

MAGNETIC CLUSTERS IN DILUTE ALLOYS OF IRON  
IN COPPER-NICKEL SOLID SOLUTIONS

BY

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## I. INTRODUCTION

It has been shown<sup>1</sup> that the paramagnetic properties of f.c.c. copper-rich Cu-Ni solid solutions change considerably when small amounts of Fe are added. For virtually Fe-free  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy, the temperature dependent part of the susceptibility is very small, but it increases greatly with Fe addition. A preliminary investigation<sup>2</sup> indicated that in quenched alloys up to a level of 100 ppm Fe most Fe atoms tend to form a magnetic dipole (including the moment of nearest neighbor Ni atoms) with a moment of  $\mu = 3.76 \mu_B$ . For a quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy with 1000 ppm Fe the magnetization can be well described,<sup>2</sup> on the assumption of clustering of Fe atoms, in terms of magnetic dipoles associated with one, two, three, and four, or more Fe atoms.

From Mössbauer source experiments Bennett et al.<sup>3</sup> concluded that a small isolated magnetic cluster with  $\mu = 4.2 \mu_B$  is centered on each Fe atom in a rapidly quenched  $\text{Cu}_{0.79}\text{Ni}_{0.21}$  alloy, to which trace amounts of  $^{57}\text{Co}$  have been added. Similar, but larger, magnetic clusters were shown to exist<sup>3</sup> in alloys of higher Ni content. From  $^{57}\text{Fe}$  Mössbauer absorption data for alloys with higher Fe concentrations (0.25 to 3%) Bennett et al.<sup>4</sup> concluded that in these alloys two distinct moment values are present; the smaller moment was claimed to be identical with that observed in the source experiments<sup>3</sup> and the larger



moment was ascribed to coupled pairs of the smaller clusters. The concentration of the two moment species, derived from the analysis of Mössbauer spectral line intensities, were claimed to be consistent,<sup>4</sup> within a factor of two, with a model, which assumes that the Fe and the Ni atoms are randomly distributed in the alloy and that the larger moment is formed when one small Fe-Ni cluster is the nearest neighbor of another. Under such conditions the two Fe moments may be coupled, even when one is the ninth-nearest neighbor of the other. Thus Bennett et al.<sup>4</sup> have in effect, proposed a long-range interaction between Fe moments via nearest neighbor Ni moments.

In contrast to the views of Bennett et al.<sup>4</sup> Window et al.<sup>5</sup> concluded from the isomer shift and the quadrupole splitting in Mössbauer spectra of dilute alloys of <sup>57</sup>Fe in Cu-Ni that both Fe-Fe and Fe-Ni clustering tendencies are present in Cu-Ni-Fe alloys.

As the above discussion points out, previous work has not unequivocally cleared up the question whether Cu-Ni-Fe alloys are random<sup>4</sup> or clustering effects are present.<sup>2,5</sup> In order to resolve this question it was decided to carry out extensive magnetization measurements as a function of the Fe content for Cu<sub>0.9</sub>Ni<sub>0.1</sub> and Cu<sub>0.8</sub>Ni<sub>0.2</sub> alloys containing 100 to 1000 ppm Fe. The reason for choosing Ni concentrations of 10 and 20 atomic percent is that at these compositions very few, if any, magnetic clusters are formed in the absence of Fe,<sup>1</sup> while at



are formed by Ni moments. For Fe levels up to 1000 ppm, the concentrations of single Fe and Fe pair clusters can be well determined from an analysis of the magnetization in terms of Brillouin functions.<sup>2</sup> These values may then be compared with the concentrations calculated on the basis of complete randomness.<sup>4</sup> If complete randomness is found to be inappropriate, and Fe-Fe clustering has to be postulated, it can be determined how the short range order parameter changes with the composition.

A long-range interaction between Fe moments, assuming randomness of the Fe atoms, has also been suggested for dilute Cu-Fe alloys.<sup>6</sup> However, recent Mössbauer work resolved<sup>7,8</sup> the presence in Cu-Fe alloys of Fe nearest neighbor pairs and larger aggregates in concentrations greater than that expected for random alloys. We therefore set out to make a careful re-examination of available magnetic data,<sup>6,9</sup> in order to ascertain whether or not they indicate the presence of magnetic clusters in dilute Cu-Fe alloys.

Based on observations of hyperfine splitting in Mössbauer spectra, it was suggested that Cu-Fe and Cu-Ni-Fe alloys are magnetically ordered at low temperatures.<sup>5,10,11</sup> It has been decided to check the validity of this suggestion by means of magnetization measurements.



## II. SPECIMEN PREPARATION

### A. Materials

The copper used for preparing the alloys was obtained in rod form from the American Smelting & Refining Company. It was 99.99% pure and contained less than 0.7 parts per million of Fe and 0.5 parts per million of Cr. High purity nickel (W.A.W. Grade; 99.99%) was supplied in strip form by the International Nickel Company. The major impurities present in the nickel were: Al (0.001%) and Ag (0.001%). All other impurities present were in concentrations of less than 0.0005%. The iron used was 99.98% pure. The major impurity was Ni (0.01%). The impurity content of each of these metals as reported by the suppliers is listed in Tables 1 and 2.

### B. Melting

To facilitate weighing out the right amount for melting, the copper rod was cut into short lengths. The cut pieces were pickled in a 30%  $\text{HNO}_3$  solution which removed the outer layers of the material. The residual acid was removed by washing repeatedly in distilled water, and finally in alcohol. As soon as the cleaning was finished the metal was placed under vacuum in a bell jar in order to prevent surface contamination and oxidation. The nickel strip was cut into rectangular pieces and then cleaned by etching, using a solution consisting of 1500



Table 1. Analysis of W.A.W. grade nickel (99.99%).

| Impurity | % Amount |
|----------|----------|
| Al       | < 0.001  |
| As       | < 0.0001 |
| B        | < 0.0001 |
| Ca       | < 0.0001 |
| Cu       | < 0.0004 |
| Pb       | < 0.0005 |
| Mg       | < 0.0001 |
| Pd       | < 0.0001 |
| Ag       | < 0.001  |
| Na       | < 0.0001 |
| Sn       | < 0.0003 |
| Ti       | < 0.0001 |
| Zn       | < 0.0001 |
| V        | < 0.0001 |
| Zr       | < 0.0001 |

Not found: Sb, Ba, Bi, Cs, Cr, Co, Cd, Ga, Ge, Au, In, Ir, La, Li, Mn, Hg, Mo, Os, Pt, K, Rh, Rb, Ru, Sc, Si, Sr, Ta, Te, Tl, W, Y.



Table 2. Spectrographic analysis of copper (99.999%) and lot analysis of iron.

| Impurity    | Amount in ppm. |
|-------------|----------------|
| Copper      |                |
| Fe          | < 0.7          |
| Sb          | < 1.0          |
| Pb          | < 1            |
| Sn          | < 1            |
| Ni          | < 1            |
| Bi          | < 0.1          |
| Cr          | < 0.5          |
| Si          | < 0.1          |
| Te          | < 2            |
| Ag          | < 0.3          |
| As          | < 2            |
| Iron        |                |
| Ti          | 20             |
| Mn          | 10             |
| Ni          | 100            |
| Al          | 5              |
| Balance Fe. |                |



parts concentrated  $\text{H}_2\text{SO}_4$ , 2250 parts concentrated  $\text{HNO}_3$ , 1000 parts  $\text{H}_2\text{O}$  and 30 grams  $\text{NaCl}$ . An etching time of about 10 seconds was found to be very satisfactory at room temperature. The residual reagent was removed by rinsing with distilled water and then with absolute alcohol. The iron was in the form of clean, shiny pieces and was cleaned with distilled water and absolute alcohol.

A special technique was developed for the preparation of virtually Fe-free Cu-Ni solid solutions. The technique involved melting the charge in a recrystallized alumina crucible under a slightly oxidizing atmosphere in an induction furnace. It was expected that any iron present would form iron oxide because of its greater affinity for oxygen. The empty alumina crucible was baked for four hours prior to the melting in order to drive out adsorbed moisture. Then the charge (about 20 grams) was placed in it and the crucible lowered into the furnace. The system was pumped down to about 5 microns of mercury and flushed several times with argon. Just before switching on the power, a calculated amount of air was introduced along with 1/2 atmosphere of argon so as to give a melting atmosphere with approximately 0.5% oxygen. Once the charge was completely molten ripples could be observed at the surface of the molten pool through a plexi-glass window at the top of the furnace. The power was kept "on" for 10 more minutes to insure good mixing. The alloy was then left in the furnace for about 3 hours to cool. The weight loss during melting was



The binary  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ ,  $\text{Cu}_{0.52}\text{Ni}_{0.48}$ ,  $\text{Cu}_{0.54}\text{Ni}_{0.46}$ ,  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  and  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys were melted as described above. Two additional binary alloys, i.e.,  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$ , prepared during the course of an earlier investigation by us, were also used in the present work. The  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy was induction melted in an argon atmosphere and later remelted in an arc furnace; the  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  was melted in the induction furnace in a slightly oxidizing atmosphere, described above.

Small known amounts of Fe additions (up to 1000 atomic ppm) to the binary  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ ,  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  and  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys were made as follows. First of all a master alloy (No. 1) was prepared by arc melting, using tungsten electrode and a water cooled copper crucible. This alloy was of the composition  $\text{Ni}_{0.95}\text{Fe}_{0.05}$ . The melting was carried out under approximately one atmosphere of argon gas and repeated six times, turning the button upside down on the copper crucible after each melting operation. This was expected to give a more uniform distribution of Fe. The arc melted button was rolled to a thickness of 0.007". This was cut into very small pieces and cleaned by etching with the same reagent which was used for cleaning the high purity nickel. A longer etching time was employed to dissolve completely any Fe contamination on the surface. This master alloy (No. 1) was used in turn to prepare another master alloy (No. 2) of the composition  $\text{Ni}_{0.999}\text{Fe}_{0.001}$ . The procedure was the same as that just described. Master alloy No. 2 was used to make small additions of Fe, in desired amounts, to the  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  (100 at ppm),



$\text{Cu}_{0.8}\text{Ni}_{0.2}$  (250 and 500 ppm) and  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  (100, 500 and 1000 ppm) alloys. An appropriate amount of the master alloy was placed underneath a piece of the binary Cu-Ni alloy and then the charge was arc melted, striking the arc on the latter. Melting was repeated three times. A  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 1000 at ppm Fe, melted in this way in our earlier investigation<sup>1,2</sup> was also used for the purposes of the present work. The specimen of a  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 100 ppm Fe, and prepared in the way discussed above during the course of the earlier work, was also available, but its size was found to be too small for accurate magnetization measurements, having been reduced in diameter for the high field measurements of Reference 2. A new alloy of this composition was prepared. The 100 ppm Fe alloy of Reference 2 shall be referred to as the "old  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy with 100 ppm Fe."

Three alloys containing 1% Fe, namely  $\text{Cu}_{0.99}\text{Fe}_{0.01}$ ,  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$  and  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$ , were also prepared by arc melting. But here no master alloy was used; appropriate amounts of the metals were melted together, and the melting was repeated four times, turning the button upside down between successive melting operations.

### C. Homogenizing Treatment

The as-cast buttons were first cold worked by compressing in a vise between two clean steel plates in three mutually perpendicular directions. The amount of deformation in each case



was about 20%. During compression the alloy button was kept at a temperature of  $\sim 100^\circ \text{C}$  with the help of a hot air gun. This aided in preventing the formation of cracks. The deformed alloy button, covered by molybdenum foil to act as an oxygen-getter, was enclosed in a fused silica capsule with  $1/4$  atmosphere of argon, then homogenized at  $1050^\circ \text{C}$  (or,  $1000^\circ \text{C}$ ; see Table 3) for 24 hours and quenched into water (or, iced-brine). A suitable portion was cut out from each homogenized button. This piece was deformed, in the same way as discussed above, and then ground into the desired shape, reannealed for 1 hour and quenched. This double deformation technique ensures good homogenization. This was established in the following manner. The magnetization of a  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy (prepared before the present investigation), deformed only once and quenched from  $1050^\circ \text{C}$ , was found to be  $0.519 \text{ emu/g}$  at  $4.2^\circ \text{K}$  in an applied field of  $1.26 \text{ kOe}$ ; after a second deformation and quenching from the high temperature the magnetization was found under the same conditions as before to be  $0.544 \text{ emu/g}$  ( $\sim 4.5\%$  higher). After repeating the deformation and quenching process a third time, measurements were found to yield a magnetization value of  $0.539 \text{ emu/g}$ . The reproducibility between the second and third measurements was thus better than  $1\%$  indicating that the degree of homogenization when the alloy was annealed following the second deformation was adequate.



Table 3. List of alloys used in the present investigation.

|  | Alloy                                | Method of Melting                      | Quenching Temperature | Quenching Medium | Shape of Specimen              |
|--|--------------------------------------|----------------------------------------|-----------------------|------------------|--------------------------------|
|  | $\text{Cu}_{0.5}\text{Ni}_{0.5}$     | Induction<br>(oxidizing atmosphere)    | 1050° C               | Water            | Spherical                      |
|  | $\text{Cu}_{0.52}\text{Ni}_{0.48}$   | - do -                                 | - do -                | - do -           | - do -                         |
|  | $\text{Cu}_{0.54}\text{Ni}_{0.46}$   | - do -                                 | - do -                | - do -           | - do -                         |
|  | $\text{Cu}_{0.6}\text{Ni}_{0.4}$     | - do -                                 | - do -                | - do -           | Cylindrical                    |
|  | $\text{Cu}_{0.7}\text{Ni}_{0.3}$     | Induction<br>(remelted in Arc furnace) | - do -                | - do -           | Rectangular-<br>Parallelepiped |
|  | $\text{Cu}_{0.8}\text{Ni}_{0.2}$     | Induction<br>(oxidizing atmosphere)    | - do -                | - do -           | Cylindrical                    |
|  | $\text{Cu}_{0.9}\text{Ni}_{0.1}$     | - do -                                 | - do -                | - do -           | Rectangular-<br>Parallelepiped |
|  | $\text{Ni}_{0.95}\text{Fe}_{0.05}$   | Arc                                    |                       |                  |                                |
|  | $\text{Ni}_{0.999}\text{Fe}_{0.001}$ | - do -                                 |                       |                  |                                |



Table 3 (Continued)

| Alloy                                              | Method of Melting | Quenching Temperature | Quenching Medium | Shape of Specimen              |
|----------------------------------------------------|-------------------|-----------------------|------------------|--------------------------------|
| 100 ppm Fe in<br>$\text{Cu}_{0.7}\text{Ni}_{0.3}$  | Arc               | 1050° C               | Water            | Rectangular-<br>Parallelepiped |
| 100 ppm Fe in<br>$\text{Cu}_{0.8}\text{Ni}_{0.2}$  | - do -            | - do -                | - do -           | - do -                         |
| 250 ppm Fe in<br>$\text{Cu}_{0.8}\text{Ni}_{0.2}$  | - do -            | - do -                | - do -           | - do -                         |
| 500 ppm Fe in<br>$\text{Cu}_{0.8}\text{Ni}_{0.2}$  | - do -            | - do -                | - do -           | - do -                         |
| 1000 ppm Fe in<br>$\text{Cu}_{0.8}\text{Ni}_{0.2}$ | - do -            | - do -                | - do -           | Cylindrical                    |
| 100 ppm Fe in<br>$\text{Cu}_{0.9}\text{Ni}_{0.1}$  | - do -            | - do -                | - do -           | Rectangular-<br>Parallelepiped |
| 500 ppm Fe in<br>$\text{Cu}_{0.9}\text{Ni}_{0.1}$  | - do -            | - do -                | - do -           | - do -                         |



#### D. Deformed and Aged Specimens

After carrying out magnetization measurements with the as-quenched specimens of the  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys with 100, 500 and 1000 ppm Fe, and  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys with 100, 500 and 1000 ppm Fe, the specimens were deformed by about ~20% in three mutually perpendicular directions, this time without the use of the hot air gun, and magnetic measurements were made in the deformed state.

In the case of the  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy, after making measurements in the as-quenched condition the specimen was aged at 300° C for 3 days and quenched into water and measurements were made in the aged condition.

#### E. Chemical Analysis

Some of the iron-containing alloys were analyzed by absorption spectrophotometric methods to determine the actual iron concentrations. The results of such analyses are presented in Table 4. For each alloy two samples were analyzed. Except for the  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy with a nominal concentration of 250 ppm Fe, the results of the analyses agree with the intended composition within experimental accuracy. The  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy with 250 ppm Fe was found to be inhomogeneous. It was not possible to determine the reason for this inhomogeneity. For all ternary Cu-Ni-Fe alloys analyzed, the iron content was found to be slightly greater than the corresponding nominal concentration.



Table 4. Results of quantitative analysis for iron by spectrophotometry.

| Alloy                                              | Atomic ppm Fe | Average Atomic ppm Fe |
|----------------------------------------------------|---------------|-----------------------|
| (a) Cu-Ni-Fe                                       |               |                       |
| 100 ppm Fe in Cu <sub>0.9</sub> Ni <sub>0.1</sub>  | 108 ± 3       | 108                   |
|                                                    | 108 ± 3       |                       |
| 500 ppm Fe in Cu <sub>0.9</sub> Ni <sub>0.1</sub>  | 524 ± 16      | 521                   |
|                                                    | 518 ± 16      |                       |
| 1000 ppm Fe in Cu <sub>0.9</sub> Ni <sub>0.1</sub> | 1052 ± 34     | 1051                  |
|                                                    | 1050 ± 34     |                       |
| 100 ppm Fe in Cu <sub>0.8</sub> Ni <sub>0.2</sub>  | 118 ± 3       | 116                   |
|                                                    | 114 ± 3       |                       |
| 250 ppm Fe in Cu <sub>0.8</sub> Ni <sub>0.2</sub>  | 288 ± 8       | 312                   |
|                                                    | 336 ± 8       |                       |
| 500 ppm Fe in Cu <sub>0.8</sub> Ni <sub>0.2</sub>  | 545 ± 14      | 559                   |
|                                                    | 573 ± 14      |                       |
| (b) Cu-Fe                                          |               |                       |
| Cu <sub>0.99</sub> Fe <sub>0.01</sub>              | 9110 ± 230    | 9250                  |
|                                                    | 9390 ± 240    |                       |



Table 5. Results of mass spectrographic analysis for impurities. The concentrations are reported in atomic ppm within a factor of 3. Symbols: X--not detected; \*--see Table 4.

| Alloy                                           | Cr   | Mn         | Fe  | Co         | W          | Mo      |
|-------------------------------------------------|------|------------|-----|------------|------------|---------|
| $\text{Cu}_{0.6}\text{Ni}_{0.4}$                | 0.8  | 0.2        | 4.2 | 2.5        | X          | X       |
| $\text{Cu}_{0.5}\text{Ni}_{0.5}$                | 4    | 4          | 15  | X          | X          | 300     |
| $\text{Cu}_{0.99}\text{Fe}_{0.01}$              | 0.06 | X          | *   | X          | X          | X       |
| 100 ppm Fe in $\text{Cu}_{0.9}\text{Ni}_{0.1}$  | 3    | $\leq 0.3$ | *   | 3          | 6          | 1       |
| 500 ppm Fe in $\text{Cu}_{0.9}\text{Ni}_{0.1}$  | 1    | $\leq 0.2$ | *   | $\leq 0.3$ | 1          | $< 0.1$ |
| 1000 ppm Fe in $\text{Cu}_{0.9}\text{Ni}_{0.1}$ | 1    | $\leq 0.1$ | *   | $\leq 0.1$ | $\leq 0.4$ | 0.3     |
| 100 ppm Fe in $\text{Cu}_{0.8}\text{Ni}_{0.2}$  | 4    | 0.5        | *   | 3.5        | X          | 4.8     |
| 250 ppm Fe in $\text{Cu}_{0.8}\text{Ni}_{0.2}$  | 2.5  | 0.5        | *   | 2.5        | X          | 70      |
| 500 ppm Fe in $\text{Cu}_{0.8}\text{Ni}_{0.2}$  | 3    | 0.6        | *   | 4          | X          | 20      |



For the sake of convenience, however, we shall continue to refer to the alloys by their nominal concentrations.

Samples from some of the alloys were analyzed for minor impurities. The analyses were carried out by mass-spectrographic methods. The results are listed in Table 5.

Both types of analyses, i.e., absorption spectro-photometric and mass-spectrographic, were performed by the Chemical Analysis Division at the Materials Research Laboratory, University of Illinois.

#### F. Storage of Specimens

Since it has been reported<sup>6</sup> that Cu-Fe alloys change their magnetic properties when stored at room temperature over long periods of time, the  $\text{Cu}_{0.99}\text{Fe}_{0.01}$ ,  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$ , and  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  alloys were stored in liquid nitrogen when not in use. All other specimens were stored at room temperature.



### III. EXPERIMENTAL PROCEDURE

#### A. Force Measurement

The magnetization measurements were made by the Faraday method. In the Faraday method the force acting on a specimen in a nonuniform magnetic field is measured. The magnetic field is so arranged that the direction of the field is horizontal ( $H_X$  in Oersteds) and the gradient of the field is in the vertical direction ( $Z$ ). A force  $F_Z$ , proportional to the susceptibility  $\chi$  (defined here as  $\frac{\sigma}{H_X}$  where  $\sigma$  is the magnetization) acts in the direction of the field gradient:

$$F_Z = \chi H_X \frac{dH_X}{dz} \quad (1)$$

The force is measured by means of a balance, as an apparent weight change  $\Delta w$  (in grams). The susceptibility of the specimen in emu/g is calculated from the weight change

$$\chi = \Delta w (980.1) / H_X \frac{dH_X}{dz} \cdot W \quad (2)$$

where 980.1 is the acceleration due to gravity in  $\text{cm/sec}^2$  and  $W$  is the specimen mass in grams.

