges, thus achieving GNR widths smaller than the minimum resolution afforded by e-beam lithography.\textsuperscript{38} The CVD graphene under the contacts is also protected during the plasma etch, achieving a larger graphene-metal contact area and reduced contact resistance. Because the AlO$_x$ etch mask can double as a seed layer for future top gate deposition,\textsuperscript{37} we left the AlO$_x$ etch mask on some devices (batch b1) for the measurements. For comparison, we also removed the AlO$_x$ etch mask (Figure 2.3(b)) using Al etch type A (Transene Company Inc.) on a subset of the devices (batch b2) to compare the AlO$_x$ covered CVD GNRs with bare CVD GNRs.

2.3 Raman Characterization of CVD GNRs

We use a Renishaw Raman spectrometer and a 633 nm laser to determine the number of layers (2D to G intensity ratio) and quality (D peak magnitude and integrated D to G ratio) of the graphene. Figure 2.5 compares the Raman spectrum of the large-area CVD graphene to several individually patterned GNRs. The integrated D to G peak area ratio $A_D/A_G$ of the CVD GNRs is $\approx 1.5$, which is comparable to ratios of $\approx 2.8$ measured for arrays of exfoliated GNRs of similar dimensions.\textsuperscript{39} This suggests our CVD GNRs are of comparable quality to exfoliated GNRs. For comparison, our bulk CVD graphene has $A_D/A_G \approx 0.2$. The difference in $A_D/A_G$ between the bulk CVD and CVD GNR could be from a combination of the extra processing steps and the presence of edges.\textsuperscript{39,40} We note that the CVD GNR only undergoes a few processing steps more than the bulk CVD graphene does, yet the CVD GNR Raman spectra exhibits a significant increase in disorder. Also, a similar amount of disorder is observed in exfoliated GNRs. These observations
suggest that disorder in GNR Raman spectra is more likely due to GNR edges than the extra processing steps of CVD graphene.

2.4 Figures

Figure 2.1 Schematic of the CVD growth on Cu and transfer process to SiO$_2$ (90 nm)/Si substrates (a-e) and fabrication of devices (f-h). The substrate is used as the back gate in electrical measurements. A thin AlO$_x$ layer is used as an etch mask to form GNRs (h), which is later removed for some of the devices (batch b1).

Figure 2.2 Optical micrograph of a row of devices on a test chip. Micron-scale PMMA residues (light blue) are sometimes visible even after annealing. Dark purple areas are bilayer graphene. Scale bar is 300 μm.
Figure 2.3 (a) An SEM image of a $W = 75$ nm $L = 110$ nm GNR between two Ti/Au (1/40 nm) finger contacts (scale bar = 1 μm). The AlO$_x$ ribbon can be seen over the contacts. (b) AFM of a $W = 60$ nm $L = 400$ nm CVD GNR. Scale bar is 100 nm.

Figure 2.4 Optical micrograph of an unsuccessful AlO$_x$ liftoff. The optical contrast is from the ~2 nm AlO$_x$ film. Scale bar is 300 μm.
Figure 2.5 Raman spectra for bulk CVD graphene and GNR devices, indicating good quality and predominantly monolayer coverage for the bulk CVD graphene and the presence of defects and edge states for the GNR. Some GNRs have visible D' peaks, another indication of defects.
CHAPTER 3
ELECTRICAL CHARACTERIZATION OF CVD GRAPHENE NANORIBBONS

3.1 Low-Bias Measurements

We apply a low-field drain bias $V_D$ and measure the drain current $I_D$ of the CVD GNRFET as a function of the back gate voltage $V_G$. All sourced voltages and measured currents are manipulated and recorded via a Keithley 4200 Semiconductor Characterization System. $V_G$ is applied to the heavily doped Si++ back gate on the bottom of the substrate which behaves like a metal electrode. Modulation of $V_G$ shifts the Fermi level of the GNR, modulating the density of charge carriers. Measuring $I_D$ as a function of $V_G$ allows us to view the modulation of charge density and quantitatively characterize the electrical behavior of our CVD GNRs.

