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FLOOD TIDE IN ILLINOIS

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Introduction

This article gives the highlights on three applied water-floods now operating in Illinois oil pools, points out earlier conditions which encouraged their application, and suggests territory favorable for water-flooding. It proposes a method of flooding certain old territory, without redrilling, and recommends flooding in the early life of certain pools.

Three Contrasting Floods

The three areas being flooded are shown in figure 1. These three operations are on sands of different ages and depths. They vary in the distances between wells and in the kind of water used. The only similarity is their success. Highest in the geologic column is the Siggins flood, operated by the Forest Oil Corporation on a Pennsylvanian sand. Lower is the Patoka flood, conducted by the Pelmont Corporation and the Sohio Oil Company on the Bethel sand, and last is the McClosky flood, operated by the Pure Oil Company on their extensive McClosky lime holdings. These three floods work on the state's productive sands of greatest areal extent.

The Siggins Operation

Under an agreement between the Ohio Oil Company and the Forest Oil Corporation, a flood was undertaken by the latter in the Siggins pool in Union Township, Cumberland County, and
Fig. 2. Well location map of the Siggins pool. This shows at A in figure 1.

Fig. 3. Contours on Siggins first sand, Siggins pool. Square near the center shows the location of the No. 2 flood. This is at the top of the structure. (Bull. 54, Pl. XXVII)

Fig. 4. Plan of the Siggins floods No. 2 and No. 3. Note the complete redrilling and close spacing of the No. 2 flood compared with the wider spacing and the drilling of input wells only in the No. 3 flood.

Fig. 5. Section and plan of Kraft flood. This was the first applied flood in Illinois. It made use of salt water injected from the surface as a flooding medium. It is the predecessor in Pennsylvanian sand to the Siggins operation. AA on figure 1 shows its location.

Fig. 1. The single letters on solid black territory indicate the present active floods, the double letters refer to earlier floods shown in detail in Figures 5, 14, and 15 and the triple letters designate territory favorable for future expansion.
Casey Township, Clark County, on part of the wells shown in figure 2, contoured on the top of the Siggins first sand in figure 3. The operation, called by them the No. 2 flood, covers 40 acres of the Chrysler farm, which occupies the SW. ¼ of the NE. ¼ of Sec. 13, T. 10 N., R. 10 E.

All the old wells were abandoned and plugged, and the 40 acres were redrilled in a pattern of five water wells on each boundary line filled in as a grid, making 25 water wells in all, with 16 producing wells drilled at the centers of squares formed by each set of four water-input wells (fig. 4). All the input and output wells were tubed with 1 ½-inch cement-lined pipe on cemented packers for the purpose of flowing the oil-producing wells.

The first 40 acres are not a commercial success because water flows too freely between the input and output wells, due either to overburden lifting from excessive early water pressures or from bypassing for the same reason. The greatest daily oil production from flood No. 2 was about 80 barrels, settling down to 40 barrels, accompanied by a volume of water that increased as the volume of oil diminished.

Before the Siggins operation started, sufficient evidence was available to lead to the belief that Pennsylvanian sands could be successfully flooded. Many ac-

PERMEABILITIES IN THREE ADJACENT WELLS

Fig. 6. Sand thickness diagram Siggins pool. This shows also the location of the No. 2 flood. The sand averages nearly seventy feet in thickness over the whole productive area. The net floodable sand averages over forty feet.

Fig. 7. Initial production diagram Siggins pool. The highest initial productions were found at the top of the structure in an area north of the No. 2 flood and covered by the No. 3 flood. Flood oil production was best in the areas of highest initial production.

Fig. 9. Permeabilities in three adjacent wells; determinations and graphs by Forest Oil Corporation. These are representative of the better parts of the Siggins pool. They are from wells of highest initial and cumulative production and better than average sand thickness. They are high on the structure.

Fig. 10. Intake well assembly Siggins pool. This is typical except that most intake wells have a second valve on the vertical pipe to the meter.
Cumulative Natural Production per Acre by Farms Siggins Pool

Fig. 8. Cumulative natural production per acre by farms Siggins pool. High productions correspond more closely to high initial productions and high structure than great sand thickness. The permeability profiles shown in figure 9 are taken in areas of high initial and cumulative production and greater than average sand thickness. The permeability profiles shown in figure 5 are from wells of lower initial and cumulative production.

Incidental floods, in which water in a stratum above had broken through the casing and traversed the oil sand, had greatly increased oil production. One of them, the Kraft farm operation, which started as an accidental flood, was converted by the writer into a commercially successful applied flood by injecting salt water from the surface. The operation is shown in plan and section in figure 5.