The specimen was suspended by means of a gold chain in the field produced by a Varian electromagnet. An aluminium heat shield was mounted near the specimen. (Prior to September 1970, a nylon string was used instead of the gold chain. All our measurements reported earlier<sup>1,2</sup> made use of this practice. It was



later noticed that the nylon string had a tendency to shrink a little when the surrounding medium was evacuated, thus displacing the specimen from the geometric center of the magnet gap. With a gold chain this problem does not arise.) The weight change  $\Delta w$ , in an applied field  $H$  (in the following we shall use the notation " $H$ " for " $H_X$ "), was calculated as:

$$\Delta w = {}_H W_{\text{specimen}} - {}_{H=0} W_{\text{specimen}} - \Delta w_g \quad (3)$$

where the term  $\Delta w_g$  is the apparent weight change upon application of the field in the absence of a specimen. It represents the force acting on the gold chain and the aluminium heat shield in the field of the magnet. An automatic mechanism, located within the bell jar, housing the balance, allows the weights to be added or removed from the tare pan in one milligram increments up to a total of 100 milligrams. Weights smaller than one milligram were read from a strip chart recorder automatically operated by the balance.

## B. Measurement and Control of Temperature

### 1. Cryostat for 300°K to 4.2°K (metal cryostat).

To control the temperature of the specimen in the temperature range 300-4.2°K, a cold finger type of cryostat was used. In this cryostat liquid helium is drawn up through a capillary and a 1/4" copper tube wound around the specimen chamber, thus cooling the specimen in turn. By varying the rate at which the helium is drawn up the tube, the temperature can be continuously



varied from 300° to 4.2°K. The temperature was measured by a Phylatron Model CD-500A GaAs sensor. A detailed description of the cryostat and the temperature measuring circuit can be found in the thesis of E. E. Barton, Jr.<sup>12</sup> Recently (1971) the length of the capillary has been changed to 2", and a filter assembly, using two 0.45 micron pore-filters, has been added between the capillary and the helium supply. These two changes were made for the purpose of reducing thermal oscillations at temperatures near 4.2°K.

## 2. Cryostat for 4.2°K to 1.3°K (glass cryostat).

Magnetization measurements in the temperature range of 4.2°K to 1.3°K were made in a double glass cryostat. In this case the specimen is suspended in a glass tube which is surrounded by a bath of liquid helium. The temperature can then be controlled by controlling the pressure of the helium vapor over the bath with the help of a vacuum pump. The temperature was determined by measuring the vapor pressure of the helium with a mercury manometer. The procedures for the operation of the cryostat and the measurement of the temperature are described in detail in the thesis of R. D. Shull.<sup>13</sup>

## C. Measurement of the Field

In our present work the applied field (0 to 12.6 kOe) was measured by means of a Hall probe (InAs diode, Model FC-34, manufactured by Siemens). Previously (our measurements reported



in 1970; see References 1 and 2) it was the practice to measure the applied field with the help of a rotating coil gaussmeter positioned as close as possible to the specimen at the center of the magnet gap. This method resulted in a small error since the field actually experienced by the specimen was slightly different from that recorded by the gaussmeter; the positions of the gaussmeter and of the specimen were not exactly the same. For the present investigation, the Hall probe readings were calibrated with the rotating coil of the gaussmeter positioned at the center of the gap. In order to calibrate the field gradient, the magnetization of a spherical nickel specimen, prepared from WAW grade Ni, was measured at 293°K as a function of the applied field between 0.2 and 12.7 kOe and compared with corresponding literature values. The details of the calibration of the field and of the field gradient are discussed in detail in a special report.<sup>14</sup>

#### D. Corrections

(1). It was pointed out that in order to obtain the correct apparent weight change  $\Delta w$  of the specimen in an applied field  $H$  (Eq. 3) the weight change  $\Delta w_g$  due to the gold chain and to the shield assembly should be subtracted. The quantity  $\Delta w_g$  was measured as a function of field (up to  $\sim 12.6$  kOe) at various fixed temperatures (between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  with the metal cryostat and between  $4.2^\circ$  and  $1.35^\circ\text{K}$  with the glass cryostat) and as a function of temperature in a constant applied field of  $\sim 12.6$  kOe



(Table 6). It was found that the variation of  $\Delta w_g$  (mg) with the field (kOe) and the temperature ( $^{\circ}\text{K}$ ) can be described by the following equations:

$$\Delta w_g = \begin{cases} (0.0128 - 5.88 \times 10^{-6} T) H^{1.81} & T \geq 80^{\circ}\text{K} \\ (0.0121 + \frac{4.54 \times 10^{-3}}{T}) H^{1.81} & T \leq 80^{\circ}\text{K} \end{cases} \quad (4)$$

(2). Of late (May, 1972) it has been found advantageous to make a small correction to the weight reading given by the Ainsworth microbalance, the balance weights (two 1mg, one 2mg, one 5mg, two 10mg, one 20mg, and one 50mg) apparently not being exact integer multiples of 1mg. The details of this correction may be found in the thesis of R. W. Tustison.<sup>15</sup> It should be noted that apart from this correction, the observed reproducibility of the balance was  $\pm 0.01\text{mg}$ .

The accuracy of the force, temperature, and field measurements is discussed in the thesis of R. D. Shull.<sup>13</sup>

#### E. Additional Measurements

Additional magnetization measurements were made on some of the specimens with a Foner-type vibrating-specimen magnetometer at the University of Illinois in Chicago. These measurements were made at  $4.2^{\circ}\text{K}$  as a function of applied field from 0 to 55 kOe. The  $4.2^{\circ}\text{K}$  isothermal data so obtained by the Foner method were found to be different (lower in all cases but one) from similar data obtained by the Faraday method in fields up to



Table 6. Measured values of  $\Delta w_g$  as a function of temperature and field. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat.

| T<br>(°K) | H<br>(Oe) | $\Delta w_g$<br>(mg) | T<br>(°K) | H<br>(Oe) | $\Delta w_g$<br>(mg) |
|-----------|-----------|----------------------|-----------|-----------|----------------------|
| 295.13    | 12738     | 1.099                | 64.78     | 12640     | 1.224                |
|           | 10857     | 0.830                | 52.46     | 12640     | 1.226                |
|           | 8900      | 0.590                | 34.45     | 12640     | 1.223                |
|           | 7160      | 0.412                | 24.39     | 12640     | 1.219                |
|           | 5677      | 0.284                | 16.69     | 12640     | 1.227                |
|           | 4618      | 0.164                |           |           |                      |
|           | 3690      | 0.112                | 11.09     | 12702     | 1.239                |
|           | 2741      | 0.067                |           | 10833     | 0.921                |
|           | 1492      | 0.022                |           | 8884      | 0.651                |
|           | 411       | 0.001                |           | 7147      | 0.446                |
|           |           |                      |           | 5667      | 0.262                |
| 242.16    | 12640     | 1.134                |           | 4611      | 0.186                |
| 188.65    | 12640     | 1.151                |           | 3684      | 0.125                |
| 132.64    | 12640     | 1.183                |           | 2734      | 0.065                |
| 99.30     | 12640     | 1.193                |           | 1487      | 0.021                |
|           |           |                      |           | 404       | 0.001                |
| 78.08     | 12738     | 1.224                |           |           |                      |
|           | 10857     | 0.921                | 6.61      | 12640     | 1.239                |
|           | 8900      | 0.651                |           |           |                      |
|           | 7158      | 0.457                | 4.2       | 12604     | 1.338                |
|           | 5670      | 0.311                |           | 10847     | 1.054                |
|           | 4615      | 0.185                |           | 8905      | 0.754                |
|           | 3689      | 0.125                |           | 7160      | 0.469                |
|           | 2739      | 0.075                |           | 5679      | 0.312                |
|           | 1490      | 0.028                |           | 4626      | 0.195                |
|           | 411       | 0.008                |           | 3694      | 0.134                |
|           | 209       | 0.003                |           | 2744      | 0.080                |



Table 6. (Continued)

| T<br>(°K) | H<br>(Oe) | $\Delta w_g$<br>(mg) | T<br>(°K) | H<br>(Oe) | $\Delta w_g$<br>(mg) |
|-----------|-----------|----------------------|-----------|-----------|----------------------|
| 4.2       | 1500      | 0.028                | 1.35      | 12560     | 1.557                |
|           | 415       | 0.006                |           | 10849     | 1.148                |
|           | 275       | 0.002                |           | 8904      | 0.819                |
|           | 214       | 0.001                |           | 7162      | 0.586                |
|           |           |                      |           | 5680      | 0.334                |
| 3.38      | 12640     | 1.333                |           | 4622      | 0.240                |
| 2.81      | 12640     | 1.360                |           | 3699      | 0.150                |
| 1.90      | 12640     | 1.436                |           | 2746      | 0.083                |
|           |           |                      |           | 1503      | 0.033                |
|           |           |                      |           | 414       | 0.003                |
|           |           |                      |           | 274       | 0.001                |



12.6 kOe. In some cases where the absolute value of the magnetization was small, e.g., for 100 ppm Fe in  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  the magnetization in a field of 12.6 kOe is  $\sim 8.9 \times 10^{-3}$  emu/g at 4.2°K, reproducibility of the vibrating magnetometer data was very poor. For the  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy, where the absolute value of the magnetization is quite large (i.e., of the order of  $\sim 0.5$  emu/g in 12 kOe field at 4.2°K), the difference in the magnetization values obtained by the vibrating magnetometer and Faraday methods was rather small. Therefore except for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ , the vibrating magnetometer data obtained at Chicago were not utilized.

Magnetization measurements on the quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy (Reference 1) were also performed at 4.2°K and in fields up to 54 kOe with a vibrating magnetometer by Dr. S. Foner at the National Magnet Laboratory at M. I. T., Cambridge. These data were somewhat lower than the corresponding Faraday technique data obtained by us during the course of our earlier investigation<sup>1</sup> of the same alloy. In spite of uncertainties of the Foner data, it was found possible to use these high field data for the analysis.

For the two alloys  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  and  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ , the Faraday technique data were assumed to be more accurate in an absolute sense. The higher field magnetometer data were used as relative values and they were normalized to the Faraday method data by using a constant factor determined at fields of 12.6 kOe and less,

$$\sigma = \sigma_F R$$



where,

$R$  is the normalization factor

$\sigma_F$  is the magnetization in emu/g as measured with the  
vibrating-specimen magnetometer

$\sigma$  is the normalized magnetization in emu/g

The normalization factors used are listed in the corresponding  
data tables.



#### IV. EXPERIMENTAL RESULTS

##### A. Data Tables



Table 7. Magnetization data for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ . The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 1, 2, 5, and 9.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 299.44    | 12566     | 0.092               | 40.25     | 7649      | 3.078               |
| 243.20    | 12538     | 0.125               |           | 7365      | 3.050               |
| 189.81    | 12538     | 0.192               |           | 6241      | 2.923               |
| 132.57    | 12538     | 0.399               |           | 5084      | 2.766               |
| 101.12    | 12535     | 0.740               |           | 4065      | 2.587               |
|           |           |                     |           | 3298      | 2.431               |
| 78.08     | 12529     | 1.308               |           | 2102      | 2.080               |
|           | 10649     | 1.155               |           | 1016      | 1.560               |
|           | 8705      | 0.976               |           | 913       | 1.501               |
|           | 6998      | 0.807               |           | 802       | 1.389               |
|           | 5548      | 0.656               |           | 669       | 1.255               |
|           | 4524      | 0.542               |           | 605       | 1.194               |
|           | 3611      | 0.436               |           | 503       | 1.089               |
|           | 2640      | 0.320               |           | 442       | 1.000               |
|           | 1404      | 0.172               |           | 315       | 0.820               |
|           | 369       | 0.036               |           | 308       | 0.783               |
|           |           |                     |           | 281       | 0.750               |
| 53.31     | 9646      | 2.354               |           | 258       | 0.720               |
|           | 7867      | 2.147               |           | 226       | 0.672               |
|           | 6241      | 1.913               |           | 213       | 0.657               |
|           | 5079      | 1.711               |           | 193       | 0.597               |
|           | 4455      | 1.502               |           | 161       | 0.524               |
|           | 3295      | 1.311               |           | 129       | 0.442               |
|           | 2099      | 0.943               |           | 97        | 0.362               |
|           | 1017      | 0.509               |           | 64        | 0.269               |
|           | 407       | 0.203               |           | 32        | 0.198               |



Table 7. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 34.80     | 6882      | 3.409               | 29.98     | 6343      | 3.710               |
|           | 6232      | 3.344               |           | 6226      | 3.694               |
|           | 5086      | 3.215               |           | 5091      | 3.592               |
|           | 4061      | 3.069               |           | 4064      | 3.474               |
|           | 3298      | 2.935               |           | 3300      | 3.371               |
|           | 2099      | 2.658               |           | 2102      | 3.147               |
|           | 1017      | 2.255               |           | 1019      | 2.848               |
|           | 929       | 2.216               |           | 866       | 2.768               |
|           | 866       | 2.158               |           | 739       | 2.716               |
|           | 802       | 2.102               |           | 611       | 2.664               |
|           | 738       | 2.082               |           | 483       | 2.586               |
|           | 674       | 2.059               |           | 357       | 2.472               |
|           | 610       | 2.004               |           | 290       | 2.458               |
|           | 546       | 1.955               |           | 226       | 2.407               |
|           | 482       | 1.866               |           | 194       | 2.254               |
|           | 418       | 1.795               |           | 161       | 2.278               |
|           | 354       | 1.714               |           | 129       | 2.185               |
|           | 322       | 1.690               |           | 97        | 2.113               |
|           | 290       | 1.654               |           | 81        | 2.044               |
|           | 258       | 1.622               |           | 64        | 1.783               |
|           | 226       | 1.522               |           | 44        | 1.261               |
|           | 193       | 1.459               |           | 32        | 1.087               |
|           | 161       | 1.326               |           | 16        | 0.851               |
|           | 129       | 1.281               | 25.22     | 5910      | 4.007               |
|           | 97        | 1.199               |           | 5082      | 3.942               |
|           | 64        | 1.060               |           | 4061      | 3.853               |
|           | 32        | 0.993               |           | 3299      | 3.767               |
|           |           |                     |           | 2498      | 3.662               |



Table 7. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 25.22     | 2085      | 3.596               | 20.08     | 4236      | 4.249               |
|           | 1269      | 3.451               |           | 3866      | 4.214               |
|           | 1022      | 3.393               |           | 4040      | 4.224               |
|           | 866       | 3.308               |           | 3529      | 4.188               |
|           | 738       | 3.312               |           | 3092      | 4.148               |
|           | 611       | 3.280               |           | 2563      | 4.083               |
|           | 482       | 3.221               |           | 2085      | 4.025               |
|           | 418       | 3.192               |           | 1548      | 3.953               |
|           | 354       | 3.156               |           | 1015      | 3.868               |
|           | 290       | 3.129               |           | 866       | 3.830               |
|           | 258       | 3.094               |           | 739       | 3.805               |
|           | 226       | 3.074               |           | 611       | 3.771               |
|           | 193       | 3.026               |           | 483       | 3.749               |
|           | 161       | 3.002               |           | 419       | 3.742               |
|           | 145       | 2.986               |           | 354       | 3.716               |
|           | 129       | 2.985               |           | 290       | 3.684               |
|           | 113       | 2.776               |           | 258       | 3.652               |
|           | 97        | 2.538               |           | 226       | 3.617               |
|           | 81        | 2.086               |           | 193       | 3.589               |
|           | 64        | 1.836               |           | 161       | 3.563               |
| 20.08     | 48        | 1.470               |           | 145       | 3.349               |
|           | 32        | 1.211               |           | 129       | 3.305               |
|           | 24        | 1.135               |           | 113       | 2.950               |
|           | 16        | 0.908               |           | 97        | 2.622               |
|           | 8         | 0.794               |           | 81        | 2.108               |
|           |           |                     |           | 64        | 1.915               |
|           |           |                     |           | 48        | 1.576               |
|           |           |                     |           | 32        | 1.229               |
|           | 5458      | 4.327               |           |           |                     |
|           | 4747      | 4.283               |           |           |                     |



Table 7. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 20.08     | 24        | 0.996               | 14.98     | 64        | 1.868               |
|           | 16        | 0.813               |           | 48        | 1.564               |
|           | 8         | 0.680               |           | 40        | 1.392               |
|           |           |                     |           | 32        | 1.229               |
| 14.98     | 5080      | 4.632               |           | 24        | 1.021               |
|           | 4699      | 4.619               |           | 16        | 0.718               |
|           | 4061      | 4.578               |           | 8         | 0.680               |
|           | 3678      | 4.562               |           |           |                     |
|           | 3288      | 4.531               | 10.39     | 4830      | 4.902               |
|           | 2602      | 4.478               |           | 4441      | 4.890               |
|           | 2030      | 4.433               |           | 4057      | 4.872               |
|           | 1605      | 4.383               |           | 3589      | 4.851               |
|           | 1214      | 4.360               |           | 3305      | 4.843               |
|           | 1006      | 4.318               |           | 2625      | 4.807               |
|           | 866       | 4.316               |           | 2084      | 4.761               |
|           | 739       | 4.287               |           | 1447      | 4.740               |
|           | 611       | 4.286               |           | 1024      | 4.695               |
|           | 483       | 4.263               |           | 897       | 4.676               |
|           | 354       | 4.257               |           | 739       | 4.657               |
|           | 290       | 4.179               |           | 611       | 4.653               |
|           | 258       | 4.227               |           | 483       | 4.689               |
|           | 226       | 4.194               |           | 418       | 4.627               |
|           | 194       | 4.137               |           | 354       | 4.603               |
|           | 161       | 3.790               |           | 290       | 4.578               |
|           | 145       | 3.511               |           | 258       | 4.616               |
|           | 129       | 3.204               |           | 226       | 4.575               |
|           | 113       | 2.878               |           | 193       | 4.372               |
|           | 97        | 2.584               |           | 161       | 3.871               |
|           | 81        | 2.214               |           | 145       | 3.523               |



Table 7. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 10.39     | 129       | 3.150               | 3.22      | 3796      | 5.211               |
|           | 113       | 2.899               |           | 3487      | 5.205               |
|           | 97        | 2.590               |           | 3176      | 5.197               |
|           | 81        | 2.081               |           | 2864      | 5.184               |
|           | 64        | 1.769               |           | 2550      | 5.171               |
|           | 48        | 1.469               |           | 2236      | 5.168               |
|           | 32        | 1.087               |           | 1920      | 5.150               |
|           | 24        | 1.046               |           | 1603      | 5.135               |
|           | 16        | 0.718               |           | 1282      | 5.135               |
| 4.2       | 8         | 0.605               |           | 964       | 5.122               |
|           |           |                     |           | 644       | 5.102               |
|           | 4501      | 5.204               |           | 484       | 5.104               |
|           | 4087      | 5.188               |           | 323       | 5.066               |
|           | 3794      | 5.180               |           | 258       | 5.014               |
|           | 3485      | 5.168               |           | 194       | 4.507               |
|           | 3174      | 5.159               |           | 129       | 3.333               |
|           | 2862      | 5.144               |           | 65        | 1.875               |
|           | 2549      | 5.136               | 1.95      | 4508      | 5.258               |
|           | 2234      | 5.120               |           | 4105      | 5.256               |
|           | 1919      | 5.095               |           | 3796      | 5.264               |
|           | 1602      | 5.086               |           | 3487      | 5.244               |
|           | 1281      | 5.072               |           | 3176      | 5.235               |
|           | 963       | 5.061               |           | 2864      | 5.227               |
|           | 644       | 5.040               |           | 2550      | 5.224               |
|           | 323       | 4.691               |           | 2236      | 5.208               |
|           |           |                     |           | 1920      | 5.191               |
| 3.22      | 4505      | 5.231               |           | 1603      | 5.183               |
|           | 4105      | 5.221               |           |           |                     |



Table 7. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 1.95      | 1282      | 5.190               | 1.63      | 2863      | 5.235               |
|           | 964       | 5.175               |           | 2550      | 5.227               |
|           | 644       | 5.163               |           | 2235      | 5.213               |
|           | 484       | 5.161               |           | 1920      | 5.199               |
|           | 323       | 5.150               |           | 1603      | 5.190               |
|           | 258       | 5.079               |           | 1281      | 5.186               |
|           | 194       | 4.497               |           | 964       | 5.179               |
|           | 129       | 3.244               |           | 644       | 5.140               |
|           | 64        | 1.830               |           | 483       | 5.173               |
|           |           |                     |           | 323       | 5.121               |
| 1.63      | 4506      | 5.260               |           | 258       | 5.073               |
|           | 4104      | 5.260               |           | 194       | 4.494               |
|           | 3796      | 5.252               |           | 129       | 3.274               |
|           | 3486      | 5.242               |           | 64        | 1.687               |
|           | 3175      | 5.240               |           |           |                     |



Table 8. Magnetization data for quenched  $\text{Cu}_{0.52}\text{Ni}_{0.48}$ . The measurements were made in the glass cryostat. See Figures 3 and 10.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 4.2       | 12499     | 3.597               | 2.81      | 5617      | 3.512               |
|           | 11677     | 3.582               |           | 4708      | 3.493               |
|           | 10842     | 3.566               |           | 3788      | 3.465               |
|           | 9998      | 3.551               |           | 2858      | 3.417               |
|           | 9144      | 3.527               |           | 1916      | 3.351               |
|           | 8279      | 3.504               |           | 643       | 3.224               |
|           | 7403      | 3.484               | 1.48      | 12503     | 3.666               |
|           | 6516      | 3.465               |           | 11676     | 3.655               |
|           | 5618      | 3.434               |           | 10841     | 3.644               |
|           | 4709      | 3.389               |           | 9997      | 3.631               |
|           | 3789      | 3.356               |           | 9143      | 3.620               |
|           | 2858      | 3.291               |           | 8278      | 3.606               |
|           | 1916      | 3.202               |           | 7402      | 3.592               |
|           | 962       | 3.127               |           | 6515      | 3.574               |
| 2.81      | 12530     | 3.635               |           | 5617      | 3.552               |
|           | 11677     | 3.622               |           | 4708      | 3.544               |
|           | 10842     | 3.607               |           | 3788      | 3.510               |
|           | 9997      | 3.594               |           | 2858      | 3.454               |
|           | 9143      | 3.579               |           | 1916      | 3.428               |
|           | 8278      | 3.566               |           | 1279      | 3.374               |
|           | 7402      | 3.548               |           | 643       | 3.327               |
|           | 6515      | 3.526               |           | 322       | 3.311               |