Measurements of both AlO$_x$ capped and bare CVD GNRs in vacuum ($\sim 10^{-5}$ Torr) at room temperature reveal $p$-doped GNRs with ohmic contacts and varying $I_{ON}/I_{OFF}$. Some devices have visible minimum conductivity voltages $V_0$, while other devices have a $V_0$ beyond our maximum “safe” back gate voltage ($\sim 40$ V) (Fig. 3.1). Annealing the GNRs at 300 °C for two hours in vacuum removes the physisorbed ambient impurities such as water$^2$ and oxygen.$^{41}$ After annealing, measurements in vacuum show the devices are less $p$-doped than in air and in some cases $n$-doped (Fig. 3.2). The data are fitted with a transport model$^{42}$ (Fig. 3.3) revealing channel mobility $\mu = 100$–500 cm$^2$V$^{-1}$s$^{-1}$ and contact resistance $R_CW \geq 500 \Omega \cdot \mu$m. The model includes thermally generated carriers, contact resistance as a function of gate voltage and temperature, puddle charge density, and the effect of fringing fields on the capacitance between the back-gate and GNR through the SiO$_2$ substrate$^{32,43}$ (Fig. 3.4). Our equation for the classical capacitance per unit
area is modified to include the fringing field capacitance based on the approach introduced by Liao\cite{32}

\[ C_{ox} = \varepsilon_{ox}\varepsilon_0 \left\{ \frac{\pi}{\ln[6(t_{ox}/W + 1)]W} + \frac{1}{t_{ox}} \right\} \]  

(3.1)

The first term in Equation 3.1 represents the GNR fringing capacitance and the second term is the GNR parallel plate capacitance. In the limit \( W \rightarrow \infty \), the equation reduces to the classical

\[ C_{ox} = \frac{\varepsilon_{ox}\varepsilon_0}{t_{ox}} \]  

(3.2)

as expected. In our case, quantum capacitance\cite{44} can be neglected due to the thickness of the buried oxide (~90 nm). Including the fringing capacitance of the GNR is important, as it leads to a correct extraction of the mobility, which appears lower than if the fringing effect is not included. Therefore, it is important that device and circuit engineers include GNR fringing capacitance in their analysis and models.

The extracted mobility values of our CVD GNRs (up to ~500 cm\(^2\)V\(^{-1}\)s\(^{-1}\)) are comparable to lithographically patterned exfoliated GNRs\cite{45} (200~1000 cm\(^2\)V\(^{-1}\)s\(^{-1}\)) and mostly lower than chemically derived GNRs\cite{17,32,46} (300~1500 cm\(^2\)V\(^{-1}\)s\(^{-1}\)). The similarity of exfoliated and CVD GNR mobilities is different than micron-scale CVD devices\cite{28}, which consistently show lower mobility than exfoliated graphene. This suggests GBs play less of a role in lowering GNR mobility than edge roughness scattering introduced from lithography. We believe that this is a consequence of the GNR dimensions being comparable to or smaller than the GB size of CVD-grown graphene.
3.2 Temperature-Dependent Measurements

We perform low-field measurements on AlO₃ capped GNRs in a vacuum probe station as a function of temperature. After pumping down to ~10⁻⁵ torr vacuum, we heat the chuck that the substrate sits on to 300 °C and let the GNR anneal for two hours. Next, we use liquid nitrogen to cool the vacuum probe station to ~80 K. After measurements at 80 K, we turn the heater on to increase the temperature of the probe station. When the temperature reaches ~120 K, we turn the heater off and repeat our measurements. Data is obtained in ~40 K increments until ~360 K. We fit the experimental results with our model and observe a weak dependence of mobility on temperature for two W = 40 nm GNRs over a temperature range of 80 to 360 K (Fig. 3.5). The mobility of a W = 20 nm GNR mobility increases up to room temperature and then slightly decreases with above room temperature. An increase in mobility with temperature can be an indication of charged impurity scattering limited low-field transport. Alternatively, recent works treat GNRs as electron and hole puddles approximately the size of their width. From this point of view, the apparent increase in mobility could be due to temperature-activated puddle hopping transport. Further systematic study is needed to determine the mechanism behind the temperature dependence of mobility in CVD GNRs.

3.3 High-Bias Measurements

To investigate the maximum current capacity (I_max) of the CVD GNRs, we perform room temperature, high-field I_D-v_D measurements in air for 22 GNRs with widths W = 15 to 50 nm and lengths L = 100 to 700 nm. V_D is incrementally increased until the GNR stops conducting due to physical breakdown which occurs at ~600 °C in air for graphene nanoribbons. We measure the drain current I_D as a function of drain voltage V_D. Figure 3.6(a) shows representative
data obtained from four GNRs. Unlike in carbon nanotube FETs\textsuperscript{48} and large-area exfoliated graphene FETs,\textsuperscript{49} current saturation is not observed in these GNRFETs before breakdown.