The Siggins operation was continued in flood No. 3, using a better method dictated by experience gained in the earlier operation. Two hundred acres north of the original 40 were developed with new input wells, drilled as five-spots at the centers of the squares formed by four old pumping wells. This procedure resulted in much wider spacing, water well to water well, and required the drilling of only a fraction of the earlier number of wells. Water pressure was kept below the danger point of 300 pounds per square inch, and the wells were pumped. These changes spelled success.

The Siggins first sand, as shown by the contour map, is an elongated dome having a maximum relief of about 140 feet. Structure, however, had no bearing on the method or success of the flooding operation.

Sand thicknesses (fig. 6), when considered along with oil content, had a greater influence. The map shows that
the south part of the No. 2 flood started in an area of relatively thin sand and that it and the No. 3 flood moved into areas of thicker and richer pay. Response to flooding closely followed these changing conditions.

Figure 7 shows initial well productions in the Siggins area.

In general, the best response to water-flooding corresponds to areas of greatest cumulative natural production (fig. 8). It is interesting to note that all this evidence agrees with findings made from core analyses and therefore would have been, even without core information, a reliable guide in the choice of the Siggins pool for flooding.

Figure 9 shows a series of permeability profiles, made for the most part from examinations of sand chips. They show high permeabilities and considerable variation from top to bottom. The operators use these profiles, also, as a guide in the location of packers. These high permeabilities prove that the extension of the well spacing for the No. 3 flood was logical.

Figure 10 shows the above-ground intake-well assembly. Oil content was determined in some cases by colorometric analyses. After selective shooting, caliper runs have been made to determine changes in well-bore profiles in order to find out to what extent the heavy shooting of dense sections increased their circumference over unshot or lightly shot open sections and in order to equalize water inlet. The greatest diameter obtained was 30 inches.

Figure 11 is a photograph of the com-
pany laboratory, and figure 12 is a photograph of the booster plant. Water is obtained from a well in the glacial drift in the valley of Hurricane Creek, pumped six miles through 6-inch pipe and boosted at the property by this pump to the desired input pressure. Unfiltered and untreated water has proved satisfactory because the system is entirely closed against oxidation, and the water is filtered by the gravel from which it is pumped.

The Screening Test

The success of the No. 3 flood will start a hunt for favorable producing strata on which to extend the process. In order to reduce the chances of failure, a screening test must be applied to Pennsylvanian and all other producing strata. Territory producing large quantities of water must be eliminated. Two operations in Illinois, one on sand which produced water from the day the first well was drilled and the other on sand which had become water-logged through badly abandoned wells, have been disappointing.

A second rule is to select rich territory. Richness can be checked by core analysis, by lease history, and by a combination of both. Figures 6, 7, and 8 give such a lease history for the Siggins field.

A study of a new field, by applying the tests shown in these drawings for the Siggins pool, provides a good screening test when supplemented by a determination of oil-water ratios from the wells under consideration. A permeability test, by electric logging old wells, will greatly help this screening test. Core analyses and oil production during flooding at Siggins have corroborated deductions made from preliminary screening.

Parts of the North Johnson pool, the first sand at Bellair (the Sussanah Smith Farm for example) as well as the New Hebron area, large parts of Oblong and Martin Townships in Crawford County that produce from the Robinson sand, and parts of the old Allen-dale field in Wabash County would stand up under such screening tests. Many areas in the new fields, no doubt, will do the same.

The Patoka Operation

The wells included in the Patoka flood are located in Secs. 20, 21, 28, and 29, T. 4 N., R. 1 E., Marion County, Illinois, near the town of Patoka, from which the pool takes its name.

Test-flooding was done at the north end of the field, in Sec. 21, the successful results of which led to a campaign in 1944 to drill intake wells and to flood

MAPS SHOWING NATURAL FLOOD ADVANCE AND ENRICHMENT OF DENNISON FLOOD

Fig. 14. Maps showing natural flood advance and enrichment of Dennison flood. This territory is shown also at CC figure 1. Water advanced from the southwest toward the northeast as shown by the contours and enriched each farm in its path with oil accumulated before. It demonstrates that pumping wells at the front edge of a flood may be by-passed by oil and is an argument in favor of five-spotting. (U.S. Geol. Survey Rept. Inv. No. 89, figure 27, p. 42, and figure 30, p. 45.)
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The (Cypress) Kirkwood wells of the old Lawrence County field produced from about the same depth as the Bethel sand at Patoka; they are spaced 9 wells to the 40-acres; the producing sand covers large areas with a thick uniform sand body; and the area has been unusually rich and free from water. The large initial productions of the wells indicate high sand permeability. All these factors favor flooding. The deductions from them are reinforced by the record production due to accidental flooding of wells on the Combos and Smith farms and by increased production due to water encroachment at Oakland City.