Table 9. Magnetization data for quenched  $\text{Cu}_{0.54}\text{Ni}_{0.46}$ . The measurements were made in the glass cryostat. See Figures 4 and 11.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 4.2       | 12536     | 2.409               | 4.2       | 32        | 1.090               |
|           | 11689     | 2.388               |           | 16        | 0.844               |
|           | 10853     | 2.370               |           | 8         | 0.633               |
|           | 10007     | 2.350               |           |           |                     |
|           | 9153      | 2.325               | 2.89      | 12574     | 2.468               |
|           | 8287      | 2.298               |           | 11686     | 2.451               |
|           | 7410      | 2.264               |           | 10850     | 2.430               |
|           | 6522      | 2.233               |           | 10005     | 2.410               |
|           | 5623      | 2.196               |           | 9150      | 2.389               |
|           | 4714      | 2.149               |           | 8285      | 2.368               |
|           | 3793      | 2.086               |           | 7408      | 2.341               |
|           | 2861      | 2.001               |           | 6521      | 2.314               |
|           | 1918      | 1.935               |           | 5622      | 2.277               |
|           | 1280      | 1.803               |           | 4712      | 2.244               |
|           | 963       | 1.713               |           | 3792      | 2.194               |
|           | 643       | 1.611               |           | 2860      | 2.127               |
|           | 483       | 1.540               |           | 1917      | 2.032               |
|           | 387       | 1.500               |           | 1280      | 1.935               |
|           | 322       | 1.470               |           | 962       | 1.864               |
|           | 260       | 1.404               |           | 643       | 1.762               |
|           | 196       | 1.310               |           | 322       | 1.645               |
|           | 161       | 1.330               |           | 56        | 1.298               |
|           | 129       | 1.284               |           |           |                     |
|           | 97        | 1.254               | 1.45      | 12618     | 2.518               |
|           | 64        | 1.266               |           | 11681     | 2.508               |
|           | 48        | 1.172               |           | 10846     | 2.490               |



Table 9. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 1.45      | 10001     | 2.479               | 1.45      | 2859      | 2.265               |
|           | 9147      | 2.462               |           | 1917      | 2.189               |
|           | 8281      | 2.445               |           | 1279      | 2.122               |
|           | 7405      | 2.427               |           | 962       | 2.047               |
|           | 6518      | 2.404               |           | 643       | 2.001               |
|           | 5620      | 2.381               |           | 322       | 1.859               |
|           | 4710      | 2.352               |           | 206       | 1.781               |
|           | 3790      | 2.315               |           | 58        | 1.447               |



Table 10. Magnetization data for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$ . The measurements were made in the metal cryostat. See Figures 13, 14, and 36.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 300.38    | 12554     | 1.806                                 | 14.84     | 12570     | 1.987                                 |
| 242.44    | 12549     | 1.762                                 | 10.92     | 12570     | 1.974                                 |
| 190.69    | 12560     | 1.843                                 | 8.89      | 12568     | 2.012                                 |
| 130.37    | 12562     | 1.766                                 |           |           |                                       |
| 99.17     | 12560     | 1.736                                 | 4.2       | 12638     | 2.521                                 |
| 76.64     | 12564     | 1.771                                 |           | 10770     | 2.101                                 |
| 60.44     | 12560     | 1.776                                 |           | 8838      | 1.701                                 |
| 44.88     | 12560     | 1.818                                 |           | 7101      | 1.432                                 |
| 34.63     | 12565     | 1.868                                 |           | 5639      | 1.040                                 |
| 33.18     | 12570     | 1.831                                 |           | 4591      | 0.883                                 |
| 25.33     | 12572     | 1.895                                 |           | 3662      | 0.743                                 |
| 20.84     | 12570     | 1.978                                 |           |           |                                       |



Table 11. Magnetization data for quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ .

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|

(a) Faraday method data. These measurements were made in the metal cryostat. See Figures 14 and 15.

|        |       |       |      |       |       |
|--------|-------|-------|------|-------|-------|
| 299.27 | 12638 | 13.00 | 7.84 | 12638 | 16.83 |
| 215.11 | 12638 | 13.05 | 6.1  | 12638 | 17.39 |
| 131.15 | 12638 | 13.30 |      |       |       |
| 76.45  | 12638 | 13.77 | 4.2  | 12608 | 18.84 |
| 60.91  | 12638 | 13.96 |      | 10674 | 16.17 |
| 40.54  | 12638 | 14.39 |      | 8784  | 13.07 |
| 24.85  | 12638 | 14.97 |      | 5601  | 8.10  |
| 11.09  | 12638 | 16.25 |      | 3637  | 5.24  |

(b) Normalized magnetometer data.  
Normalization factor  $R=1.068$ .  
See Figure 15.

|     |       |       |     |       |       |
|-----|-------|-------|-----|-------|-------|
| 4.2 | 54300 | 76.04 | 4.2 | 23160 | 34.30 |
|     | 50407 | 71.00 |     | 19267 | 28.56 |
|     | 46514 | 66.31 |     | 15375 | 21.93 |
|     | 42622 | 61.10 |     | 12608 | 18.66 |
|     | 38729 | 55.79 |     | 10674 | 15.83 |
|     | 34837 | 50.48 |     | 8784  | 12.99 |
|     | 30944 | 45.09 |     | 5601  | 8.31  |
|     | 27052 | 39.78 |     | 3637  | 5.31  |



Table 12. Magnetization data for quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ .

| T<br>(°K)                                                                                                                                                                                                    | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| (a) Faraday method data. The measurements between<br>~300°K and 4.2°K were made in the metal cryostat;<br>the measurements at and below 4.2°K were made in<br>the glass cryostat. See Figures 16 through 19. |           |                                       |           |           |                                       |
| 298.41                                                                                                                                                                                                       | 12567     | 3.32                                  | 29.47     | 2644      | 3.08                                  |
| 243.49                                                                                                                                                                                                       | 12570     | 3.62                                  |           | 1406      | 1.48                                  |
| 190.77                                                                                                                                                                                                       | 12566     | 4.03                                  |           |           |                                       |
| 131.15                                                                                                                                                                                                       | 12571     | 5.09                                  | 20.58     | 12552     | 18.50                                 |
| 95.04                                                                                                                                                                                                        | 12569     | 6.25                                  |           | 10669     | 15.99                                 |
| 74.75                                                                                                                                                                                                        | 12558     | 7.29                                  |           | 8688      | 13.11                                 |
| 61.49                                                                                                                                                                                                        | 12558     | 8.43                                  |           | 7010      | 10.70                                 |
|                                                                                                                                                                                                              |           |                                       |           | 5556      | 8.49                                  |
| 40.84                                                                                                                                                                                                        | 12541     | 11.48                                 |           | 4521      | 6.86                                  |
|                                                                                                                                                                                                              | 10666     | 9.78                                  |           | 3613      | 5.57                                  |
|                                                                                                                                                                                                              | 8714      | 8.04                                  |           | 2643      | 4.09                                  |
|                                                                                                                                                                                                              | 7004      | 6.42                                  |           | 1409      | 1.94                                  |
|                                                                                                                                                                                                              | 5554      | 5.07                                  |           |           |                                       |
|                                                                                                                                                                                                              | 4524      | 4.04                                  | 14.84     | 12566     | 23.74                                 |
|                                                                                                                                                                                                              | 3612      | 3.36                                  |           | 10680     | 20.48                                 |
|                                                                                                                                                                                                              | 2642      | 2.36                                  |           | 8711      | 16.99                                 |
|                                                                                                                                                                                                              | 1406      | 1.21                                  |           | 7015      | 13.97                                 |
|                                                                                                                                                                                                              |           |                                       |           | 5563      | 11.10                                 |
| 29.47                                                                                                                                                                                                        | 12552     | 14.57                                 |           | 4528      | 9.21                                  |
|                                                                                                                                                                                                              | 10670     | 12.42                                 |           | 3617      | 7.45                                  |
|                                                                                                                                                                                                              | 8718      | 10.22                                 |           | 2641      | 5.34                                  |
|                                                                                                                                                                                                              | 7016      | 8.25                                  |           | 1409      | 2.84                                  |
|                                                                                                                                                                                                              | 5557      | 6.53                                  |           |           |                                       |
|                                                                                                                                                                                                              | 4522      | 5.30                                  | 10.39     | 12554     | 29.77                                 |
|                                                                                                                                                                                                              | 3613      | 4.27                                  |           | 10673     | 26.17                                 |



Table 12. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 10.39     | 8720      | 22.21                          | 2.52      | 4060      | 30.32                          |
|           | 7014      | 18.40                          |           | 3297      | 26.74                          |
|           | 5561      | 15.01                          |           | 2101      | 19.77                          |
|           | 4520      | 12.47                          |           | 1019      | 11.26                          |
|           | 3616      | 10.03                          |           | 642       | 7.66                           |
|           | 2646      | 7.56                           |           | 467       | 4.44                           |
|           | 1407      | 3.92                           |           | 374       | 3.80                           |
| 4.20      |           |                                |           | 292       | 3.27                           |
|           | 12694     | 45.49                          |           | 245       | 2.65                           |
|           | 11556     | 43.45                          |           | 212       | 2.00                           |
|           | 9743      | 39.90                          | 1.49      | 12675     | 54.17                          |
|           | 7881      | 35.49                          |           | 11540     | 52.60                          |
|           | 6255      | 30.93                          |           | 9733      | 50.01                          |
|           | 5091      | 27.18                          |           | 7868      | 46.73                          |
|           | 4066      | 22.96                          |           | 6244      | 43.19                          |
|           | 3301      | 19.74                          |           | 5081      | 40.03                          |
|           | 2104      | 13.15                          |           | 4057      | 36.32                          |
|           | 1018      | 7.01                           |           | 3295      | 33.01                          |
|           | 538       | 3.04                           |           | 2097      | 26.03                          |
|           | 340       | 1.87                           |           | 1014      | 16.48                          |
|           | 257       | 1.55                           |           | 636       | 11.73                          |
|           | 205       | 1.16                           |           | 534       | 10.11                          |
|           |           |                                |           | 443       | 6.66                           |
| 2.52      | 12678     | 50.84                          |           | 338       | 5.46                           |
|           | 11540     | 49.11                          |           | 289       | 4.74                           |
|           | 9730      | 46.03                          |           | 254       | 4.35                           |
|           | 7869      | 41.91                          |           | 229       | 3.94                           |
|           | 6246      | 38.00                          |           |           |                                |



Table 12. (Continued)

| T<br>(°K)                                                                                       | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-------------------------------------------------------------------------------------------------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| (b) Normalized magnetometer data.<br>Normalization factor $R=1.046$ .<br>See Figures 16 and 18. |           |                                |           |           |                                |
| 4.2                                                                                             | 55000     | 82.80                          | 4.2       | 15000     | 49.20                          |
|                                                                                                 | 50000     | 79.82                          |           | 12000     | 44.30                          |
|                                                                                                 | 45000     | 76.61                          |           | 10000     | 40.42                          |
|                                                                                                 | 40000     | 73.22                          |           | 8000      | 35.80                          |
|                                                                                                 | 35000     | 69.56                          |           | 6000      | 30.13                          |
|                                                                                                 | 30000     | 65.58                          |           | 4000      | 22.85                          |
|                                                                                                 | 25000     | 61.00                          |           | 2000      | 13.14                          |
|                                                                                                 | 20000     | 55.68                          |           |           |                                |



Table 13. Magnetization data for aged  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ .

| T<br>(°K)                                                                                                                                                                                                     | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| (a) Faraday method data. The measurements between<br>~300°K and 4.2°K were made in the metal cryostat;<br>the measurements at and below 4.2°K were made<br>in the glass cryostat. See Figures 18, 19, and 20. |           |                                |           |           |                                |
| 297.33                                                                                                                                                                                                        | 12559     | 3.27                           | 40.84     | 12566     | 14.77                          |
|                                                                                                                                                                                                               | 10670     | 2.71                           |           | 10660     | 12.54                          |
|                                                                                                                                                                                                               | 8716      | 2.25                           |           | 8665      | 9.99                           |
|                                                                                                                                                                                                               | 7007      | 1.81                           |           | 6993      | 8.04                           |
|                                                                                                                                                                                                               | 4517      | 1.14                           |           | 5534      | 6.89                           |
|                                                                                                                                                                                                               | 5551      | 1.47                           |           | 4503      | 5.61                           |
|                                                                                                                                                                                                               | 3609      | 1.01                           |           | 3598      | 3.83                           |
|                                                                                                                                                                                                               | 2645      | 0.82                           |           | 2634      | 2.89                           |
| 244.19                                                                                                                                                                                                        | 12583     | 3.52                           | 34.63     | 3573      | 4.77                           |
| 189.75                                                                                                                                                                                                        | 12578     | 4.10                           |           |           |                                |
| 132.64                                                                                                                                                                                                        | 12581     | 5.40                           | 20.58     | 12560     | 26.11                          |
| 101.14                                                                                                                                                                                                        | 12581     | 6.72                           |           | 10645     | 22.47                          |
|                                                                                                                                                                                                               |           |                                |           | 8683      | 18.60                          |
| 77.67                                                                                                                                                                                                         | 12578     | 8.31                           |           | 6981      | 15.14                          |
|                                                                                                                                                                                                               | 10682     | 6.91                           |           | 5531      | 12.42                          |
|                                                                                                                                                                                                               | 8722      | 5.70                           |           | 4503      | 10.27                          |
|                                                                                                                                                                                                               | 7013      | 4.65                           |           | 3592      | 7.62                           |
|                                                                                                                                                                                                               | 5560      | 3.63                           |           | 2651      | 5.10                           |
|                                                                                                                                                                                                               | 4523      | 2.97                           |           | 1401      | 3.21                           |
|                                                                                                                                                                                                               | 3612      | 2.42                           |           |           |                                |
|                                                                                                                                                                                                               | 2642      | 1.86                           | 15.27     | 3573      | 10.71                          |
|                                                                                                                                                                                                               | 1406      | 0.90                           |           | 2626      | 7.53                           |
| 60.60                                                                                                                                                                                                         | 12578     | 10.13                          | 10.39     | 12594     | 42.03                          |
| 52.55                                                                                                                                                                                                         | 12578     | 11.66                          |           | 10702     | 37.88                          |



Table 13. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 10.39     | 8741      | 32.54                          | 2.52      | 12615     | 68.97                          |
|           | 6976      | 27.79                          |           | 10718     | 65.96                          |
|           | 5574      | 23.12                          |           | 8725      | 61.10                          |
|           | 4540      | 19.51                          |           | 6896      | 56.71                          |
|           | 3624      | 15.96                          |           | 5579      | 51.98                          |
|           | 2651      | 12.25                          |           | 4539      | 47.72                          |
|           | 1409      | 6.30                           |           | 3629      | 42.79                          |
| 7.06      |           |                                |           | 2656      | 36.35                          |
|           | 12525     | 50.60                          |           | 1409      | 25.11                          |
|           | 10631     | 46.12                          |           | 1056      | 20.32                          |
|           | 8673      | 40.83                          |           | 373       | 8.55                           |
|           | 6974      | 35.50                          |           | 241       | 5.69                           |
|           | 5531      | 30.54                          | 1.49      | 12602     | 72.93                          |
|           | 4500      | 26.21                          |           | 10713     | 70.23                          |
|           | 3597      | 21.30                          |           | 8759      | 66.79                          |
|           | 2631      | 16.66                          |           | 7037      | 63.10                          |
|           | 1399      | 9.66                           |           | 5579      | 58.77                          |
| 4.2       |           |                                |           | 4540      | 55.01                          |
|           | 12602     | 62.41                          |           | 3627      | 50.55                          |
|           | 10719     | 58.30                          |           | 2652      | 44.20                          |
|           | 8754      | 53.40                          |           | 1411      | 33.06                          |
|           | 7039      | 48.07                          |           | 1214      | 30.93                          |
|           | 5579      | 42.60                          |           | 1067      | 28.82                          |
|           | 4544      | 38.00                          |           | 953       | 26.86                          |
|           | 3626      | 32.11                          |           | 804       | 24.52                          |
|           | 2656      | 26.12                          |           | 644       | 21.12                          |
|           | 1411      | 16.31                          |           | 484       | 18.40                          |
|           | 372       | 5.08                           |           | 323       | 15.54                          |
|           |           |                                |           | 216       | 11.61                          |



Table 13. (Continued)

| T<br>(°K)                                                                                 | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-------------------------------------------------------------------------------------------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| (b) Normalized magnetometer data.<br>Normalization factor $R = 0.989$ .<br>See Figure 18. |           |                                |           |           |                                |
| 4.2                                                                                       | 55000     | 99.42                          | 4.2       | 15000     | 65.75                          |
|                                                                                           | 50000     | 96.55                          |           | 12000     | 60.50                          |
|                                                                                           | 45000     | 93.51                          |           | 10000     | 56.17                          |
|                                                                                           | 40000     | 90.23                          |           | 8000      | 50.88                          |
|                                                                                           | 35000     | 86.73                          |           | 6000      | 44.18                          |
|                                                                                           | 30000     | 82.76                          |           | 4000      | 35.04                          |
|                                                                                           | 25000     | 78.00                          |           | 2000      | 21.52                          |
|                                                                                           | 20000     | 72.80                          |           |           |                                |



Table 14. Magnetization data for quenched  $\text{Cu}_{0.99}\text{Fe}_{0.01}$ . The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. The data are listed in the order in which they were taken.

| T<br>(°K)                                                                      | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|--------------------------------------------------------------------------------|-----------|---------------------|-----------|-----------|---------------------|
| (a) Specimen cooled in an applied field<br>of $\sim 12.65$ kOe. See Figure 26. |           |                     |           |           |                     |
| 295.57                                                                         | 12648     | 0.0298              | 35.08     | 5636      | 0.1561              |
| 245.53                                                                         | 12648     | 0.0383              |           | 4585      | 0.1281              |
| 189.10                                                                         | 12648     | 0.0543              |           | 3664      | 0.1063              |
| 159.30                                                                         | 12647     | 0.0725              |           | 2716      | 0.0681              |
| 99.95                                                                          | 12646     | 0.1169              |           | 1477      | 0.0459              |
|                                                                                |           |                     |           | 402       | 0.0155              |
| 77.84                                                                          | 12644     | 0.1491              |           |           |                     |
|                                                                                | 10794     | 0.1258              | 24.86     | 12633     | 0.3764              |
|                                                                                | 8849      | 0.1025              |           | 10785     | 0.3369              |
|                                                                                | 7117      | 0.0817              |           | 8840      | 0.2904              |
|                                                                                | 5645      | 0.0689              |           | 7110      | 0.2456              |
|                                                                                | 4590      | 0.0543              |           | 5639      | 0.2026              |
|                                                                                | 3668      | 0.0350              |           | 4587      | 0.1654              |
|                                                                                | 2719      | 0.0356              |           | 3662      | 0.1404              |
|                                                                                | 1475      | 0.0206              |           | 2716      | 0.1041              |
|                                                                                | 402       | 0.0079              |           | 1478      | 0.0567              |
|                                                                                |           |                     |           | 402       | 0.0195              |
| 61.90                                                                          | 12643     | 0.1860              |           |           |                     |
|                                                                                |           |                     | 11.27     | 12630     | 0.5493              |
| 35.08                                                                          | 12638     | 0.3029              |           | 10777     | 0.5044              |
|                                                                                | 10774     | 0.2696              |           | 8833      | 0.4522              |
|                                                                                | 8838      | 0.2294              |           | 7103      | 0.3988              |
|                                                                                | 7108      | 0.1907              |           | 5633      | 0.3438              |



Table 14. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 11.27     | 4578      | 0.2987              | 4.2       | 8831      | 0.5558              |
|           | 3657      | 0.2561              |           | 7104      | 0.4964              |
|           | 2711      | 0.2048              |           | 5635      | 0.4364              |
|           | 1473      | 0.1246              |           | 4582      | 0.3905              |
|           | 401       | 0.0457              |           | 3657      | 0.3417              |
|           |           |                     |           | 2711      | 0.2824              |
| 6.61      | 12643     | 0.6231              |           | 1476      | 0.1782              |
|           | 10783     | 0.5820              |           | 400       | 0.0616              |
|           | 8834      | 0.5283              |           |           |                     |
|           | 7094      | 0.4737              | 1.4       | 12645     | 0.6743              |
|           | 5635      | 0.4176              |           | 10771     | 0.6289              |
|           | 4582      | 0.3703              |           | 8831      | 0.5095              |
|           | 3658      | 0.3268              |           | 7099      | 0.5096              |
|           | 2710      | 0.2684              |           | 5629      | 0.4499              |
|           | 1475      | 0.1740              |           | 4579      | 0.4010              |
|           | 379       | 0.0615              |           | 3656      | 0.3520              |
|           |           |                     |           | 2710      | 0.2856              |
| 4.2       | 12643     | 0.6537              |           | 1475      | 0.1869              |
|           | 10782     | 0.6085              |           | 400       | 0.0822              |

(b) Specimen cooled in a field of  
1000 Oe. See Figure 29.

|       |      |        |      |      |        |
|-------|------|--------|------|------|--------|
| 15.27 | 1000 | 0.0552 | 6.50 | 1000 | 0.1155 |
| 12.81 | 1000 | 0.0669 | 5.67 | 1000 | 0.1252 |
| 11.09 | 1000 | 0.0762 | 4.80 | 1000 | 0.1287 |
| 10.05 | 1000 | 0.0815 | 4.23 | 1000 | 0.1306 |
| 7.71  | 1000 | 0.1025 | 4.20 | 1000 | 0.1276 |
| 7.19  | 1000 | 0.1078 | 3.80 | 1000 | 0.1284 |



Table 14. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 3.50      | 1000      | 0.1266              | 1.71      | 1000      | 0.1217              |
| 2.93      | 1000      | 0.1272              | 1.63      | 1000      | 0.1218              |
| 2.63      | 1000      | 0.1238              | 1.52      | 1000      | 0.1159              |
| 2.28      | 1000      | 0.1232              | 1.35      | 1000      | 0.1182              |
| 1.86      | 1000      | 0.1238              |           |           |                     |

(c) Specimen cooled in zero field.  
See Figure 29.