Maximum current densities in each batch are relatively high.\textsuperscript{50} The devices capped by an AlO$_x$ layer (Fig. 3.6(b), batch b1) show average $I_{\text{max}} \sim 0.7$ mA/μm, with the highest $I_{\text{max}} \sim 1.2$ mA/μm. For other devices (without the protective AlO$_x$ layer, batch b2) we found peak current density $I_{\text{max}} \sim 1.3$ mA/μm, with the highest value of $\sim 3.4$ mA/μm in air for the widest device measured ($W \sim 50$ nm). Due to variation and small sample size, it is not clear if the GNRs with an AlO$_x$ capping layer will always break at higher current densities than uncovered CVD GNRs. Two AlO$_x$ capped GNRs measured in vacuum both exhibited $I_{\text{max}} \sim 2.8$ mA/μm.

As shown in Fig 3.6(b), no clear scaling between $I_{\text{max}}$ and device dimensions ($L/W$ ratio) is found. Each batch of CVD GNRs has devices of similar $L/W$ ratios that exhibit an order of magnitude in $I_{\text{max}}$ variation. This suggests that sample-to-sample variability from impurities,\textsuperscript{18,51} edges,\textsuperscript{13,52,53} non-uniform graphene growth\textsuperscript{29} and contacts\textsuperscript{54,55} remains a concern and must be further improved.

The GNR breakdown power $P_{\text{BD}}$ scales approximately proportionally with GNR area (Fig. 3.6(c)), indicative of the role of heat dissipation from the GNR to the SiO$_2$ under such high-bias conditions.\textsuperscript{32,56} These GNRs also demonstrate a reciprocal relationship between breakdown current density and nanoribbon resistivity as shown in Fig. 3.6(d), similar to exfoliated graphene nanoribbons\textsuperscript{24} and CVD graphene microribbons.\textsuperscript{50} Using the relation $I_{\text{max}}/W = A\rho^{-n}$, the best fit for the data yields $n = 0.625$ with $R^2 \approx 0.75$. Generally, a value of $n$ close to unity suggests that the breakdown is primarily due to the electric field, while a value close to 0.5 corresponds to breakdown due to local heating at a certain temperature.\textsuperscript{50} Therefore, the value $n \approx 0.625$ ob-
tained here suggests that breakdown is first initiated at locations that are heated. For narrow GNRs, this probably results in the complete failure of the structure rather than being field-dependent.

As shown in Fig. 3.7, the dependence of breakdown current density with resistivity is similar to that of exfoliated GNRs and CVD graphene. However, for a given resistivity, the current carrying capacity of our CVD GNRs on 90nm SiO₂ is higher than the capacity of exfoliated GNRs and CVD graphene on 300 nm SiO₂. To understand the relationship between breakdown current density $J_{BR}$, resistivity $\rho$, and oxide thickness $t_{ox}$, we use equations from Liao⁴² to obtain the following (see Appendix A for the full derivation)

\[
J_{BR} = \frac{g(T_{BD} - T_0)}{t_g \rho W} \times \left[ \frac{\cosh \left( \frac{L}{2L_H} \right) + gL_H R_T \sinh \left( \frac{L}{2L_H} \right)}{\cosh \left( \frac{L}{2L_H} \right) + gL_H R_T \sinh \left( \frac{L}{2L_H} \right) - 1} \right]^{0.5}
\]

(3.3)

Here, $T_{BD}$ is the breakdown temperature, $T_0$ is ambient temperature, $t_g$ is the thickness of graphene, $W$ is the width of the GNR, $L$ is the length of the GNR, $L_H$ is the healing length along the graphene, and $R_T$ is the thermal resistance at the metal contacts.