McClosky Operation

The third flooding process has taken place on McClosky lime in areas marked "Basin McClosky" on the general plan. It covers pools which are owned almost entirely by the Pure Oil Company, the block being so complete that it amounts to a unit operation with all the advantages of such a layout.

Nature taught the lesson. The McClosky natural water encroachments in Dennison and Petty Townships, Lawrence County (fig. 14), showed that water moved large quantities of oil and that permeable horizons were continuous over wide areas.

Flooding the McClosky was recommended by the Illinois Geological Survey in 1937 in Circular 23, "Contributions of the Fifth Annual Mineral Industries Conference," October 9, 1937, "Recent Developments in Water Flooding in Illinois Oil Fields," by Frederick Squires, page 123:

"Flood characteristics of the McClosky are these: Water travels fast, oil production is always benefitted. Only part of the area has been flooded. Therefore
there the obvious deductions are: (1) That the remaining McClosky should be intentionally flooded; (2) that this can be done without new drilling, by using alternate wells for flooding and pumping; and (3) that recoveries, if at all like natural floods, will amount to millions.

The Pure Oil Co. has started a series of floods shown in figures 15 and 16. They are using 32 old wells as input wells and produce from other old wells. The Basin McClosky was drilled in general with one well to 20 acres, although smaller areas had one well to 10 acres and still smaller tracts, drilled after Pearl Harbor, had one well to 40 acres. It is obvious from the map that almost all the 20-acre patterns have unequal distances, either 1,320 or 660 feet, between adjoining wells. The 10-acre pattern is a uniform 600-foot spacing, and the 40-acre pattern a uniform 1,320-foot spacing.

Water for the earliest injection in the southern end of the tract was obtained from the Pure's Little Wabash River pumping station. It was used without treatment and only a small amount of filtering. The McClosky lime is so open that nothing plugs it, making chemical treatment unnecessary. It should be remarked here that the areas under flood had reached their economic limit of yield under primary recovery methods before resorting to this secondary process. In later installations, the casing in input wells was perforated opposite the water-bearing Cypress, which flooded the McClosky under natural head. Twenty-eight separate floods have affected more than 3,800 acres to a greater or lesser degree.

Large volumes of water were used. The speed and direction of water advance has varied as shown by the dated contours surrounding each input well (figs. 17 and 18). Invasion is extremely rapid.

An oil production graph is given for two adjoining wells, shown here as figure 19. They are the first and second locations from the water-input well. The second location is usually more productive as is shown here.

The total oil production obtained to date from the 3,800 acres affected indicates that the production from all the McClosky acreage shown on the two McClosky maps will be very great when subjected to flooding.

Judging by the success already achieved in flooding the McClosky sand, a large proportion of the remaining territory will respond favorably. Such pools as Johnsonville seem certain to succeed.

The method now in use may be improved after longer experience. Fivespot well spacing and line flooding may be tried and the results compared, insofar as possible, with the circle floods now in operation.

Input water from the Cypress sand or other upper sands may be metered and regulated as conditions require. If and when new McClosky pools are found, the probability of later flooding should influence the location of wells. Certainly neighboring wells should be equidistant. A glance at figures 17 and 18 shows that permeabilities, always high, vary widely. A 40-acre spacing should work in such areas as 3 and 6 (on figs. 17 and 18). After developing on 40-acre spacing and noting the permeabilities encountered, closer spacing would be possible if necessary.

The next question to arise would be the time to flood. Reservoir pressure could be maintained by flooding as soon as the field was outlined. This would be a logical procedure.

**Summary**

The one thing that these three floods have in common is success (fig. 20). They vary in every other important respect—the sands, the flooding water, the age of the wells, the well spacing, and the number of new wells required (fig. 21). This is in striking contrast to flooding in Pennsylvania, New York, Kansas, and Oklahoma, where the operations have a much greater similarity. Experience gained in these fields cannot be applied to all the problems in Illinois, where each sand is a law unto itself. The principal difference between Illinois sands and out-of-state sands is permeability. The average high permeabilities for 50 wells each at 745 millidarcies for the Cypress, 221 for the Bethel, and 1,658 for the McClosky. Inasmuch as degree of permeability determines well spacing, Illinois sands with their greater permeability permit wider well spacing than do out-of-state sands, as is demonstrated in the spacing in the three fields just discussed. The Siggins No. 2 flood started with 330 feet between like wells (the Bradford technique); the
Siggins No. 3 increased this amount to 440 feet; Patoka went to 660 feet; and the Basin McClosky expanded it to an average of 1,000 feet.