|      |      |        |       |      |        |
|------|------|--------|-------|------|--------|
| 1.40 | 1000 | 0.0965 | 4.23  | 1000 | 0.1296 |
| 1.48 | 1000 | 0.1042 | 4.49  | 1000 | 0.1296 |
| 1.59 | 1000 | 0.1085 | 4.98  | 1000 | 0.1286 |
| 1.72 | 1000 | 0.1105 | 5.59  | 1000 | 0.1257 |
| 1.85 | 1000 | 0.1136 | 6.61  | 1000 | 0.1140 |
| 2.05 | 1000 | 0.1202 | 8.58  | 1000 | 0.0932 |
| 2.17 | 1000 | 0.1233 | 10.92 | 1000 | 0.0771 |
| 2.47 | 1000 | 0.1242 | 14.11 | 1000 | 0.0628 |
| 2.84 | 1000 | 0.1251 | 16.69 | 1000 | 0.0545 |
| 2.99 | 1000 | 0.1254 | 24.86 | 1000 | 0.0405 |
| 3.13 | 1000 | 0.1254 | 35.84 | 1000 | 0.0243 |
| 3.33 | 1000 | 0.1271 | 39.81 | 1000 | 0.0236 |
| 3.64 | 1000 | 0.1259 | 48.05 | 1000 | 0.0200 |
| 3.90 | 1000 | 0.1290 | 55.02 | 1000 | 0.0162 |
| 4.20 | 1000 | 0.1296 |       |      |        |

(d) Low-field data for remanence-  
temperature determination. See  
Figure 23.

|     |     |        |     |     |        |
|-----|-----|--------|-----|-----|--------|
| 4.2 | 388 | 0.0539 | 4.2 | 322 | 0.0466 |
|     | 355 | 0.0497 |     | 290 | 0.0418 |



Table 14. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 4.2       | 258       | 0.0381              | 1.43      | 322       | 0.0738              |
|           | 226       | 0.0335              |           | 290       | 0.0742              |
|           | 194       | 0.0283              |           | 258       | 0.0730              |
|           | 161       | 0.0231              |           | 226       | 0.0724              |
|           | 129       | 0.0184              |           | 194       | 0.0683              |
|           | 97        | 0.0160              |           | 161       | 0.0626              |
|           | 65        | 0.0144              |           | 129       | 0.0613              |
|           | 48        | 0.0107              |           | 97        | 0.0635              |
|           | 32        | 0.0096              |           | 65        | 0.0598              |
|           | 16        | 0.0064              |           | 48        | 0.0603              |
| 1.43      | 381       | 0.0739              |           | 32        | 0.0614              |
|           | 355       | 0.0738              |           | 16        | 0.0582              |



Table 15. Magnetization data for quenched  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$ . The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. The data are listed in the order in which they were taken.

| T<br>(°K)                                                                   | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------------------------------------------------------------------------|-----------|---------------------|-----------|-----------|---------------------|
| (a) Specimen cooled in an applied field of $\sim 12.65$ kOe. See Figure 27. |           |                     |           |           |                     |
| 300.63                                                                      | 12625     | 0.0492              | 32.90     | 12560     | 0.5969              |
| 242.91                                                                      | 12599     | 0.0659              |           | 11460     | 0.5546              |
| 217.74                                                                      | 12583     | 0.0757              |           | 9648      | 0.4821              |
| 189.72                                                                      | 12577     | 0.0907              |           | 7773      | 0.4001              |
| 159.62                                                                      | 12575     | 0.1123              |           | 6179      | 0.3258              |
| 134.23                                                                      | 12567     | 0.1387              |           | 5029      | 0.2695              |
| 104.09                                                                      | 12565     | 0.1862              |           | 4019      | 0.2179              |
|                                                                             |           |                     |           | 3229      | 0.1763              |
| 69.46                                                                       | 12559     | 0.2900              |           | 2019      | 0.1010              |
|                                                                             | 11539     | 0.2679              |           | 1742      | 0.0952              |
|                                                                             | 9733      | 0.2289              |           | 1424      | 0.0791              |
|                                                                             | 7867      | 0.1865              |           | 1214      | 0.0675              |
|                                                                             | 6243      | 0.1485              |           | 1092      | 0.0605              |
|                                                                             | 5082      | 0.1208              |           | 956       | 0.0532              |
|                                                                             | 4065      | 0.0966              |           | 215       | 0.0146              |
|                                                                             | 3303      | 0.0785              |           |           |                     |
|                                                                             | 2101      | 0.0504              | 23.81     | 12543     | 0.7600              |
|                                                                             | 1591      | 0.0378              |           | 11538     | 0.7179              |
|                                                                             | 1238      | 0.0296              |           | 9729      | 0.6289              |
|                                                                             | 1068      | 0.0257              |           | 7862      | 0.5290              |
|                                                                             | 954       | 0.0228              |           | 6239      | 0.4392              |
|                                                                             | 213       | 0.0048              |           | 5077      | 0.3658              |
|                                                                             |           |                     |           | 4055      | 0.2994              |
| 56.23                                                                       | 12553     | 0.3620              |           | 3295      | 0.2468              |
| 42.43                                                                       | 12548     | 0.4826              |           | 2099      | 0.1598              |



Table 15. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 23.81     | 1747      | 0.1316              | 12.14     | 4053      | 0.5265              |
|           | 1491      | 0.1143              |           | 3292      | 0.4470              |
|           | 1273      | 0.0983              |           | 2098      | 0.3089              |
|           | 1065      | 0.0828              |           | 1710      | 0.2586              |
|           | 242       | 0.0169              |           | 1489      | 0.2306              |
|           | 211       | 0.0162              |           | 1287      | 0.2002              |
| 16.69     |           |                     |           | 1114      | 0.1725              |
|           | 12540     | 0.9449              |           | 952       | 0.1459              |
|           | 11524     | 0.8967              |           | 213       | 0.0298              |
|           | 9716      | 0.8000              | 7.57      | 9721      | 1.0682              |
|           | 7861      | 0.6905              |           | 7851      | 0.9527              |
|           | 6236      | 0.5835              |           | 6205      | 0.8392              |
|           | 5075      | 0.4982              |           | 5077      | 0.7373              |
|           | 4054      | 0.4117              |           | 4055      | 0.6376              |
|           | 3291      | 0.3475              |           | 3296      | 0.5524              |
|           | 2098      | 0.2278              |           | 2099      | 0.3979              |
|           | 1826      | 0.2013              |           | 1707      | 0.3396              |
|           | 1588      | 0.1767              |           | 1491      | 0.3070              |
|           | 1336      | 0.1509              |           | 1281      | 0.2682              |
|           | 1159      | 0.1332              |           | 1145      | 0.2452              |
|           | 1034      | 0.1202              |           | 1022      | 0.2502              |
|           | 953       | 0.1114              |           | 949       | 0.2093              |
|           | 213       | 0.0298              |           | 202       | 0.0564              |
| 12.14     | 11431     | 1.0336              | 5.44      | 9723      | 1.1089              |
|           | 9690      | 0.9431              |           | 7875      | 0.9842              |
|           | 7851      | 0.8279              |           | 6238      | 0.8674              |
|           | 6235      | 0.7128              |           | 5059      | 0.7670              |
|           | 5075      | 0.6189              |           |           |                     |



Table 15. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 5.44      | 3292      | 0.5823              | 4.2       | 6237      | 0.8830              |
|           | 2090      | 0.4218              |           | 5081      | 0.7826              |
|           | 1778      | 0.3732              |           | 4055      | 0.6768              |
|           | 1571      | 0.3385              |           | 3297      | 0.5910              |
|           | 1411      | 0.3128              |           | 2099      | 0.4293              |
|           | 1240      | 0.2808              |           | 1752      | 0.3712              |
|           | 1112      | 0.2591              |           | 1510      | 0.3282              |
|           | 949       | 0.2268              |           | 1335      | 0.2983              |
|           | 211       | 0.0492              |           | 1206      | 0.2737              |
|           |           |                     |           | 1083      | 0.2454              |
| 4.2       | 9724      | 1.1279              |           | 953       | 0.2250              |
|           | 7861      | 1.0071              |           | 214       | 0.0453              |

(b) Specimen cooled in a field of  $\sim 700$  Oe.  
See Figure 30.

|      |     |        |      |     |        |
|------|-----|--------|------|-----|--------|
| 4.2  | 700 | 0.1732 | 2.12 | 700 | 0.1658 |
| 3.68 | 700 | 0.1709 | 1.98 | 700 | 0.1614 |
| 3.34 | 700 | 0.1691 | 1.82 | 700 | 0.1642 |
| 2.61 | 700 | 0.1741 | 1.68 | 700 | 0.1573 |
| 2.20 | 700 | 0.1712 | 1.61 | 700 | 0.1648 |
| 2.17 | 700 | 0.1734 | 1.45 | 700 | 0.1590 |

(c) Specimen cooled in zero field. See  
Figure 30.

|      |     |        |      |     |        |
|------|-----|--------|------|-----|--------|
| 1.45 | 700 | 0.1271 | 1.65 | 700 | 0.1408 |
| 1.57 | 700 | 0.1484 | 1.70 | 700 | 0.1397 |
| 1.61 | 700 | 0.1456 | 1.78 | 700 | 0.1441 |



Table 15. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 1.85      | 700       | 0.1510              | 3.35      | 700       | 0.1557              |
| 2.03      | 700       | 0.1550              | 3.57      | 700       | 0.1574              |
| 2.13      | 700       | 0.1513              | 3.64      | 700       | 0.1539              |
| 2.46      | 700       | 0.1539              | 3.72      | 700       | 0.1554              |
| 2.72      | 700       | 0.1550              | 3.84      | 700       | 0.1656              |
| 3.04      | 700       | 0.1528              | 4.00      | 700       | 0.1626              |
| 3.15      | 700       | 0.1554              | 4.2       | 700       | 0.1640              |

(d) Low-field data for remanence-  
temperature determination. See  
Figure 24.

|     |     |        |      |     |        |
|-----|-----|--------|------|-----|--------|
| 4.2 | 643 | 0.1599 | 2.12 | 644 | 0.1579 |
|     | 579 | 0.1464 |      | 580 | 0.1504 |
|     | 515 | 0.1344 |      | 516 | 0.1375 |
|     | 451 | 0.1184 |      | 451 | 0.1230 |
|     | 419 | 0.1095 |      | 419 | 0.1119 |
|     | 387 | 0.1022 |      | 387 | 0.1075 |
|     | 355 | 0.0969 |      | 355 | 0.1003 |
|     | 322 | 0.0922 |      | 323 | 0.0949 |
|     | 290 | 0.0842 |      | 290 | 0.0888 |
|     | 258 | 0.0765 |      | 258 | 0.0835 |
|     | 226 | 0.0701 |      | 226 | 0.0788 |
|     | 194 | 0.0592 |      | 194 | 0.0740 |
|     | 161 | 0.0523 |      | 161 | 0.0654 |
|     | 129 | 0.0444 |      | 129 | 0.0596 |
|     | 97  | 0.0374 |      | 97  | 0.0561 |
|     | 65  | 0.0304 |      | 65  | 0.0515 |
|     | 32  | 0.0187 |      | 32  | 0.0468 |



Table 15. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 1.61      | 644       | 0.1657              | 1.61      | 258       | 0.0947              |
|           | 580       | 0.1606              |           | 226       | 0.0948              |
|           | 515       | 0.1549              |           | 194       | 0.0834              |
|           | 451       | 0.1462              |           | 161       | 0.0739              |
|           | 419       | 0.1329              |           | 129       | 0.0725              |
|           | 287       | 0.1287              |           | 97        | 0.0624              |
|           | 355       | 0.1208              |           | 65        | 0.0585              |
|           | 323       | 0.1109              |           | 32        | 0.0422              |
|           | 290       | 0.1024              |           |           |                     |



Table 16. Magnetization data for quenched  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$ . The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. The data are listed in the order in which they were taken.

| T<br>(°K)                                                                      | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|--------------------------------------------------------------------------------|-----------|---------------------|-----------|-----------|---------------------|
| (a) Specimen cooled in an applied field<br>of $\sim 12.55$ kOe. See Figure 28. |           |                     |           |           |                     |
| 297.86                                                                         | 12575     | 0.0494              | 42.50     | 8871      | 0.3923              |
| 266.93                                                                         | 12561     | 0.0562              |           | 7131      | 0.3195              |
| 245.76                                                                         | 12560     | 0.0631              |           | 5656      | 0.2545              |
| 216.38                                                                         | 12556     | 0.0741              |           | 4608      | 0.2091              |
| 191.24                                                                         | 12553     | 0.0863              |           | 3679      | 0.1678              |
| 163.64                                                                         | 12553     | 0.1049              |           | 2738      | 0.1249              |
| 131.10                                                                         | 12555     | 0.1382              |           | 1491      | 0.0683              |
| 102.65                                                                         | 12552     | 0.1873              |           | 412       | 0.0180              |
|                                                                                |           |                     |           | 273       | 0.0113              |
|                                                                                |           |                     |           | 212       | 0.0088              |
| 70.06                                                                          | 12548     | 0.2979              |           |           |                     |
|                                                                                | 10804     | 0.2582              |           |           |                     |
|                                                                                | 8874      | 0.2134              | 33.37     | 12541     | 0.6864              |
|                                                                                | 7133      | 0.1722              |           |           |                     |
|                                                                                | 5657      | 0.1370              | 24.28     | 12540     | 0.9082              |
|                                                                                | 4607      | 0.1115              |           | 10795     | 0.8106              |
|                                                                                | 3684      | 0.0897              |           | 8872      | 0.6927              |
|                                                                                | 2739      | 0.0676              |           | 7129      | 0.5773              |
|                                                                                | 1490      | 0.0363              |           | 5655      | 0.4668              |
|                                                                                | 412       | 0.0095              |           | 4604      | 0.3852              |
|                                                                                | 273       | 0.0067              |           | 3679      | 0.3115              |
|                                                                                | 213       | 0.0035              |           | 2734      | 0.2347              |
|                                                                                |           |                     |           | 1490      | 0.1230              |
| 56.39                                                                          | 12541     | 0.3853              |           | 412       | 0.0355              |
|                                                                                |           |                     |           | 273       | 0.0236              |
| 42.50                                                                          | 12541     | 0.5373              |           | 212       | 0.0175              |
|                                                                                | 10780     | 0.4706              |           |           |                     |



Table 16. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 15.70     | 10067     | 1.0785              | 7.99      | 1497      | 0.3838              |
|           | 8829      | 0.9919              |           | 1276      | 0.3353              |
|           | 7134      | 0.8545              |           | 1163      | 0.3082              |
|           | 5657      | 0.7139              |           | 1053      | 0.2855              |
|           | 2611      | 0.6082              |           | 957       | 0.2591              |
|           | 3682      | 0.4991              |           | 215       | 0.0466              |
|           | 2735      | 0.3836              |           | 60        | 0.0045              |
|           | 1492      | 0.2162              | 5.59      | 8126      | 1.3725              |
|           | 412       | 0.0599              |           | 7139      | 1.2819              |
|           | 272       | 0.0408              |           | 5658      | 1.1235              |
| 10.92     | 56        | 0.0123              |           | 4598      | 0.9959              |
|           | 8821      | 1.2110              |           | 3682      | 0.8691              |
|           | 7138      | 1.0673              |           | 2736      | 0.7149              |
|           | 5657      | 0.9124              |           | 1490      | 0.4626              |
|           | 4605      | 0.7934              |           | 412       | 0.1594              |
|           | 3680      | 0.6740              |           | 315       | 0.1110              |
|           | 2735      | 0.5334              |           | 258       | 0.0975              |
|           | 2334      | 0.4620              |           | 213       | 0.0853              |
|           | 2040      | 0.4132              |           | 56        | 0.0248              |
|           | 998       | 0.2124              | 4.2       | 8080      | 1.4131              |
|           | 941       | 0.2023              |           | 7145      | 1.3265              |
|           | 209       | 0.0346              |           | 5662      | 1.1673              |
| 7.99      | 8896      | 1.3291              |           | 4612      | 1.0364              |
|           | 7151      | 1.1763              |           | 3688      | 0.9015              |
|           | 5670      | 1.0235              |           | 2742      | 0.7420              |
|           | 4617      | 0.8985              |           | 1496      | 0.4778              |
|           | 3687      | 0.7725              |           | 1276      | 0.4174              |
|           | 2745      | 0.5234              |           | 1115      | 0.3798              |



Table 16. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 4.2       | 958       | 0.3295              | 4.2       | 55        | 0.0253              |
|           | 216       | 0.0676              |           |           |                     |

(b) Specimen cooled in a field of  
~1000 Oe. See Figure 31.

|        |      |        |      |      |        |
|--------|------|--------|------|------|--------|
| 303.20 | 1000 | 0.0049 | 5.44 | 1000 | 0.3344 |
| 241.79 | 1000 | 0.0046 | 4.92 | 1000 | 0.3463 |
| 189.31 | 1000 | 0.0064 | 4.2  | 1000 | 0.3526 |
| 136.47 | 1000 | 0.0099 | 4.2  | 1000 | 0.3469 |
| 71.88  | 1000 | 0.0193 | 3.74 | 1000 | 0.3563 |
| 60.16  | 1000 | 0.0269 | 3.15 | 1000 | 0.3555 |
| 43.61  | 1000 | 0.0413 | 2.28 | 1000 | 0.3501 |
| 34.98  | 1000 | 0.0536 | 2.11 | 1000 | 0.3524 |
| 26.47  | 1000 | 0.0736 | 1.89 | 1000 | 0.3428 |
| 19.80  | 1000 | 0.1043 | 1.72 | 1000 | 0.3439 |
| 13.14  | 1000 | 0.1645 | 1.64 | 1000 | 0.3485 |
| 8.73   | 1000 | 0.2485 | 1.61 | 1000 | 0.3526 |
| 7.31   | 1000 | 0.2783 | 1.45 | 1000 | 0.3432 |
| 6.50   | 1000 | 0.3031 |      |      |        |

(c) Specimen cooled in zero field.  
See Figure 31.

|      |      |        |      |      |        |
|------|------|--------|------|------|--------|
| 1.50 | 1000 | 0.3438 | 2.00 | 1000 | 0.3522 |
| 1.60 | 1000 | 0.3408 | 2.09 | 1000 | 0.3512 |
| 1.64 | 1000 | 0.3457 | 2.53 | 1000 | 0.3500 |
| 1.67 | 1000 | 0.3480 | 2.75 | 1000 | 0.3470 |
| 1.76 | 1000 | 0.3463 | 3.01 | 1000 | 0.3539 |
| 1.81 | 1000 | 0.3481 | 3.16 | 1000 | 0.3492 |
| 1.86 | 1000 | 0.3490 | 3.34 | 1000 | 0.3506 |



Table 16. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 3.42      | 1000      | 0.3486              | 7.19      | 1000      | 0.2962              |
| 3.58      | 1000      | 0.3494              | 8.43      | 1000      | 0.2613              |
| 3.70      | 1000      | 0.3470              | 9.54      | 1000      | 0.2334              |
| 3.80      | 1000      | 0.3553              | 10.92     | 1000      | 0.2062              |
| 3.95      | 1000      | 0.3478              | 12.14     | 1000      | 0.1864              |
| 4.10      | 1000      | 0.3493              | 14.84     | 1000      | 0.1493              |
| 4.2       | 1000      | 0.3484              | 19.80     | 1000      | 0.1102              |
| 4.2       | 1000      | 0.3573              | 23.68     | 1000      | 0.0866              |
| 4.08      | 1000      | 0.3531              | 26.47     | 1000      | 0.0757              |
| 5.37      | 1000      | 0.3440              | 35.84     | 1000      | 0.0537              |
| 6.20      | 1000      | 0.3245              |           |           |                     |

(d) Low-field data for remanence-temperature determination. See Figure 25.

|     |     |        |      |     |        |
|-----|-----|--------|------|-----|--------|
| 4.2 | 451 | 0.1742 | 4.2  | 43  | 0.0357 |
|     | 421 | 0.1691 |      | 31  | 0.0245 |
|     | 390 | 0.1610 |      |     |        |
|     | 355 | 0.1488 | 2.42 | 451 | 0.1694 |
|     | 322 | 0.1369 |      | 419 | 0.1627 |
|     | 291 | 0.1245 |      | 388 | 0.1554 |
|     | 259 | 0.1139 |      | 358 | 0.1244 |
|     | 226 | 0.0979 |      | 322 | 0.1330 |
|     | 195 | 0.0884 |      | 291 | 0.1241 |
|     | 162 | 0.0731 |      | 259 | 0.1170 |
|     | 129 | 0.0641 |      | 227 | 0.1081 |
|     | 109 | 0.0590 |      | 196 | 0.0972 |
|     | 97  | 0.0508 |      | 164 | 0.0797 |
|     | 81  | 0.0457 |      | 130 | 0.0672 |
|     | 65  | 0.0405 |      | 97  | 0.0538 |



Table 16. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>(emu/g) |
|-----------|-----------|---------------------|-----------|-----------|---------------------|
| 2.42      | 65        | 0.0447              | 1.57      | 227       | 0.0965              |
|           | 46        | 0.0335              |           | 196       | 0.0884              |
|           | 29        | 0.0212              |           | 164       | 0.0807              |
|           |           |                     |           | 130       | 0.0721              |
| 1.57      | 451       | 0.1570              |           | 97        | 0.0602              |
|           | 420       | 0.1485              |           | 65        | 0.0496              |
|           | 388       | 0.1418              |           | 42        | 0.0401              |
|           | 356       | 0.1329              |           | 26        | 0.0298              |
|           | 290       | 0.1127              |           |           |                     |



Table 17. Magnetization data for 108 ppm Fe in Cu. These values were read off from  $\sigma$  vs. H plots at various temperatures supplied to us by Dr. J. L. Tholence and Dr. R. Tournier (Reference 6). See Figure 32.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 1.3       | 10000     | 1.242                          | 10        | 40000     | 3.175                          |
|           | 20000     | 2.354                          |           | 50000     | 3.866                          |
|           | 30000     | 3.369                          |           | 60000     | 4.579                          |
|           | 40000     | 4.352                          | 20        | 10000     | 0.616                          |
|           | 50000     | 5.238                          |           | 20000     | 1.242                          |
|           | 60000     | 6.026                          |           | 30000     | 1.857                          |
| 4.2       | 10000     | 1.058                          |           | 40000     | 2.430                          |
|           | 20000     | 2.095                          |           | 50000     | 2.948                          |
|           | 30000     | 3.067                          |           | 60000     | 3.488                          |
|           | 40000     | 3.942                          | 32.5      | 10000     | 0.497                          |
|           | 50000     | 4.827                          |           | 20000     | 0.983                          |
|           | 60000     | 5.616                          |           | 30000     | 1.470                          |
| 10        | 10000     | 8.210                          |           | 40000     | 1.944                          |
|           | 20000     | 1.631                          |           | 50000     | 2.354                          |
|           | 30000     | 2.430                          |           | 60000     | 2.786                          |