The heat loss coefficient into the substrate $g$ is defined as

\[
g^{-1} = \left\{ \frac{\frac{\pi k_{ox}}{\ln[6(t_{ox}/W + 1)]} + k_{ox} W}{t_{ox}} \right\}^{-1} + \frac{R_{Cox}}{W},
\]

(3.4)

where $R_{Cox}$ is the thermal boundary resistance at the graphene/oxide interface, $k_{ox}$ is the thermal conductivity of the oxide, and $W$ is the width of the graphene nanoribbon. 
From (3.3) and (3.4) we observe that $J_{BR}$ decreases as $t_{ox}$ increases, in agreement with Fig. 3.7. This also agrees with physical intuition; graphene on a thick thermal insulator (300 nm SiO$_2$) will reach $T_{BD}$ at a lower power than graphene on a thin thermal insulator (90 nm SiO$_2$) because the thick insulator cannot dissipate heat as well as the thin insulator. Hence, for a given resistivity, breakdown current density will increase as oxide thickness decreases. As shown in Fig. 3.8, our model fits the data if we use a power of 0.53 instead of 0.5.

3.4 Figures

![Graph showing $I_D$ vs $V_D$ for different $V_G$ values. The inset shows the $R$ vs $V_G$ relationship.](image)

**Figure 3.1** Low field $I_D$-$V_D$ for a $W = 50$ nm and $L = 200$ nm GNRFET at room temperature in vacuum demonstrates ohmic contacts. Inset shows the $R$-$V_G$ for the same device.
Figure 3.2 Annealing in vacuum at 300 °C removes water and oxygen, shifting the Dirac point closer to zero for a $W = 40$ nm, $L = 400$ nm CVD GNR.

![Graph showing R vs V_G before and after anneal](image)

Figure 3.2

Figure 3.3 An example of fitting experimental GNR data (circles) with our model (lines). To fit the data for this $W = 20$ nm, $L = 200$ nm GNR, we use contact resistance $R_{CON} = 700\text{–}1000 \, \Omega \cdot \mu \text{m}$ and puddle charge density $n_0 = 1\text{–}4 \times 10^{12} \, \text{cm}^{-2}$.

![Graph showing R vs V_G for different conditions](image)

Figure 3.3
**Figure 3.4(a)** A fringing field capacitance exists between the conductive GNR and the Si++ back gate.

**Figure 3.5** Extracted hole mobility for three AlO$_x$ capped CVD GNRs. The GNRs exhibit a weak dependence on temperature. The variation in mobility between the 20 nm and 40 nm CVD GNRs is common; our CVD GNRs did not show a clear relationship between mobility and width. For these GNRs, our model used puddle charge density $n_0 = 1\times10^{12}$ cm$^{-2}$ and contact resistance $R_{CON} = 500$–1000 $\Omega\cdot\mu$m to fit the experimental data.
Figure 3.6 (a) High field CVD-grown GNR measurements. Unlike for CNTs, no current saturation is observed. (b) $I_{\text{MAX}}$ typically reaches $>1$ mA/μm but does not appear to scale with $L/W$. Most devices from batch b1 were broken in air except two that were broken in vacuum. (c) Breakdown power as a function of device area. (d) Breakdown current density has a power law dependence on the sheet resistance with a slope of $-0.625$. 
A similar dependence of breakdown current density on resistivity exists for large area CVD graphene on 300 nm SiO$_2$ (Lee et al.$^{30}$), CVD graphene nanoribbons on 90 nm SiO$_2$ (our work), and graphene nanoribbons patterned from exfoliated graphene on 300 nm SiO$_2$ (Murali et al.$^{24}$). Representative error bars are shown on four of the data points, and the CVD GNR data is fit (black line) using the equation $y = 4 \times 10^9 + 10x^{-0.624}$. Our devices on 90 nm oxide reach higher $J_{BR}$ than the devices on 300 nm oxide due to better heat dissipation of the thinner oxide.

**Figure 3.7** A similar dependence of breakdown current density on resistivity exists for large area CVD graphene on 300 nm SiO$_2$ (Lee et al.$^{30}$), CVD graphene nanoribbons on 90 nm SiO$_2$ (our work), and graphene nanoribbons patterned from exfoliated graphene on 300 nm SiO$_2$ (Murali et al.$^{24}$). Representative error bars are shown on four of the data points, and the CVD GNR data is fit (black line) using the equation $y = 4 \times 10^9 + 10x^{-0.624}$. Our devices on 90 nm oxide reach higher $J_{BR}$ than the devices on 300 nm oxide due to better heat dissipation of the thinner oxide.
Equation 3 agrees with our experimental data if we raise to the power of 0.53 instead of 0.5. The lower bound of the model assumes the CVD graphene is four layers thick, $W = 15$ nm, $L = 500$ nm, and the thermal conductivity of graphene $k_g = 50$ Wm$^{-1}$K$^{-1}$. The upper bound assumes single layer graphene, $W = 60$ nm, $L = 100$ nm, and $k_g = 500$ Wm$^{-1}$K$^{-1}$. $T_{BD}$ is 600 °C for both cases.
CHAPTER 4
CONCLUSION