By these figures it is demonstrated that the permeability of some oil sands in Illinois is so great that the minimum well spacing could be the same as (or greater than) the standard old field spacing of 400-440 feet. Therefore, such old fields can be flooded without redrilling but by using old wells only. Large areas of the Cypress, Bethel, and McClosky sands of the old fields come into this category. When their permeabilities would permit spacing wider than 440 feet between like wells, the only effect of using old wells is that their spacing, which is closer than is necessary, makes for a quicker clean up.

The early belief was that flooding should be applied only in the old age of wells, like those in the Siggins sand. The wells in the Patoka and McClosky floods are comparatively young; yet together they show even better results in flood production and have a far greater salvage value. The logical step appears to be to flood, or to conjointly repressurize and flood most fields soon after drilling, and to flow the wells from start to finish.

**Engineering Problems Involved**

The petroleum engineer should be encouraged to reinvestigate, since a rule need not be true just because it is old.

Bradford sands were once thought floodable only because they were tight. Now they are believed to be floodable in spite of their tightness. Illinois flooding presents many new problems, some of which are listed below.

A meter should be provided for measuring and a valve for regulating the water which leaves an upper sand to flood a lower sand. Both devices should record above ground.

A side-wall sampler should be designed to operate in shot holes in order to get permeability test samples from old wells and to aid in screening them for flooding.

Permeability should also be determined in the well itself. The weakest spot in any screening method is the lack of permeability data. Without it, there is no sure measure for well spacing. Without it, there is no sure way of telling whether old wells, without new drilling, may be flooded out within an economic time limit.

Permeability information might be determined in old wells by measuring fluid injections as the sand bore is filled up, foot by foot, with a removable seal. It might be obtained also by measuring the intake rates of two liquids of different conductivity under equal pressure when the interface is located by an electric pilot. Permeability to liquids might be computable from the results of tests on permeabilities to gases entering uniformly reduced sections of producing sand.

The use of alkaline flooding water was mentioned in a patent 1,238,355 issued to me many years ago. The method was tried only on sands, where it was
a failure, probably due to its action on clay. Alkaline water gives astonishingly good sand-washing results on small specimens in the laboratory but dismal failures in the field whenever clay is present in the sand. It should be demonstrated by field test whether or not the McClosky lime, which is always free from clay, will permit more successful flooding with alkaline than with neutral water.

A reliable selective plugging method is needed. Aquella, with its one-micron particle sizes, might be made to enter and plug sand pores that are too permeable. Gas injected in a five-spot water-flood might provide a retarding effect by blocking off the zones that are too permeable, thereby checking too rapid flooding. Alternating pressure and release of gas, effected through the output well of a water-flood five-spot, might check the advance of water through more permeable sections because of the speed differences of gas and liquid movement.

Horizontal drilling might be used in new ways. Horizontal holes in unworkable coal veins might be used as burning chambers provided with electric ignition, steam, air and gas currents in which gas is produced by incomplete combustion of coal. This lean gas could be enriched by passing it through oil sands. In many places, coal and oil strata are layer-caked in the Illinois coal basin.

The process of well cementing is open to improvement. Well casing might be formed with cement alone and without pipe. A mud sheath is formed every time a rotary well is drilled. Dr. Swann, inventor of the Swann underreamer, made a good start on a method of forming a cement sheath.

The introduction of heat and chemicals, such as gaseous HC1 into oil bearing lime formations should be thoroughly investigated. Flooding needs rustless pipe with threaded couplings. A practical coupling must be devised.

Almost every method for reservoir control depends on unification. It can be done for the farmer by a single clause in the lease. It needs to be simplified for the operator.

An example of such forward-looking problems and their solutions is illustrated in the electric logging permeability test made by the Survey on an old well in the Siggins No. 3 flood. Figure 22 shows the mobile laboratory in the background and the well logging equipment at the well. Figure 23 shows the geophysical log by C. A. Bays, and for comparison, permeabilities obtained from cores taken from neighboring wells and from the drilling log of the well itself.

The owners were satisfied with the results of the test because they used this well as a water input, and it has proved satisfactory for this purpose. This method of electric logging of old wells for relative permeabilities will be of great help in choosing old wells for flood possibilities as it fills out the screening program in the only test which cannot be determined by lease histories.

Conclusion

These three floods, conducted under widely different methods on as widely different sands, have reached the common goal of success. They cover only a small proportion of the area of the sands on which they operate and a far tinier fraction of the total area of the sands of Illinois. Each flood has proved to be a separate problem, for the solution of which out-of-state operations present little precedent. A tremendous opportunity for expansion lies ahead of the petroleum engineer.

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