Table 18. Magnetization data for 112 ppm Fe in Cu. These data were supplied to us by Dr. E. C. Hirschkoﬀ and Prof. J. C. Wheatley. (Reference 9)  
See Figures 33 and 34.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 0.0126    | 0.977     | 0.2644                         | 0.0135    | 0.977     | 0.2484                         |
| 0.0206    | 0.977     | 0.1836                         | 0.0116    | 0.977     | 0.2731                         |
| 0.0346    | 0.977     | 0.1326                         | 0.0092    | 0.977     | 0.3147                         |
| 0.0935    | 0.977     | 0.0679                         |           |           |                                |
| 0.1131    | 0.977     | 0.0590                         | 0.0123    | 10.000    | 2.7056                         |
| 0.0516    | 0.977     | 0.1012                         | 0.0291    | 10.000    | 1.5409                         |
| 0.1715    | 0.977     | 0.0437                         | 0.0194    | 10.000    | 2.0149                         |
| 0.1285    | 0.977     | 0.0555                         | 0.0360    | 10.000    | 1.3299                         |
| 0.0253    | 0.977     | 0.1663                         | 0.1000    | 10.000    | 0.6732                         |
| 0.0170    | 0.977     | 0.2159                         | 0.1795    | 10.000    | 0.4558                         |
| 0.0135    | 0.977     | 0.2513                         | 0.1451    | 10.000    | 0.5268                         |
| 0.0796    | 0.977     | 0.0765                         | 0.2967    | 10.000    | 0.3097                         |
| 0.2092    | 0.977     | 0.0410                         | 0.4065    | 10.000    | 0.2445                         |
| 0.3521    | 0.977     | 0.0278                         | 0.2118    | 10.000    | 0.3810                         |
| 0.4098    | 0.977     | 0.0243                         | 0.1187    | 10.000    | 0.5897                         |
| 0.2404    | 0.977     | 0.0373                         | 0.0792    | 10.000    | 0.7704                         |
| 0.1053    | 0.977     | 0.0633                         | 0.0247    | 10.000    | 1.7277                         |
| 0.1524    | 0.977     | 0.0495                         | 0.0148    | 10.000    | 2.3938                         |
| 0.0876    | 0.977     | 0.0713                         | 0.0411    | 10.000    | 1.2185                         |
| 0.0705    | 0.977     | 0.0824                         | 0.0134    | 10.000    | 2.5274                         |
| 0.0603    | 0.977     | 0.0909                         | 0.0633    | 10.000    | 0.9096                         |
| 0.0443    | 0.977     | 0.1119                         | 0.1314    | 10.000    | 0.5656                         |
| 0.0297    | 0.977     | 0.1476                         | 0.2421    | 10.000    | 0.3821                         |
| 0.0394    | 0.977     | 0.1216                         | 0.0904    | 10.000    | 0.7223                         |
| 0.0519    | 0.977     | 0.1027                         | 0.0216    | 10.000    | 1.8693                         |
| 0.0189    | 0.977     | 0.2004                         | 0.0501    | 10.000    | 1.0672                         |
| 0.0148    | 0.977     | 0.2337                         | 0.0710    | 10.000    | 0.8470                         |



Table 18. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 0.1092    | 10.000    | 0.6351                         | 0.0288    | 60.830    | 8.5894                         |
| 0.3401    | 10.000    | 0.3075                         | 0.0222    | 60.830    | 9.7470                         |
| 0.1608    | 10.000    | 0.4907                         | 0.0141    | 60.830    | 11.5402                        |
| 0.0819    | 10.000    | 0.7679                         | 0.0115    | 60.830    | 12.2083                        |
| 0.0579    | 10.000    | 0.9755                         | 0.0096    | 60.830    | 12.6934                        |
| 0.0174    | 10.000    | 2.1634                         |           |           |                                |
| 0.0115    | 10.000    | 2.7699                         | 0.0124    | 96.380    | 15.3762                        |
|           |           |                                | 0.0263    | 96.380    | 12.5616                        |
| 0.0192    | 60.830    | 10.4108                        | 0.0933    | 96.380    | 6.7219                         |
| 0.0166    | 60.830    | 10.9108                        | 0.1497    | 96.380    | 5.0696                         |
| 0.0383    | 60.830    | 7.4624                         | 0.0413    | 96.380    | 10.6342                        |
| 0.0606    | 60.830    | 5.6736                         | 0.0211    | 96.380    | 13.6435                        |
| 0.1049    | 60.830    | 3.9735                         | 0.0344    | 96.380    | 11.4576                        |
| 0.1309    | 60.830    | 3.4251                         | 0.0171    | 96.380    | 14.2972                        |
| 0.1587    | 60.830    | 3.0402                         | 0.0148    | 96.380    | 14.7061                        |
| 0.1912    | 60.830    | 2.6620                         | 0.0189    | 96.380    | 13.8442                        |
| 0.2512    | 60.830    | 2.2220                         | 0.0594    | 96.380    | 8.6292                         |
| 0.3030    | 60.830    | 1.9143                         | 0.0298    | 96.380    | 12.0305                        |
| 0.3937    | 60.830    | 1.6391                         | 0.1453    | 96.380    | 4.9850                         |
| 0.2174    | 60.830    | 2.4190                         | 0.2695    | 96.380    | 3.2640                         |
| 0.3436    | 60.830    | 1.7772                         | 0.3086    | 96.380    | 3.0416                         |
| 0.1132    | 60.830    | 3.7458                         | 0.3472    | 96.380    | 2.8225                         |
| 0.0124    | 60.830    | 12.0478                        | 0.0788    | 96.380    | 7.4572                         |
| 0.0257    | 60.830    | 9.1028                         | 0.1130    | 96.380    | 5.9324                         |
| 0.0333    | 60.830    | 7.9826                         | 0.1842    | 96.380    | 4.3253                         |
| 0.0436    | 60.830    | 6.8734                         | 0.2247    | 96.380    | 3.7946                         |
| 0.0508    | 60.830    | 6.2786                         | 0.1326    | 96.380    | 5.3898                         |
| 0.0866    | 60.830    | 4.4797                         | 0.1026    | 96.380    | 6.3111                         |
| 0.0711    | 60.830    | 5.1047                         | 0.0915    | 96.380    | 6.7924                         |



Table 18. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 0.0711    | 96.380    | 7.9135                         | 0.0132    | 217.110   | 26.9653                        |
| 0.0519    | 96.380    | 9.4417                         | 0.0198    | 217.110   | 25.1694                        |
| 0.0240    | 96.380    | 13.0452                        | 0.0391    | 217.110   | 21.0806                        |
| 0.0135    | 96.380    | 15.0311                        | 0.1085    | 217.110   | 13.1701                        |
| 0.0117    | 96.380    | 15.4190                        | 0.2584    | 217.110   | 7.7274                         |
|           |           |                                | 0.1567    | 217.110   | 10.7818                        |
| 0.0133    | 160.200   | 21.5650                        | 0.0680    | 217.110   | 17.0691                        |
| 0.0196    | 160.200   | 19.9037                        | 0.1916    | 217.110   | 9.4598                         |
| 0.0278    | 160.200   | 18.0702                        | 0.2392    | 217.110   | 8.1838                         |
| 0.0394    | 160.200   | 16.0681                        | 0.3174    | 217.110   | 6.7300                         |
| 0.0621    | 160.200   | 13.1921                        | 0.4424    | 217.110   | 5.2412                         |
| 0.0828    | 160.200   | 11.4262                        | 0.3831    | 217.110   | 5.9578                         |
| 0.1073    | 160.200   | 9.7970                         | 0.0830    | 217.110   | 15.4190                        |
| 0.1316    | 160.200   | 8.7678                         | 0.1381    | 217.110   | 11.5785                        |
| 0.1543    | 160.200   | 7.9118                         | 0.2207    | 217.110   | 8.6325                         |
| 0.1658    | 160.200   | 7.6572                         | 0.1745    | 217.110   | 10.0580                        |
| 0.2169    | 160.200   | 6.4306                         | 0.0526    | 217.110   | 19.1162                        |
| 0.3164    | 160.200   | 4.9955                         | 0.0296    | 217.110   | 23.1899                        |
| 0.4048    | 160.200   | 4.2175                         | 0.0148    | 217.110   | 26.4578                        |
| 0.1174    | 160.200   | 9.4418                         | 0.0239    | 217.110   | 24.0937                        |
| 0.1828    | 160.200   | 7.2019                         | 0.0344    | 217.110   | 21.9296                        |
| 0.2532    | 160.200   | 5.7883                         | 0.0118    | 217.110   | 27.1538                        |
| 0.0512    | 160.200   | 14.6311                        | 0.0095    | 217.110   | 27.7238                        |
| 0.0166    | 160.200   | 20.7914                        |           |           |                                |
| 0.0126    | 160.200   | 21.7845                        |           |           |                                |
| 0.0094    | 160.200   | 22.4364                        |           |           |                                |



Table 19. Magnetization data for 478 ppm Fe in Cu. These data were supplied to us by Dr. E. C. Hirschkoﬀ and Prof. J. C. Wheatley (Reference 9). See Figure 35.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-5}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 0.0145    | 10.000    | 12.6179                        | 0.2487    | 10.000    | 5.8180                         |
| 0.0197    | 10.000    | 12.5495                        | 0.3185    | 10.000    | 4.9416                         |
| 0.0377    | 10.000    | 12.2604                        | 0.4098    | 10.000    | 4.2110                         |
| 0.0632    | 10.000    | 11.5726                        | 0.2932    | 10.000    | 5.2708                         |
| 0.0111    | 10.000    | 9.6524                         | 0.2212    | 10.000    | 6.4294                         |
| 0.1595    | 10.000    | 7.8626                         | 0.3745    | 10.000    | 4.4124                         |
| 0.0808    | 10.000    | 10.9528                        | 0.2053    | 10.000    | 6.6182                         |
| 0.0229    | 10.000    | 12.5591                        | 0.1802    | 10.000    | 7.2198                         |
| 0.0298    | 10.000    | 12.4704                        | 0.1456    | 10.000    | 8.3170                         |
| 0.0131    | 10.000    | 12.5403                        | 0.0464    | 10.000    | 12.1152                        |
| 0.0164    | 10.000    | 12.5543                        | 0.0114    | 10.000    | 12.5200                        |
| 0.0964    | 10.000    | 10.3105                        | 0.0094    | 10.000    | 12.4793                        |
| 0.1330    | 10.000    | 8.8045                         | 0.0090    | 10.000    | 12.4517                        |



Table 20. Magnetization data for the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloy containing 100 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 36 and 37.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 299.44    | 12565     | 2.09                                  | 4.2       | 8866      | 6.20                                  |
| 244.22    | 12565     | 2.14                                  |           | 7137      | 4.93                                  |
| 190.55    | 12557     | 2.16                                  |           | 5661      | 4.03                                  |
| 132.24    | 12553     | 2.23                                  |           | 4600      | 3.30                                  |
| 102.56    | 12550     | 2.31                                  |           | 3682      | 2.38                                  |
| 78.08     | 12545     | 2.47                                  |           | 2737      | 1.65                                  |
| 63.23     | 12544     | 2.60                                  |           | 2690      | 1.71                                  |
| 42.96     | 12567     | 2.84                                  |           | 1453      | 1.10                                  |
| 39.44     | 12551     | 2.97                                  |           | 395       | 0.24                                  |
| 34.09     | 12556     | 3.13                                  |           |           |                                       |
| 28.21     | 12555     | 3.29                                  | 3.15      | 12597     | 10.52                                 |
| 21.6      | 12553     | 3.74                                  |           | 10828     | 9.07                                  |
| 14.80     | 12593     | 4.45                                  |           | 8862      | 7.59                                  |
| 9.80      | 12560     | 5.31                                  |           | 7149      | 6.13                                  |
|           |           |                                       |           | 5668      | 4.81                                  |
| 6.00      | 12566     | 6.94                                  |           | 4601      | 4.00                                  |
|           | 10676     | 5.89                                  |           | 3684      | 3.27                                  |
|           | 8720      | 4.80                                  |           | 2738      | 2.30                                  |
|           | 7009      | 3.78                                  |           | 412       | 0.38                                  |
|           | 5557      | 3.07                                  |           |           |                                       |
|           | 4610      | 2.40                                  | 2.42      | 12572     | 12.10                                 |
|           | 3685      | 1.84                                  |           | 10825     | 10.53                                 |
|           | 2690      | 1.47                                  |           | 8893      | 8.81                                  |
|           | 1454      | 1.00                                  |           | 7147      | 7.29                                  |
|           |           |                                       |           | 5666      | 5.81                                  |
| 4.2       | 12550     | 8.85                                  |           | 4617      | 4.89                                  |
|           | 10663     | 7.56                                  |           | 3685      | 4.09                                  |



Table 20. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 2.42      | 2740      | 2.58                           | 1.34      | 12572     | 15.40                          |
|           | 1491      | 1.49                           |           | 10826     | 14.10                          |
| 1.97      |           |                                |           | 8896      | 12.00                          |
|           | 12569     | 13.32                          |           | 7147      | 10.43                          |
|           | 10824     | 11.83                          |           | 5666      | 8.67                           |
|           | 8895      | 10.00                          |           | 4614      | 7.37                           |
|           | 7147      | 8.08                           |           | 3687      | 6.10                           |
|           | 5667      | 6.62                           |           | 2740      | 4.62                           |
|           | 4611      | 5.36                           |           | 1491      | 2.70                           |
|           | 3685      | 4.49                           |           |           |                                |
|           | 2738      | 2.89                           |           |           |                                |
|           | 411       | 0.45                           |           |           |                                |



Table 21. Magnetization data for the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloy containing 500 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 36 and 38.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 300.50    | 12568     | 0.278                                 | 4.2       | 12557     | 3.795                                 |
| 243.28    | 12564     | 0.291                                 |           | 10671     | 3.286                                 |
| 189.78    | 12555     | 0.315                                 |           | 8715      | 2.723                                 |
| 132.54    | 12546     | 0.360                                 |           | 7006      | 2.238                                 |
| 101.54    | 12545     | 0.407                                 |           | 5554      | 1.784                                 |
| 78.54     | 12545     | 0.476                                 |           | 4520      | 1.476                                 |
| 61.74     | 12543     | 0.544                                 |           | 3612      | 1.161                                 |
| 41.95     | 12542     | 0.711                                 |           | 2646      | 0.873                                 |
| 33.09     | 12547     | 0.830                                 |           | 1403      | 0.479                                 |
| 25.90     | 12547     | 0.986                                 |           | 366       | 0.185                                 |
| 18.34     | 12547     | 1.264                                 |           |           |                                       |
| 12.48     | 12520     | 1.741                                 | 3.34      | 12538     | 4.361                                 |
|           |           |                                       |           | 10657     | 3.784                                 |
| 7.77      | 12520     | 2.461                                 |           | 8715      | 3.186                                 |
|           | 10639     | 2.124                                 |           | 6996      | 2.597                                 |
|           | 8689      | 1.748                                 |           | 5546      | 2.093                                 |
|           | 6986      | 1.414                                 |           | 4513      | 1.690                                 |
|           | 5537      | 1.109                                 |           | 3606      | 1.355                                 |
|           | 4505      | 0.915                                 |           | 2650      | 1.013                                 |
|           | 3600      | 0.733                                 |           | 1402      | 0.533                                 |
|           | 2623      | 0.525                                 |           | 366       | 0.129                                 |
|           | 1401      | 0.319                                 |           |           |                                       |
|           | 368       | 0.089                                 | 2.05      | 12507     | 5.640                                 |
|           |           |                                       |           | 10655     | 5.010                                 |
| 5.59      | 12523     | 3.163                                 |           | 8702      | 4.295                                 |



Table 21. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 2.05      | 6995      | 3.602                          | 1.51      | 12542     | 6.275                          |
|           | 5546      | 2.945                          |           | 10655     | 5.661                          |
|           | 4515      | 2.428                          |           | 8680      | 4.911                          |
|           | 3598      | 1.968                          |           | 6998      | 4.201                          |
|           | 2642      | 1.438                          |           | 5547      | 3.494                          |
|           | 1403      | 0.783                          |           | 4507      | 2.927                          |
|           | 367       | 0.152                          |           | 3607      | 2.394                          |
|           |           |                                |           | 2639      | 1.817                          |
|           |           |                                |           | 1404      | 0.985                          |
|           |           |                                |           | 367       | 0.303                          |



Table 22. Magnetization data for the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloy containing 1000 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 36 and 39.

| T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|---------------------------|-----------|---------------------------------------|---------------------------|-----------|---------------------------------------|
| 301.34                    | 12569     | 0.377                                 | 9.71                      | 12564     | 4.121                                 |
| 243.93                    | 12563     | 0.406                                 |                           |           |                                       |
| 189.75                    | 12564     | 0.455                                 | 7.06                      | 12545     | 5.172                                 |
| 135.60                    | 12556     | 0.556                                 |                           | 10657     | 4.474                                 |
| 103.01                    | 12566     | 0.655                                 |                           | 8703      | 3.704                                 |
| 82.74                     | 12564     | 0.771                                 |                           | 6997      | 3.022                                 |
| 64.66                     | 12564     | 0.921                                 |                           | 5548      | 2.430                                 |
| 48.47                     | 12566     | 1.155                                 |                           | 4515      | 1.985                                 |
| 39.22                     | 12566     | 1.365                                 |                           | 3608      | 1.566                                 |
| 30.79                     | 12566     | 1.636                                 |                           | 2644      | 1.128                                 |
| 24.16                     | 12563     | 1.965                                 |                           | 1413      | 0.598                                 |
| 22.96                     | 12561     | 2.074                                 |                           | 373       | 0.121                                 |
| 19.93                     | 12559     | 2.288                                 |                           |           |                                       |
| 16.55                     | 12541     | 2.653                                 | 6.20                      | 12563     | 5.788                                 |
| 13.63                     | 12563     | 3.176                                 | 5.75                      | 12563     | 6.295                                 |
| 11.09                     | 12549     | 3.665                                 | 4.2                       | 12565     | 7.606                                 |
|                           | 10658     | 3.157                                 |                           | 10679     | 6.653                                 |
|                           | 8695      | 2.604                                 |                           | 8728      | 5.575                                 |
|                           | 6998      | 2.093                                 |                           | 7010      | 4.573                                 |
|                           | 5549      | 1.673                                 |                           | 5559      | 3.677                                 |
|                           | 4520      | 1.378                                 |                           | 4523      | 3.022                                 |
|                           | 3609      | 1.079                                 |                           | 3616      | 2.433                                 |
|                           | 2645      | 0.794                                 |                           | 2645      | 1.778                                 |
|                           | 1409      | 0.426                                 |                           | 1411      | 0.954                                 |
|                           | 375       | 0.274                                 |                           | 373       | 0.242                                 |



Table 22. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 3.28      | 12569     | 8.706                          | 2.02      | 4523      | 4.984                          |
|           | 10681     | 7.678                          |           | 3614      | 4.099                          |
|           | 8727      | 6.517                          |           | 2648      | 3.100                          |
|           | 7013      | 5.397                          |           | 1409      | 1.703                          |
|           | 5559      | 4.398                          |           | 369       | 0.440                          |
|           | 4523      | 3.630                          | 1.42      | 12563     | 11.582                         |
|           | 3615      | 2.925                          |           | 10666     | 10.538                         |
|           | 2650      | 2.149                          |           | 8687      | 9.263                          |
|           | 1409      | 1.134                          |           | 7000      | 8.033                          |
|           | 371       | 0.318                          |           | 5548      | 6.823                          |
| 2.02      | 12567     | 10.594                         |           | 4514      | 5.845                          |
|           | 10678     | 9.539                          |           | 3607      | 4.893                          |
|           | 8701      | 8.272                          |           | 2637      | 3.751                          |
|           | 7010      | 7.081                          |           | 1400      | 2.146                          |
|           | 5557      | 5.902                          |           | 362       | 0.524                          |



Table 23. Magnetization data for the quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 100 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 40 and 41.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 299.09    | 12688     | 6.50                                  | 4.2       | 8840      | 13.43                                 |
| 244.22    | 12687     | 6.53                                  |           | 7109      | 10.67                                 |
| 188.87    | 12677     | 6.56                                  |           | 5637      | 8.28                                  |
| 124.15    | 12670     | 6.66                                  |           | 4586      | 6.95                                  |
| 98.80     | 12668     | 6.91                                  |           | 3664      | 5.88                                  |
| 74.75     | 12666     | 6.96                                  |           | 2715      | 4.06                                  |
| 59.67     | 12662     | 7.14                                  |           | 1463      | 2.25                                  |
| 43.67     | 12660     | 7.25                                  |           |           |                                       |
| 31.38     | 12650     | 8.04                                  | 2.84      | 12602     | 22.40                                 |
| 27.89     | 12650     | 8.28                                  |           | 10616     | 19.56                                 |
|           |           |                                       |           | 8683      | 16.49                                 |
| 20.20     | 12649     | 8.89                                  |           | 7017      | 13.55                                 |
|           |           |                                       |           | 5538      | 10.90                                 |
| 9.70      | 12649     | 11.72                                 |           | 4519      | 8.71                                  |
|           | 10784     | 10.13                                 |           | 3586      | 7.10                                  |
|           | 8839      | 8.48                                  |           | 2600      | 5.01                                  |
|           | 7109      | 6.55                                  |           | 1406      | 2.75                                  |
|           | 5636      | 5.12                                  |           |           |                                       |
|           | 4586      | 3.87                                  | 1.58      | 12606     | 25.54                                 |
|           | 3664      | 2.92                                  |           | 10625     | 22.81                                 |
|           | 2614      | 2.45                                  |           | 8739      | 20.01                                 |
|           | 1417      | 1.77                                  |           | 6983      | 16.72                                 |
|           |           |                                       |           | 5568      | 13.90                                 |
| 6.50      | 12650     | 14.56                                 |           | 4482      | 11.72                                 |
|           |           |                                       |           | 3583      | 9.51                                  |
| 4.2       | 12650     | 18.64                                 |           | 2613      | 7.05                                  |
|           | 10785     | 16.16                                 |           | 1379      | 4.80                                  |