We demonstrate large-scale fabrication of GNRs patterned from graphene grown by CVD. Our CVD GNRs have higher current carrying capacities and similar mobilities compared to GNRs fabricated using less scalable methods, suggesting that graphene grain boundaries play a negligible role in CVD GNRs. CVD graphene has a small D peak in its Raman spectra, whereas GNRs from both CVD and exfoliated graphene have sizeable disorder induced D and D' peaks in their Raman spectra. This supports the theory that CVD grain boundaries are negligible and points to nanoribbon edges as a major concern affecting performance and variability. The excellent current carrying capacity and the low \( I_{\text{ON}}/I_{\text{OFF}} \) ratios suggest that lithographically patterned CVD GNRs of dimensions \( W = 15–50 \) nm could be used in future large-scale integrated circuits as interconnects, but are not yet adequate for field-effect transistors. Future work to narrow the CVD ribbons and appropriately terminate edge dangling bonds is necessary to determine if a band gap suitable for digital electronics will result from quantum confinement. Temperature-dependent low-bias measurements reveal a weak temperature dependence of mobility. For a first order approximation, circuit design engineers could model the mobility of CVD GNR interconnects as temperature independent. In conclusion, CVD GNRs illustrate the promise of wafer-scale graphene integration while revealing variability, contacts, and impurities as future challenges for improving performance.
APPENDIX
DERIVATION OF EQUATION (3.3)

To understand the relationship between breakdown current density $J_{BR}$, resistivity $\rho$, and oxide thickness $t_{ox}$, we begin with the heat equation along graphene devices from Liao$^{32}$.

\[
P_{BD} = gL(T_{BD} - T_0) \times \left[ \frac{\cosh\left(\frac{L}{2L_H}\right) + gL_H R_T \sinh\left(\frac{L}{2L_H}\right)}{\cosh\left(\frac{L}{2L_H}\right) + gL_H R_T \sinh\left(\frac{L}{2L_H}\right) - 1} \right]
\]  
(A.1)

Here, $P_{BD}$ is the breakdown power, $T_{BD}$ is the breakdown temperature, $T_0$ is the ambient temperature, $L$ is the length of the graphene nanoribbon, $L_H$ is the thermal healing length along the graphene, and $R_T$ is the thermal resistance at the metal contacts. The heat loss coefficient into the substrate $g$ is defined as

\[
g^{-1} = \left\{ \frac{\pi k_{ox}}{\ln(6t_{ox}/W + 1)} + \frac{k_{ox} W}{t_{ox}} \right\}^{-1} + \frac{R_{Cox}}{W},
\]  
(A.2)

where $R_{Cox}$ is the thermal boundary resistance at the graphene/oxide interface, $k_{ox}$ is the thermal conductivity of the oxide, and $W$ is the width of the graphene nanoribbon.

To get $P_{BD}$ as a function of $J_{BR}$ and $\rho$, we first write $P_{BD}$ in terms of $I$ and $R$. Combining the definition of power $P_{BD} = IV$ and Ohm’s law $V = IR$ we get

\[
P_{BD} = I^2 R
\]  
(A.3)
Next we define $I$ in terms of $J_{BR}$ as $I = J_{BR} W t_g$, where $t_g$ is the thickness of the graphene.

Defining $R$ in terms of $\rho$ gives $R = \frac{\rho L}{W t_g}$. Substituting these definitions into (A.3) gives $P_{BD}$ as a function of $J_{BR}$ and $\rho$.

$$P_{BD} = J_{BR}^2 t_g \rho W L$$  \hspace{1cm} (A.4)

Substituting (A.4) into (A.1) and rearranging yields $J_{BR}$ as a function of $\rho$ and $t_{ox}$.

$$J_{BR} = \left( g \frac{g(T_{BD} - T_0)}{t_g \rho W} \times \left[ \frac{\cosh \left( \frac{L}{2L_H} \right) + gL_H R_T \sinh \left( \frac{L}{2L_H} \right)}{\cosh \left( \frac{L}{2L_H} \right) + gL_H R_T \sinh \left( \frac{L}{2L_H} \right) - 1} \right] \right)^{0.5}$$  \hspace{1cm} (A.5)
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