Table 24. Magnetization data for the quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 250 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat.

| T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) | T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) |
|---------------------------|-----------|---------------------------------------|---------------------------|-----------|---------------------------------------|
| 296.06                    | 12650     | 6.93                                  | 4.2                       | 8725      | 24.97                                 |
| 243.59                    | 12650     | 6.97                                  |                           | 6981      | 20.38                                 |
| 189.78                    | 12650     | 7.12                                  |                           | 5550      | 16.20                                 |
| 122.42                    | 12650     | 7.43                                  |                           | 4487      | 12.97                                 |
| 100.68                    | 12650     | 7.81                                  |                           | 3578      | 10.33                                 |
| 78.05                     | 12650     | 8.02                                  |                           | 2628      | 7.71                                  |
| 64.70                     | 12650     | 8.67                                  |                           | 1375      | 3.77                                  |
| 55.88                     | 12650     | 9.06                                  |                           |           |                                       |
| 47.44                     | 12650     | 9.41                                  | 2.73                      | 12578     | 46.57                                 |
| 41.54                     | 12650     | 9.61                                  |                           | 10605     | 41.00                                 |
| 33.64                     | 12650     | 11.09                                 |                           | 8722      | 35.00                                 |
| 30.99                     | 12650     | 11.01                                 |                           | 6956      | 28.22                                 |
|                           |           |                                       |                           | 5551      | 22.61                                 |
| 20.06                     | 12684     | 13.59                                 |                           | 4493      | 18.25                                 |
|                           | 10811     | 11.53                                 |                           | 3600      | 14.50                                 |
|                           | 8859      | 9.50                                  |                           | 2608      | 10.61                                 |
|                           | 7125      | 7.87                                  |                           | 1395      | 5.35                                  |
|                           | 5649      | 6.01                                  |                           |           |                                       |
|                           | 4595      | 5.17                                  | 1.49                      | 12581     | 58.25                                 |
|                           | 3671      | 4.22                                  |                           | 10617     | 52.51                                 |
|                           | 2724      | 2.66                                  |                           | 8740      | 46.05                                 |
|                           | 1484      | 1.61                                  |                           | 6979      | 39.10                                 |
|                           |           |                                       |                           | 5552      | 32.51                                 |
| 16.69                     | 12650     | 14.86                                 |                           | 4493      | 27.25                                 |
| 11.09                     | 12650     | 18.80                                 |                           | 3579      | 22.48                                 |
| 6.3                       | 12650     | 27.71                                 |                           | 2629      | 17.58                                 |
|                           |           |                                       |                           | 1401      | 9.25                                  |
| 4.2                       | 12567     | 34.25                                 |                           |           |                                       |
|                           | 10687     | 29.88                                 |                           |           |                                       |



Table 25. Magnetization data for the quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 500 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 40 and 42.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 297.70    | 12650     | 0.742                                 | 9.90      | 7117      | 2.051                                 |
| 270.00    | 12650     | 0.755                                 |           | 5642      | 1.650                                 |
| 217.30    | 12650     | 0.779                                 |           | 4590      | 1.336                                 |
| 159.70    | 12650     | 0.824                                 |           | 3667      | 1.070                                 |
| 99.90     | 12650     | 0.970                                 |           | 2721      | 0.823                                 |
| 78.00     | 12650     | 1.036                                 |           | 1468      | 0.394                                 |
| 76.05     | 12650     | 1.045                                 |           |           |                                       |
| 62.02     | 12650     | 1.150                                 | 7.19      | 12650     | 4.618                                 |
| 46.24     | 12650     | 1.331                                 |           |           |                                       |
| 44.45     | 12650     | 1.336                                 | 4.2       | 12664     | 6.865                                 |
| 38.68     | 12650     | 1.455                                 |           | 10796     | 5.971                                 |
| 33.64     | 12650     | 1.585                                 |           | 8848      | 5.012                                 |
|           |           |                                       |           | 7117      | 4.092                                 |
| 25.15     | 12668     | 1.861                                 |           | 5642      | 3.311                                 |
|           | 10802     | 1.591                                 |           | 4590      | 2.705                                 |
|           | 8853      | 1.299                                 |           | 3667      | 2.176                                 |
|           | 7120      | 1.028                                 |           | 2718      | 1.658                                 |
|           | 5643      | 0.831                                 |           | 1474      | 0.925                                 |
|           | 4591      | 0.687                                 |           |           |                                       |
|           | 3667      | 0.532                                 | 2.66      | 12583     | 9.338                                 |
|           | 2735      | 0.413                                 |           | 10695     | 8.291                                 |
|           | 1468      | 0.228                                 |           | 8690      | 7.016                                 |
|           |           |                                       |           | 7025      | 5.799                                 |
| 17.39     | 12650     | 0.242                                 |           | 5568      | 4.647                                 |
|           |           |                                       |           | 4532      | 3.815                                 |
| 9.90      | 12654     | 3.627                                 |           | 3622      | 3.100                                 |
|           | 10796     | 3.104                                 |           | 2650      | 2.250                                 |
|           | 8848      | 2.550                                 |           | 1415      | 1.225                                 |



Table 26. Magnetization data for the quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 1000 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 40 and 43.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 297.58    | 12640     | 0.81                                  | 4.2       | 1407      | 1.60                                  |
| 242.97    | 12640     | 0.85                                  |           | 756       | 0.74                                  |
| 161.64    | 12640     | 0.99                                  |           |           |                                       |
| 62.66     | 12640     | 1.66                                  | 3.03      | 12572     | 15.36                                 |
| 42.69     | 12640     | 2.20                                  |           | 10690     | 13.69                                 |
| 27.68     | 12640     | 3.03                                  |           | 8734      | 11.84                                 |
| 24.68     | 12640     | 3.30                                  |           | 7023      | 9.86                                  |
| 19.42     | 12640     | 3.98                                  |           | 5570      | 8.10                                  |
| 10.71     | 12640     | 6.44                                  |           | 4516      | 6.84                                  |
|           |           |                                       |           | 3620      | 5.36                                  |
| 9.83      | 12640     | 6.88                                  |           | 2648      | 4.23                                  |
|           | 10770     | 5.95                                  |           | 1411      | 2.22                                  |
|           | 8820      | 4.88                                  |           | 1000      | 1.45                                  |
|           | 5620      | 3.16                                  |           |           |                                       |
|           | 3650      | 2.10                                  | 1.50      | 12580     | 19.93                                 |
|           | 1460      | 0.93                                  |           | 10690     | 18.34                                 |
|           |           |                                       |           | 8734      | 16.28                                 |
| 4.2       | 12574     | 12.98                                 |           | 7021      | 14.22                                 |
|           | 10688     | 11.37                                 |           | 5568      | 12.18                                 |
|           | 8707      | 9.63                                  |           | 4532      | 10.67                                 |
|           | 6985      | 7.78                                  |           | 3621      | 9.03                                  |
|           | 5561      | 6.46                                  |           | 2643      | 7.06                                  |
|           | 4526      | 5.24                                  |           | 1409      | 4.00                                  |
|           | 3617      | 4.25                                  |           | 1000      | 2.93                                  |
|           | 2646      | 3.05                                  |           |           |                                       |



Table 27. Magnetization data for the quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy containing 100 ppm Fe. The measurements were made in the metal cryostat. See Figure 44.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 296.16    | 12640     | 13.21                          | 5.84      | 12640     | 33.16                          |
| 243.10    | 12640     | 13.30                          |           |           |                                |
| 189.86    | 12640     | 13.46                          | 4.2       | 12640     | 38.44                          |
| 131.93    | 12640     | 13.88                          |           | 10770     | 33.75                          |
| 101.04    | 12640     | 14.31                          |           | 8824      | 28.18                          |
| 77.03     | 12640     | 14.85                          |           | 7100      | 23.11                          |
| 60.56     | 12640     | 15.45                          |           | 5630      | 18.45                          |
| 39.51     | 12640     | 16.90                          |           | 4585      | 15.09                          |
| 31.89     | 12640     | 17.69                          |           | 3660      | 12.19                          |
| 24.84     | 12640     | 18.82                          |           | 1470      | 4.72                           |
| 16.96     | 12640     | 21.11                          |           |           |                                |



Table 28. Magnetization data for the deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloy containing 100 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 45 and 46.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 297.10    | 12569     | 2.17                                  | 2.99      | 12571     | 9.78                                  |
| 242.99    | 12569     | 2.22                                  |           | 10682     | 8.48                                  |
| 189.72    | 12569     | 2.26                                  |           | 8688      | 6.80                                  |
| 132.48    | 12560     | 2.32                                  |           | 7018      | 5.71                                  |
| 99.76     | 12560     | 2.40                                  |           | 5561      | 4.65                                  |
| 74.86     | 12560     | 2.56                                  |           | 4525      | 3.87                                  |
| 61.30     | 12560     | 2.66                                  |           | 3615      | 3.28                                  |
| 43.29     | 12550     | 2.88                                  |           | 2646      | 2.25                                  |
| 34.45     | 12550     | 3.04                                  |           | 1407      | 1.02                                  |
| 26.25     | 12550     | 3.30                                  |           |           |                                       |
| 20.71     | 12550     | 3.70                                  | 2.08      | 12575     | 11.04                                 |
| 16.41     | 12550     | 3.96                                  |           | 10686     | 9.55                                  |
| 12.81     | 12550     | 4.11                                  |           | 8729      | 7.96                                  |
| 10.05     | 12550     | 4.68                                  |           | 7017      | 6.67                                  |
| 7.84      | 12550     | 5.29                                  |           | 5563      | 5.11                                  |
|           |           |                                       |           | 4526      | 4.31                                  |
| 4.2       | 12554     | 7.78                                  |           | 3616      | 3.57                                  |
|           | 10672     | 6.62                                  |           | 2647      | 2.36                                  |
|           | 8718      | 5.36                                  |           | 1410      | 1.30                                  |
|           | 7009      | 4.15                                  |           |           |                                       |
|           | 5556      | 3.45                                  | 1.44      | 12579     | 12.93                                 |
|           | 4524      | 2.79                                  |           | 10689     | 11.55                                 |
|           | 3612      | 2.24                                  |           | 8732      | 9.67                                  |
|           | 2647      | 1.61                                  |           | 7019      | 7.90                                  |
|           | 1406      | 0.82                                  |           | 5564      | 6.54                                  |
|           |           |                                       |           | 4527      | 5.48                                  |
|           |           |                                       |           | 3617      | 4.43                                  |
|           |           |                                       |           | 2646      | 3.35                                  |



Table 29. Magnetization data for the deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloy containing 500 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 45 and 47.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 297.15    | 12573     | 0.272                                 | 4.2       | 8727      | 2.347                                 |
| 243.02    | 12559     | 0.286                                 |           | 7017      | 1.897                                 |
| 162.55    | 12563     | 0.304                                 |           | 5565      | 1.512                                 |
| 131.78    | 12559     | 0.349                                 |           | 4527      | 1.241                                 |
| 100.48    | 12559     | 0.392                                 |           | 2649      | 0.704                                 |
| 77.63     | 12559     | 0.451                                 |           | 1410      | 0.384                                 |
| 59.42     | 12559     | 0.521                                 |           |           |                                       |
| 43.74     | 12557     | 0.639                                 | 3.02      | 12573     | 3.952                                 |
| 34.98     | 12556     | 0.728                                 |           | 10686     | 3.446                                 |
| 26.01     | 12556     | 0.887                                 |           | 8730      | 2.886                                 |
| 20.15     | 12550     | 0.105                                 |           | 7010      | 2.362                                 |
| 16.13     | 12549     | 1.230                                 |           | 5565      | 1.902                                 |
| 12.48     | 12551     | 1.529                                 |           | 4528      | 1.572                                 |
| 7.77      | 12548     | 2.069                                 |           | 3618      | 1.267                                 |
|           |           |                                       |           | 2648      | 0.901                                 |
| 5.60      | 12543     | 2.678                                 |           | 1407      | 0.476                                 |
|           | 10667     | 2.306                                 |           |           |                                       |
|           | 8716      | 1.923                                 | 2.15      | 12582     | 4.721                                 |
|           | 7010      | 1.562                                 |           | 10691     | 4.175                                 |
|           | 5556      | 1.231                                 |           | 8732      | 3.459                                 |
|           | 4522      | 1.006                                 |           | 7018      | 2.968                                 |
|           | 3614      | 0.797                                 |           | 5567      | 2.415                                 |
|           | 2646      | 0.615                                 |           | 4529      | 1.999                                 |
|           | 1410      | 0.325                                 |           | 3620      | 1.613                                 |
|           |           |                                       |           | 2648      | 1.200                                 |
| 4.2       | 12570     | 3.284                                 |           | 1408      | 0.616                                 |
|           | 10683     | 2.830                                 |           |           |                                       |



Table 29. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 1.36      | 12564     | 5.573                          | 1.36      | 4530      | 2.593                          |
|           | 10690     | 5.046                          |           | 3621      | 2.146                          |
|           | 8735      | 4.348                          |           | 2647      | 1.632                          |
|           | 7022      | 3.699                          |           | 1413      | 0.915                          |
|           | 5567      | 3.067                          |           | 369       | 0.235                          |



Table 30. Magnetization data for the deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloy containing 1000 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 45 and 48.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 297.53    | 12589     | 0.364                                 | 4.2       | 7018      | 3.881                                 |
| 243.02    | 12589     | 0.391                                 |           | 5563      | 3.116                                 |
| 188.23    | 12589     | 0.456                                 |           | 4528      | 2.556                                 |
| 132.60    | 12584     | 0.538                                 |           | 3618      | 2.058                                 |
| 79.47     | 12584     | 0.744                                 |           | 2647      | 1.505                                 |
| 60.60     | 12584     | 0.901                                 |           | 1408      | 0.796                                 |
| 44.56     | 12584     | 1.139                                 |           |           |                                       |
| 35.93     | 12576     | 1.336                                 | 3.14      | 12573     | 7.876                                 |
| 26.57     | 12578     | 1.679                                 |           | 10687     | 6.950                                 |
| 20.19     | 12577     | 2.040                                 |           | 8732      | 5.880                                 |
| 14.69     | 12577     | 2.648                                 |           | 7020      | 4.871                                 |
| 11.09     | 12574     | 3.246                                 |           | 5565      | 3.934                                 |
|           |           |                                       |           | 4529      | 3.285                                 |
| 7.06      | 12562     | 4.523                                 |           | 3622      | 2.650                                 |
|           | 10678     | 3.914                                 |           | 2648      | 1.962                                 |
|           | 8725      | 3.182                                 |           | 1407      | 0.998                                 |
|           | 7010      | 2.579                                 |           |           |                                       |
|           | 5564      | 2.064                                 | 2.30      | 12591     | 9.154                                 |
|           | 4527      | 1.683                                 |           | 10694     | 8.232                                 |
|           | 3619      | 1.327                                 |           | 8737      | 7.125                                 |
|           | 2647      | 0.980                                 |           | 7025      | 6.055                                 |
|           | 1407      | 0.526                                 |           | 4531      | 4.233                                 |
|           |           |                                       |           | 3620      | 3.516                                 |
| 4.2       | 12568     | 6.539                                 |           | 2650      | 2.663                                 |
|           | 10687     | 5.696                                 |           | 1411      | 1.498                                 |
|           | 8729      | 4.757                                 |           | 5406      | 4.950                                 |



Table 30. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 1.47      | 12580     | 9.977                          | 1.47      | 4534      | 4.924                          |
|           | 10694     | 8.756                          |           | 3622      | 4.091                          |
|           | 8748      | 7.931                          |           | 2649      | 3.152                          |
|           | 7022      | 6.834                          |           | 1411      | 1.803                          |
|           | 5571      | 5.788                          |           | 369       | 0.398                          |



Table 31. Magnetization data for the deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 100 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 49 and 50.

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}\text{emu/g}$ ) |
|-----------|-----------|---------------------------------------|-----------|-----------|---------------------------------------|
| 294.87    | 12640     | 6.33                                  | 9.71      | 2729      | 3.20                                  |
| 246.83    | 12640     | 6.34                                  |           | 1486      | 1.45                                  |
| 132.11    | 12640     | 6.39                                  |           |           |                                       |
| 68.15     | 12640     | 6.75                                  | 4.2       | 12601     | 16.47                                 |
| 53.92     | 12640     | 6.98                                  |           | 10846     | 14.45                                 |
|           |           |                                       |           | 8904      | 11.72                                 |
| 20.06     | 12702     | 8.62                                  |           | 7162      | 9.38                                  |
|           | 10829     | 7.30                                  |           | 5679      | 7.33                                  |
|           | 8873      | 5.98                                  |           | 4622      | 6.29                                  |
|           | 7139      | 4.76                                  |           | 3695      | 4.97                                  |
|           | 5661      | 3.78                                  |           | 2747      | 3.62                                  |
|           | 4604      | 3.14                                  |           | 1497      | 1.87                                  |
|           | 3679      | 2.49                                  |           |           |                                       |
|           | 2729      | 1.78                                  | 2.88      | 12596     | 20.27                                 |
|           | 1484      | 0.70                                  |           | 10865     | 17.71                                 |
|           |           |                                       |           | 8917      | 14.76                                 |
| 10.74     | 12640     | 11.11                                 |           | 7163      | 12.14                                 |
|           |           |                                       |           | 5671      | 9.74                                  |
| 9.71      | 12709     | 11.85                                 |           | 4613      | 7.76                                  |
|           | 10835     | 10.24                                 |           | 3695      | 6.25                                  |
|           | 8870      | 8.46                                  |           | 2745      | 4.60                                  |
|           | 7141      | 6.93                                  |           | 1495      | 2.52                                  |
|           | 5663      | 5.66                                  |           |           |                                       |
|           | 4603      | 4.75                                  | 2.26      | 12604     | 22.29                                 |
|           | 3679      | 3.42                                  |           | 10846     | 19.60                                 |



Table 31. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-3}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 2.26      | 8909      | 16.45                          | 1.44      | 12599     | 25.68                          |
|           | 7165      | 13.67                          |           | 10843     | 23.13                          |
|           | 5681      | 10.99                          |           | 8905      | 20.00                          |
|           | 4623      | 8.77                           |           | 7161      | 17.11                          |
|           | 3696      | 7.05                           |           | 5678      | 14.19                          |
|           | 2746      | 5.03                           |           | 4622      | 11.64                          |
|           | 1499      | 2.78                           |           | 3695      | 9.17                           |
|           |           |                                |           | 2744      | 6.85                           |
|           |           |                                |           | 1495      | 3.69                           |
|           |           |                                |           | 415       | 1.14                           |



Table 32. Magnetization data for the deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 500 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 49 and 51.

| T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|---------------------------|-----------|---------------------------------------|---------------------------|-----------|---------------------------------------|
| 292.36                    | 12742     | 0.733                                 | 8.43                      | 1467      | 0.459                                 |
| 243.65                    | 12733     | 0.743                                 |                           | 406       | 0.136                                 |
| 183.54                    | 12724     | 0.775                                 |                           |           |                                       |
| 128.45                    | 12720     | 0.841                                 | 4.2                       | 12682     | 6.290                                 |
| 93.63                     | 12714     | 0.934                                 |                           | 10817     | 5.474                                 |
| 75.88                     | 12710     | 1.011                                 |                           | 8871      | 4.563                                 |
| 62.15                     | 12720     | 1.086                                 |                           | 7134      | 3.723                                 |
| 48.05                     | 12716     | 1.241                                 |                           | 5657      | 2.969                                 |
| 41.60                     | 12713     | 1.337                                 |                           | 4603      | 2.438                                 |
| 33.37                     | 12712     | 1.509                                 |                           | 3677      | 1.959                                 |
| 29.72                     | 12712     | 1.608                                 |                           | 2729      | 1.436                                 |
| 22.35                     | 12716     | 1.913                                 |                           | 1484      | 0.781                                 |
| 19.40                     | 12707     | 2.087                                 |                           | 407       | 0.181                                 |
| 16.27                     | 12721     | 2.378                                 |                           |           |                                       |
| 14.70                     | 12712     | 2.598                                 | 3.05                      | 12681     | 7.675                                 |
| 12.14                     | 12710     | 2.966                                 |                           | 10813     | 6.773                                 |
|                           |           |                                       |                           | 8866      | 5.735                                 |
| 8.43                      | 12716     | 3.871                                 |                           | 7132      | 4.724                                 |
|                           | 10840     | 3.322                                 |                           | 5654      | 3.839                                 |
|                           | 8885      | 2.731                                 |                           | 4604      | 3.159                                 |
|                           | 7145      | 2.217                                 |                           | 3677      | 2.547                                 |
|                           | 5666      | 1.745                                 |                           | 2729      | 1.915                                 |
|                           | 4611      | 1.440                                 |                           | 1484      | 1.051                                 |
|                           | 3685      | 1.129                                 |                           | 406       | 0.237                                 |
|                           | 2734      | 0.875                                 |                           |           |                                       |



Table 32. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 1.37      | 12677     | 10.469                         | 1.37      | 4600      | 5.266                          |
|           | 10812     | 9.566                          |           | 3675      | 4.368                          |
|           | 8866      | 8.463                          |           | 2728      | 3.370                          |
|           | 7131      | 7.310                          |           | 1484      | 1.879                          |
|           | 5655      | 6.184                          |           | 407       | 0.492                          |



Table 33. Magnetization data for the deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy containing 1000 ppm Fe. The measurements between  $\sim 300^\circ\text{K}$  and  $4.2^\circ\text{K}$  were made in the metal cryostat; the measurements at and below  $4.2^\circ\text{K}$  were made in the glass cryostat. See Figures 49 and 52.

| T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) | T<br>( $^\circ\text{K}$ ) | H<br>(Oe) | $\sigma$<br>( $10^{-2}\text{emu/g}$ ) |
|---------------------------|-----------|---------------------------------------|---------------------------|-----------|---------------------------------------|
| 298.13                    | 12640     | 0.77                                  | 4.2                       | 2710      | 2.69                                  |
| 243.15                    | 12640     | 0.81                                  |                           | 1470      | 1.49                                  |
| 189.95                    | 12640     | 0.87                                  |                           |           |                                       |
| 132.02                    | 12640     | 1.00                                  | 3.05                      | 12589     | 13.64                                 |
| 100.88                    | 12640     | 1.15                                  |                           | 10695     | 12.07                                 |
| 74.93                     | 12640     | 1.36                                  |                           | 8736      | 10.23                                 |
| 59.30                     | 12640     | 1.57                                  |                           | 7024      | 8.49                                  |
| 40.99                     | 12640     | 2.05                                  |                           | 5567      | 7.01                                  |
| 31.16                     | 12640     | 2.45                                  |                           | 4529      | 5.82                                  |
|                           |           |                                       |                           | 3621      | 4.67                                  |
| 20.50                     | 12636     | 3.30                                  |                           | 2649      | 3.46                                  |
|                           | 8827      | 2.29                                  |                           | 1407      | 1.62                                  |
|                           | 5624      | 1.49                                  |                           | 369       | 0.45                                  |
|                           | 3650      | 0.99                                  |                           |           |                                       |
|                           | 1460      | 0.40                                  | 2.00                      | 12593     | 16.09                                 |
|                           |           |                                       |                           | 10660     | 14.61                                 |
| 9.88                      | 12640     | 5.81                                  |                           | 8741      | 12.84                                 |
|                           |           |                                       |                           | 7028      | 11.01                                 |
| 4.2                       | 12640     | 11.27                                 |                           | 5571      | 9.34                                  |
|                           | 10780     | 9.94                                  |                           | 4532      | 8.04                                  |
|                           | 8833      | 8.39                                  |                           | 3620      | 6.65                                  |
|                           | 7100      | 6.87                                  |                           | 2649      | 5.03                                  |
|                           | 5629      | 5.56                                  |                           | 1408      | 2.32                                  |
|                           | 4568      | 4.56                                  |                           | 369       | 0.56                                  |
|                           | 3658      | 3.69                                  |                           |           |                                       |



Table 33. (Continued)

| T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) | T<br>(°K) | H<br>(Oe) | $\sigma$<br>( $10^{-2}$ emu/g) |
|-----------|-----------|--------------------------------|-----------|-----------|--------------------------------|
| 1.47      | 12582     | 17.83                          | 1.47      | 4533      | 9.41                           |
|           | 10692     | 16.39                          |           | 3622      | 8.19                           |
|           | 8735      | 14.64                          |           | 2648      | 6.45                           |
|           | 7021      | 12.82                          |           | 1409      | 3.56                           |
|           | 5568      | 11.05                          |           | 369       | 0.94                           |



## B. Data Analysis

### 1. Cu-Ni.

#### a. Weakly ferromagnetic alloys.

The magnetization results for quenched, weakly ferromagnetic Cu-Ni alloys containing 50, 48, and 46 at % nickel are given in Tables 7, 8 and 9 respectively. For the quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  alloy isothermal magnetization measurements were made at 78°K and lower temperatures (Figs. 1, 2); for the  $\text{Cu}_{0.52}\text{Ni}_{0.48}$  and  $\text{Cu}_{0.54}\text{Ni}_{0.46}$  alloys, measurements were made only at 4.2°K and lower temperatures, as shown in Figs. 3 and 4. The Curie temperature  $T_c$  for  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  was estimated from  $\sigma^2$  vs.  $\frac{H_i}{\sigma}$  graphs (Fig. 5) to be  $\sim 37^\circ\text{K}$ , at which  $\sigma^2 = 0$  extrapolates to  $\frac{H_i}{\sigma} = 0$ . Here  $H_i$  (Oe) is the internal field, as calculated from the applied field  $H$  (Oe) and the demagnetization correction for a spherical specimen:  $H_i = H - \frac{4\pi}{3} \sigma \rho$ . Here  $\rho$  is the density of the alloy, which was assumed to be 8.95 g/cc. taking the weighted average of the density values of copper and nickel. The Curie temperature so obtained for  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  is in good agreement with the value obtained ( $36 \pm 1^\circ\text{K}$ ), for an alloy of the same composition by Robbins et al.<sup>16</sup> Referring now to Fig. 1, one may also note that the isothermal  $\sigma$  vs.  $H$  graphs for the  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  alloy at  $\sim 40^\circ\text{K}$  and  $\sim 53^\circ\text{K}$  show pronounced curvature, indicating that giant magnetic



Figure 1. Isothermal magnetization data for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  between  $78.08^\circ\text{K}$  and  $10.39^\circ\text{K}$ . See Table 7.



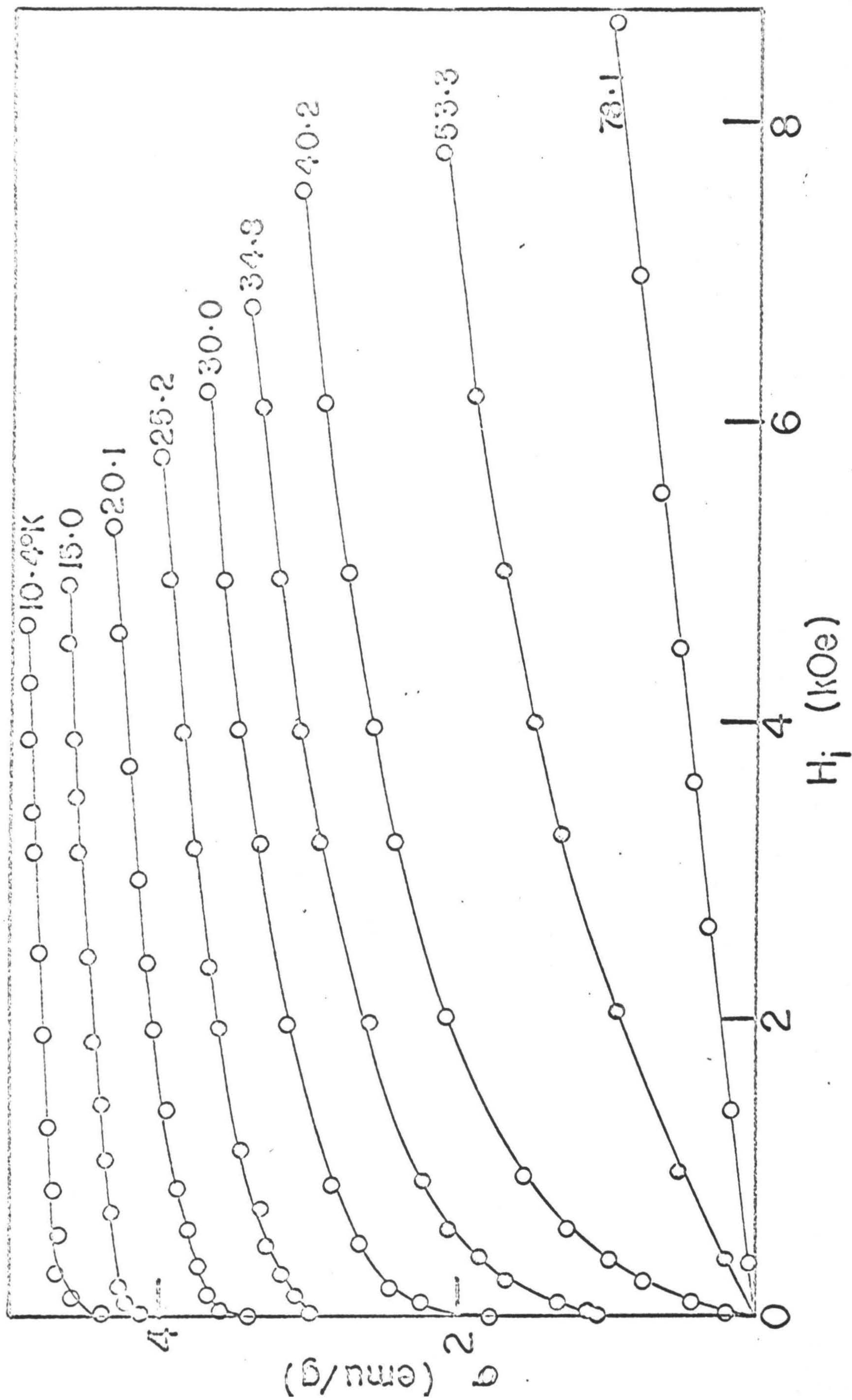




Figure 2. Isothermal low temperature ( $T \leq 4.2^\circ\text{K}$ ) magnetization data for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ . See Table 7.



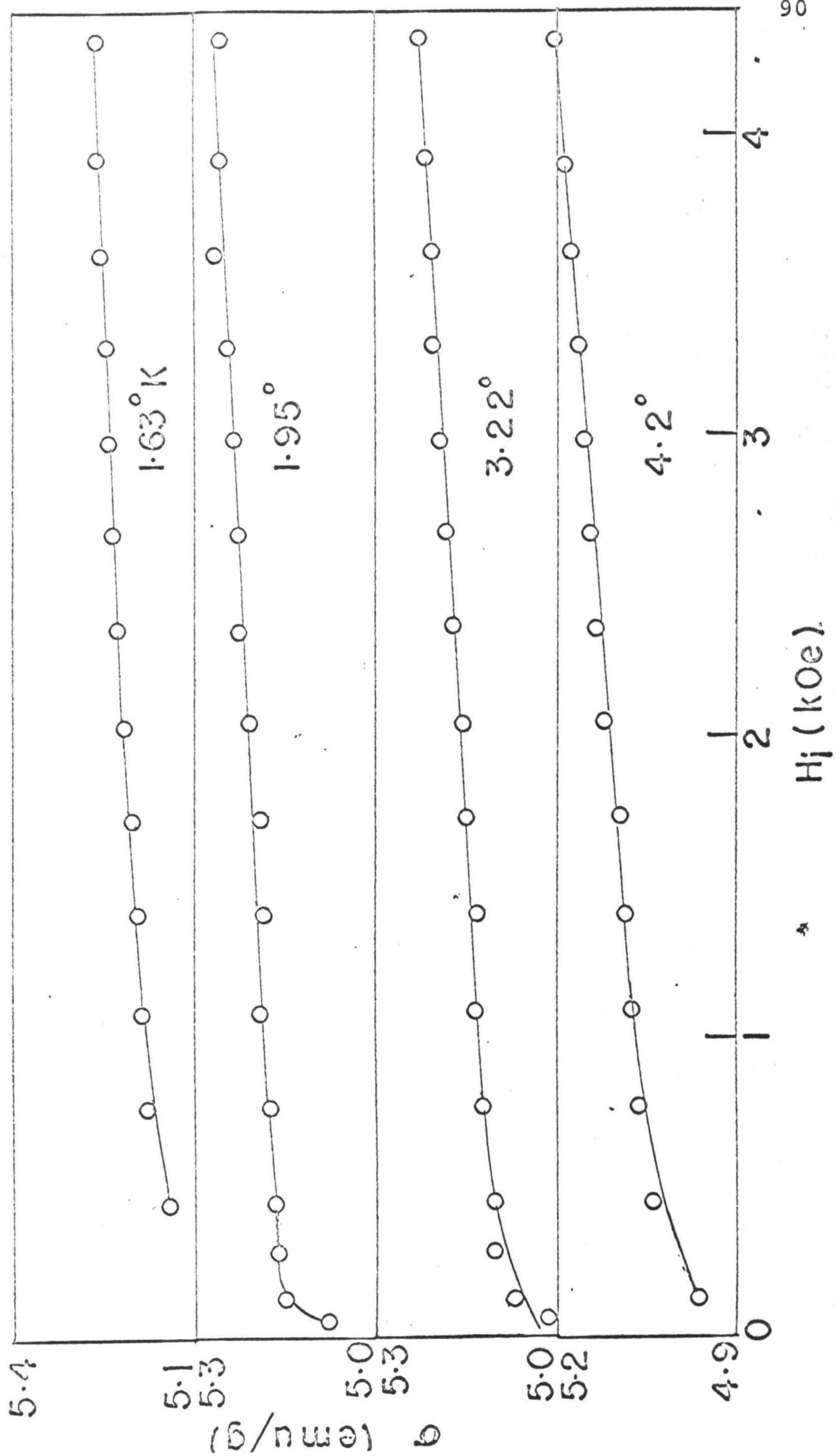




Figure 3. Isothermal low temperature ( $T \leq 4.2^\circ\text{K}$ ) magnetization data for quenched  $\text{Cu}_{0.52}\text{Ni}_{0.48}$ . See Table 8.



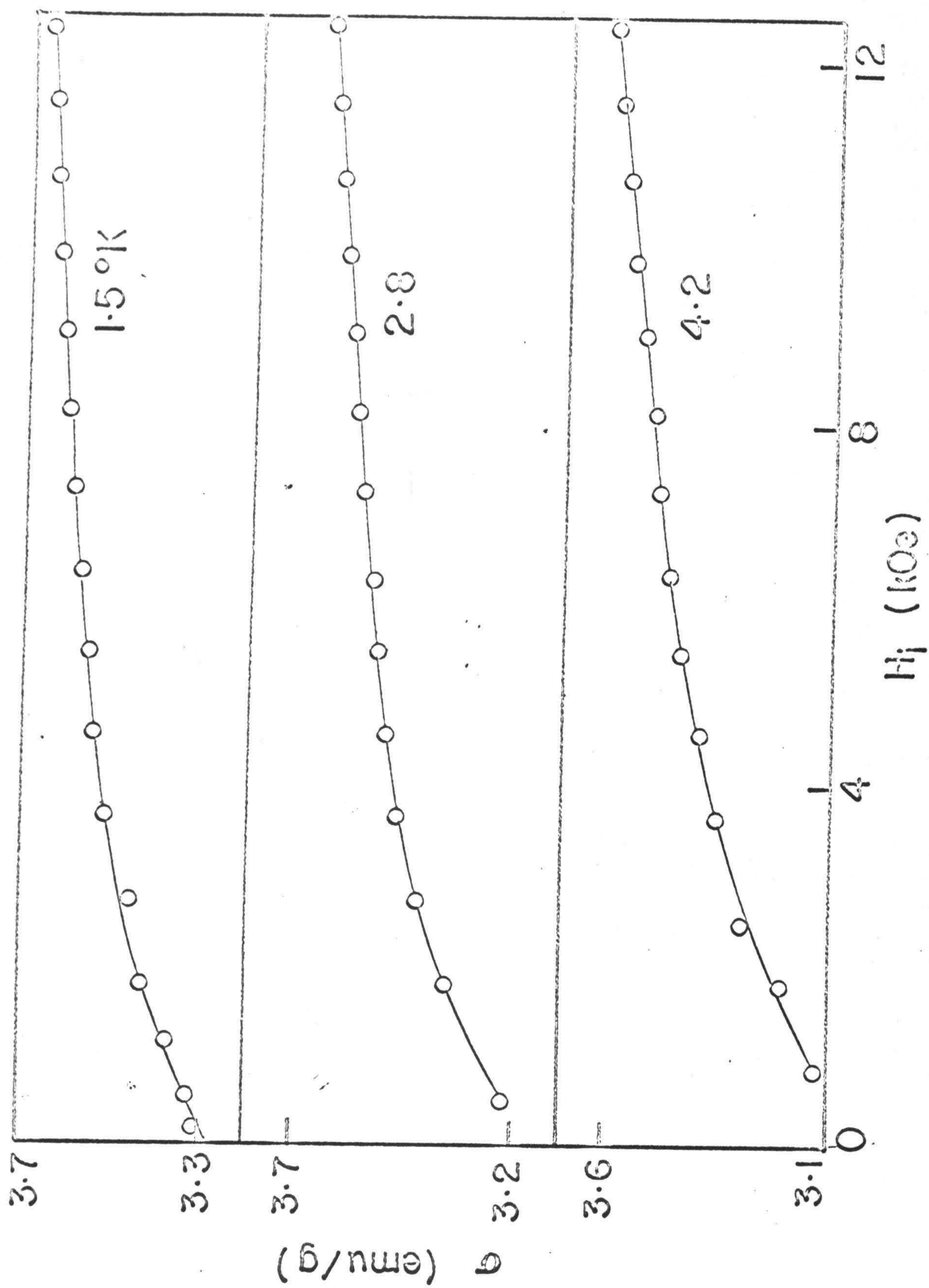




Figure 4. Isothermal low temperature ( $T \leq 4.2^\circ\text{K}$ ) magnetization data for quenched  $\text{Cu}_{0.54}\text{Ni}_{0.46}$ . See Table 9.



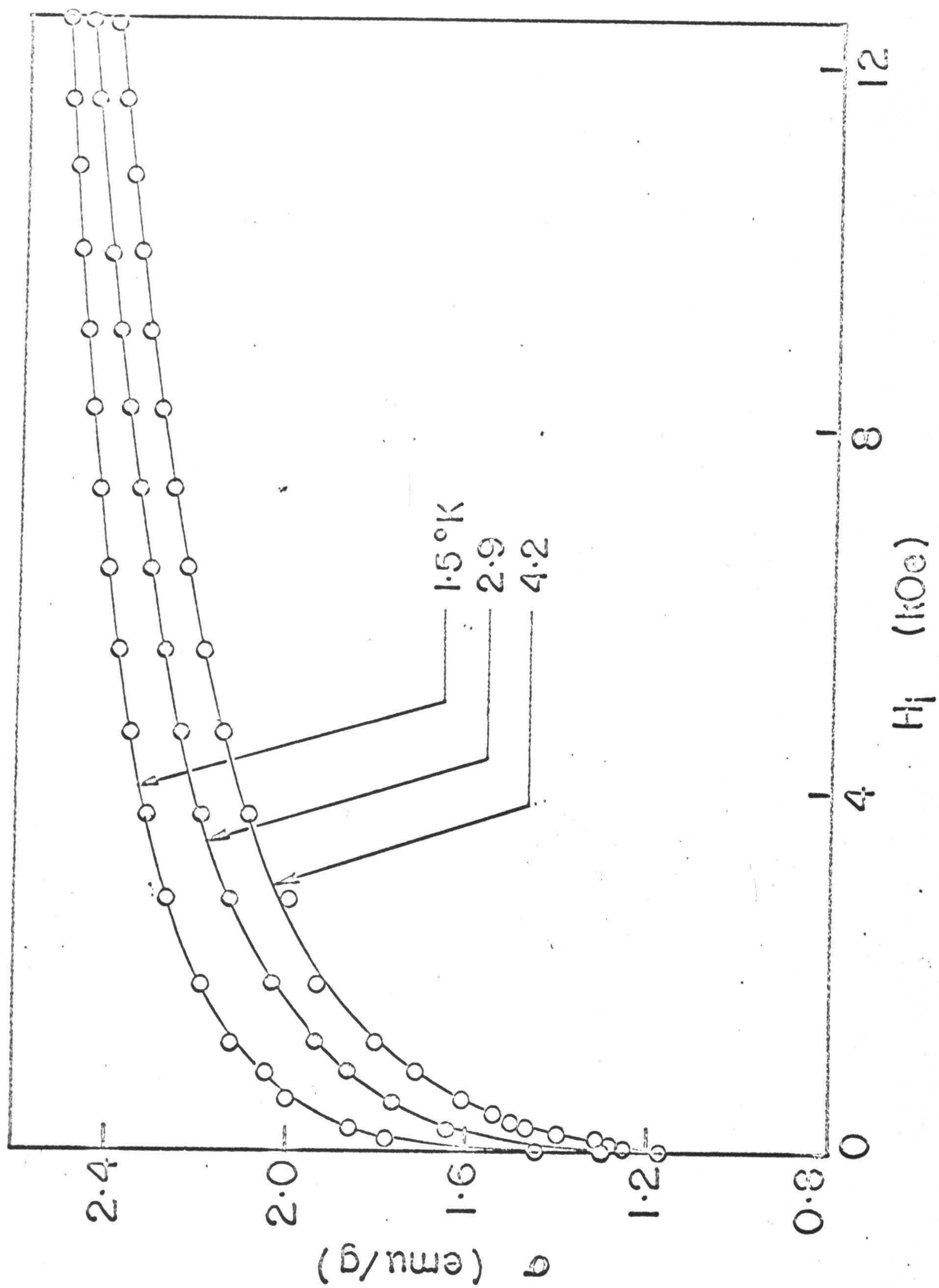
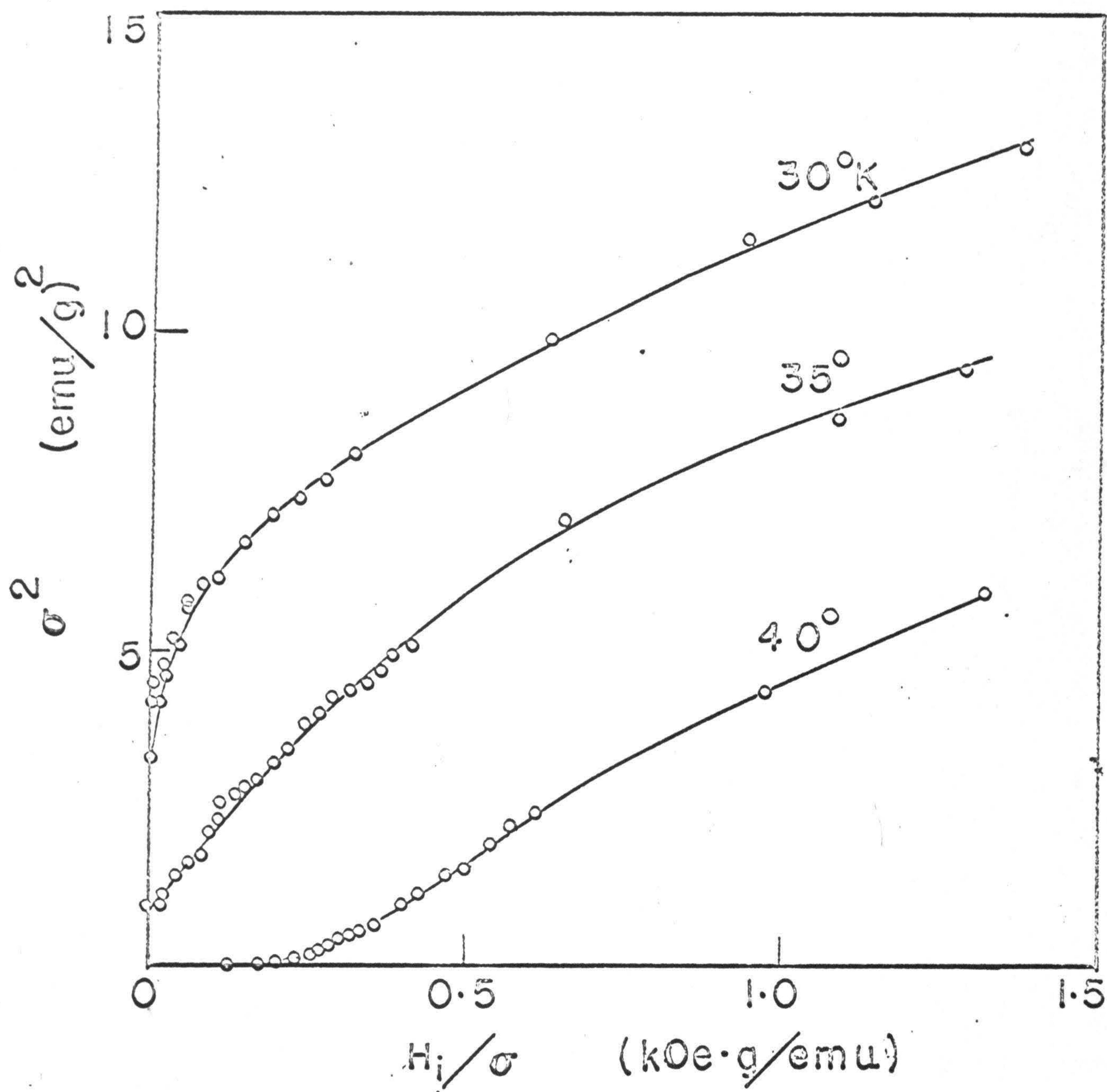




Figure 5.  $\sigma^2$  vs.  $\frac{H_i}{\sigma}$  graphs at low fields, for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ . The Curie temperature  $T_c$  is estimated to be  $\approx 37^\circ\text{K}$ .







moments are present well above the Curie temperature. The  $1/\chi_i$  (the inverse initial susceptibility) versus  $T$  graph at temperatures above  $T_C$ , shows considerable deviation from normal Curie-Weiss type behavior (Fig. 6). Above  $\sim 160^\circ\text{K}$  the graph is linear, with a paramagnetic Curie temperature  $pT_C$  of  $\sim 90^\circ\text{K}$ . Below  $\sim 160^\circ\text{K}$  the graph is curved, indicating a continuous increase in the "differential Curie constant" and a continuous decrease in the "differential Weiss temperature" as the Curie temperature  $T_C \approx 37^\circ\text{K}$  is approached. These results may be interpreted in terms of giant magnetic moments just above  $T_C$  and their gradual breakup into smaller clusters as the temperature is raised.

Recently<sup>17</sup> the initial susceptibility for a  $\text{Cu}_{0.47}\text{Ni}_{0.53}$  alloy was represented by an equation of the form

$$\chi_i(T) = \frac{A}{(T-T_C)^\nu} \quad \text{for } T > T_C \quad (6)$$

We found that the susceptibility data for the  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  alloy can also be represented by the above equation with parameter values of  $A = 0.0136$  and  $\nu = 1.133$ , as shown in a  $\ln \chi_i$   $\ln(T-T_C)$  graph (Fig. 7). However, the physical significance of Eq. 6 is not entirely clear.

The Curie temperature of the ferromagnetically weakest alloy, i.e.,  $\text{Cu}_{0.54}\text{Ni}_{0.46}$ , was estimated to be  $>4.2^\circ\text{K}$  from Fig. 8 where one finds remanence in the  $\sigma^2$  vs.  $H_i/\sigma$  graphs at  $4.2^\circ\text{K}$ .

The saturation magnetization values for all three alloys, i.e.,  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ ,  $\text{Cu}_{0.52}\text{Ni}_{0.48}$  and  $\text{Cu}_{0.54}\text{Ni}_{0.46}$ , were determined



Figure 6.  $\chi_i$  vs.  $T$  and  $\frac{1}{\chi_i}$  vs.  $T$  graphs for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ .



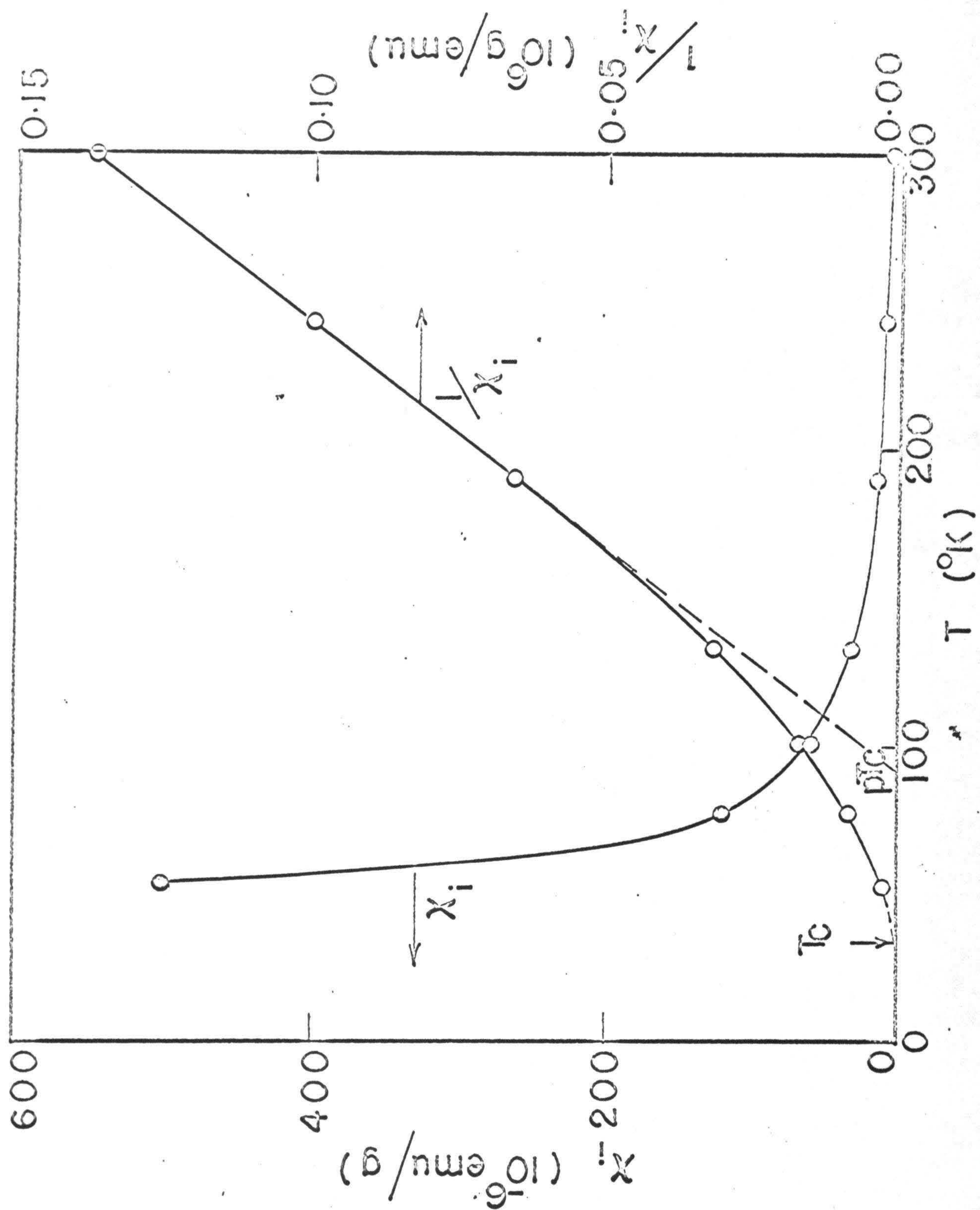




Figure 7. Logarithmic graph of  $\chi_i$  vs.  $(T-T_c)$  for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ .



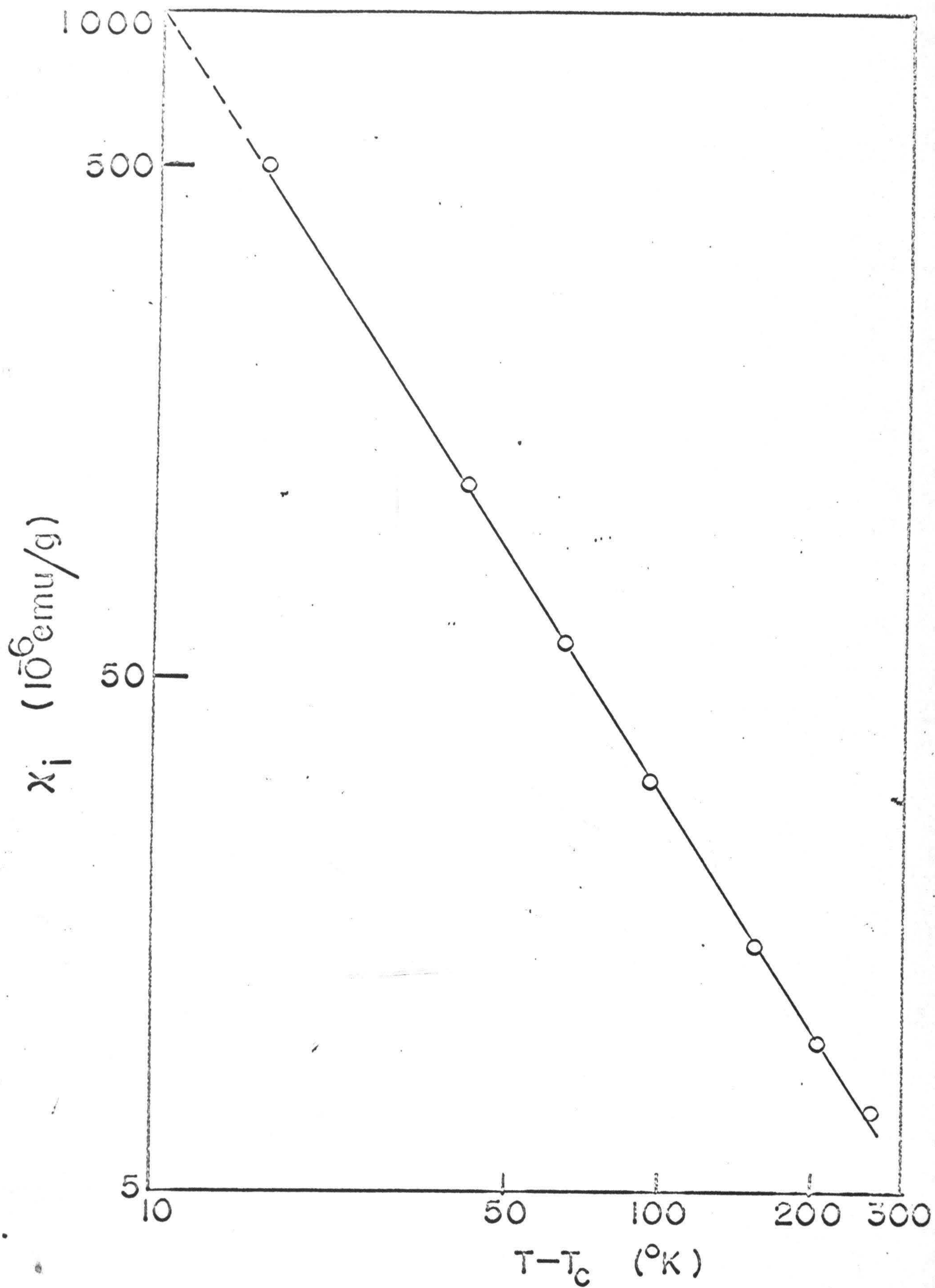
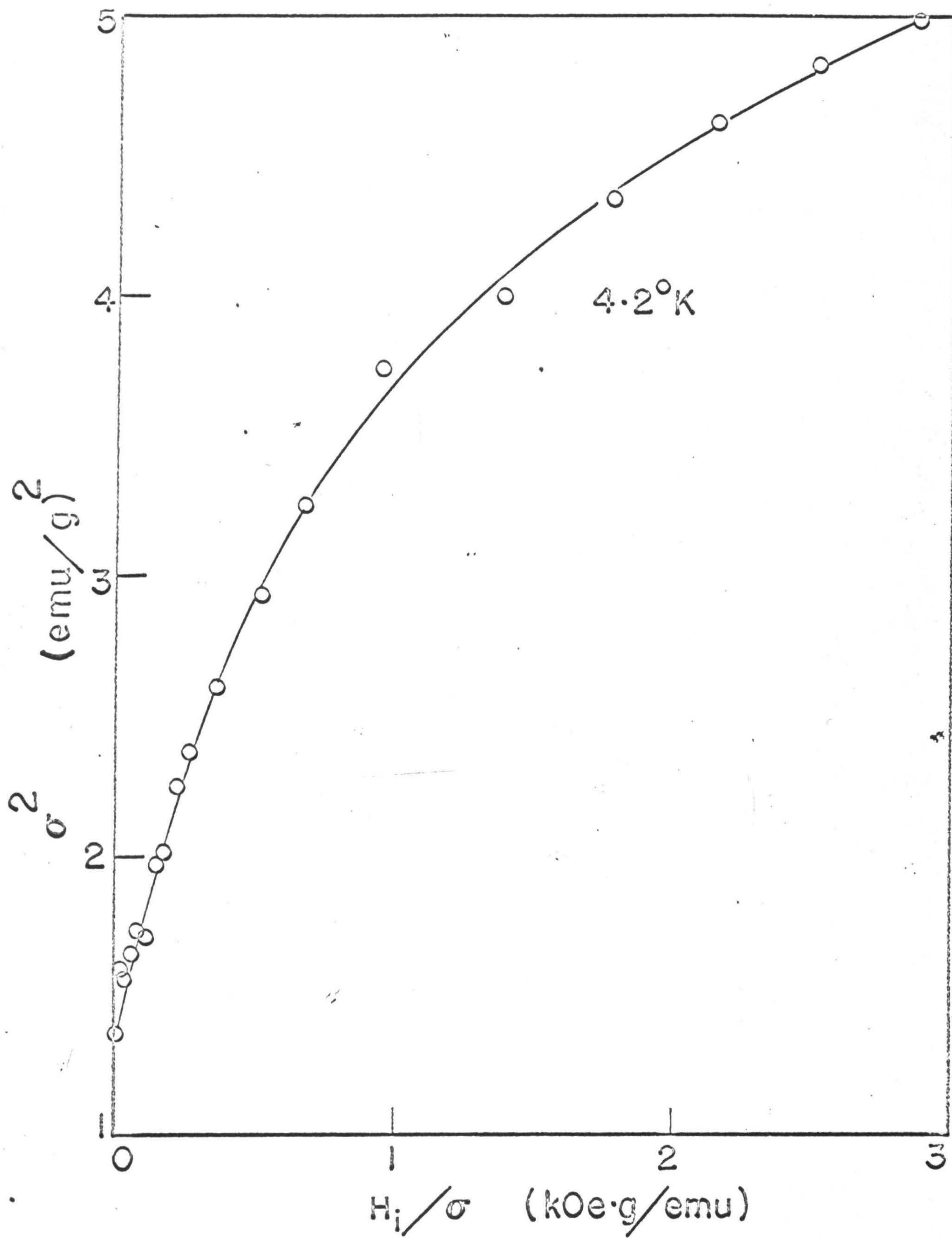




Figure 8.  $\sigma^2$  vs.  $\frac{H_i}{\sigma}$  graphs for the quenched  $\text{Cu}_{0.54}\text{Ni}_{0.46}$  alloy for  $4.2^\circ\text{K}$ . The Curie temperature is somewhat higher than  $4.2^\circ\text{K}$ .







from the low temperature data ( $T \leq 4.2^\circ\text{K}$ ) as follows. For each alloy  $\sigma$  vs.  $1/H_i$  isotherms were drawn to obtain the values of  $\sigma_{H_i=\infty, T}$  by extrapolation to  $1/H_i = 0$  (Figs. 9, 10, 11). A  $\sigma_{H_i=\infty, T}$  vs.  $T$  graph was then extrapolated to  $T = 0$  (Fig. 12) to give  $\sigma_{H_i=\infty, T=0}$ , the saturation magnetization at absolute zero (Table 34). From the value of  $\sigma_{H_i=\infty, T=0}$ , the values of  $\bar{\mu}$ , the average magnetic moment per alloy atom, were calculated (Table 34).

Table 34. Values of the saturation magnetization  $\sigma_{\infty, 0}$  (emu/g) and of  $\bar{\mu}$ , the average magnetic moment per alloy atom, in Bohr magnetons.

| Alloy                              | $\sigma_{\infty, 0}$ | $\bar{\mu}$ |
|------------------------------------|----------------------|-------------|
| $\text{Cu}_{0.5}\text{Ni}_{0.5}$   | 5.30                 | 0.058       |
| $\text{Cu}_{0.52}\text{Ni}_{0.48}$ | 3.75                 | 0.041       |
| $\text{Cu}_{0.54}\text{Ni}_{0.46}$ | 2.65                 | 0.029       |

#### b. Paramagnetic alloys.

The magnetic data for the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloys, and for the  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy in the as-quenched and aged conditions, are listed in Tables 10 to 20.

$\text{Cu}_{0.9}\text{Ni}_{0.1}$ : The magnetization at  $4.2^\circ\text{K}$  for the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloy is found to be linear with  $H$  up to 12.6 kOe, as seen in Fig. 13. The susceptibility (Fig. 14) may be thought of<sup>2</sup> as comprising the band susceptibility,  $\chi_b$ , of the solid solution,



Figure 9.  $\sigma$  vs.  $\frac{1}{H_i}$  graphs for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$ . By extrapolating to  $\frac{1}{H_i} = 0$  values of  $\sigma_{H_i=\infty, T}$  were determined for the different temperatures.



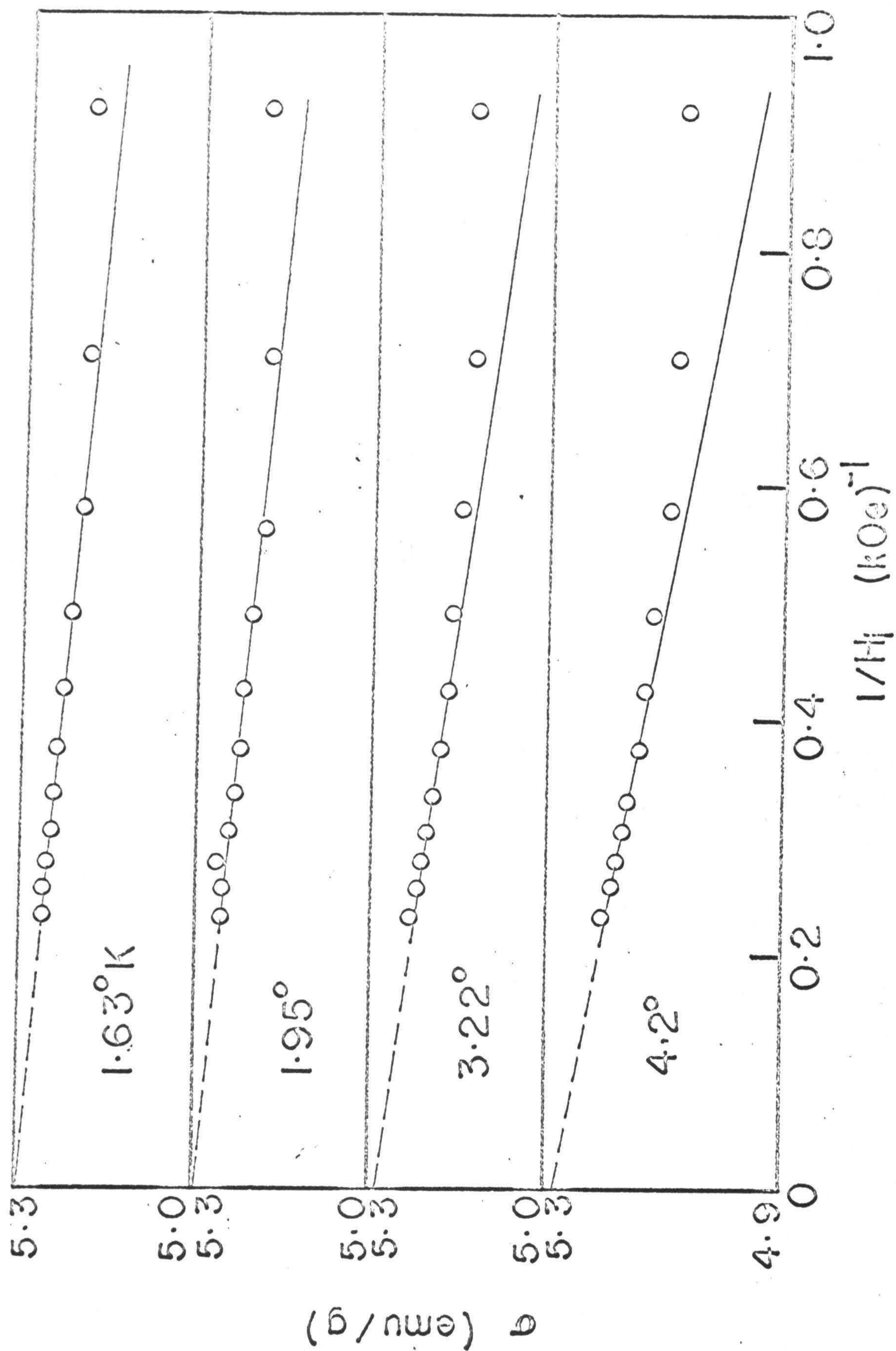




Figure 10.  $\sigma$  vs.  $\frac{1}{H_i}$  graphs for quenched  $\text{Cu}_{0.52}\text{Ni}_{0.48}$ . By extrapolating to  $\frac{1}{H_i} = 0$  values of  $\sigma_{H_i=\infty, T}$  were determined for the different temperatures.



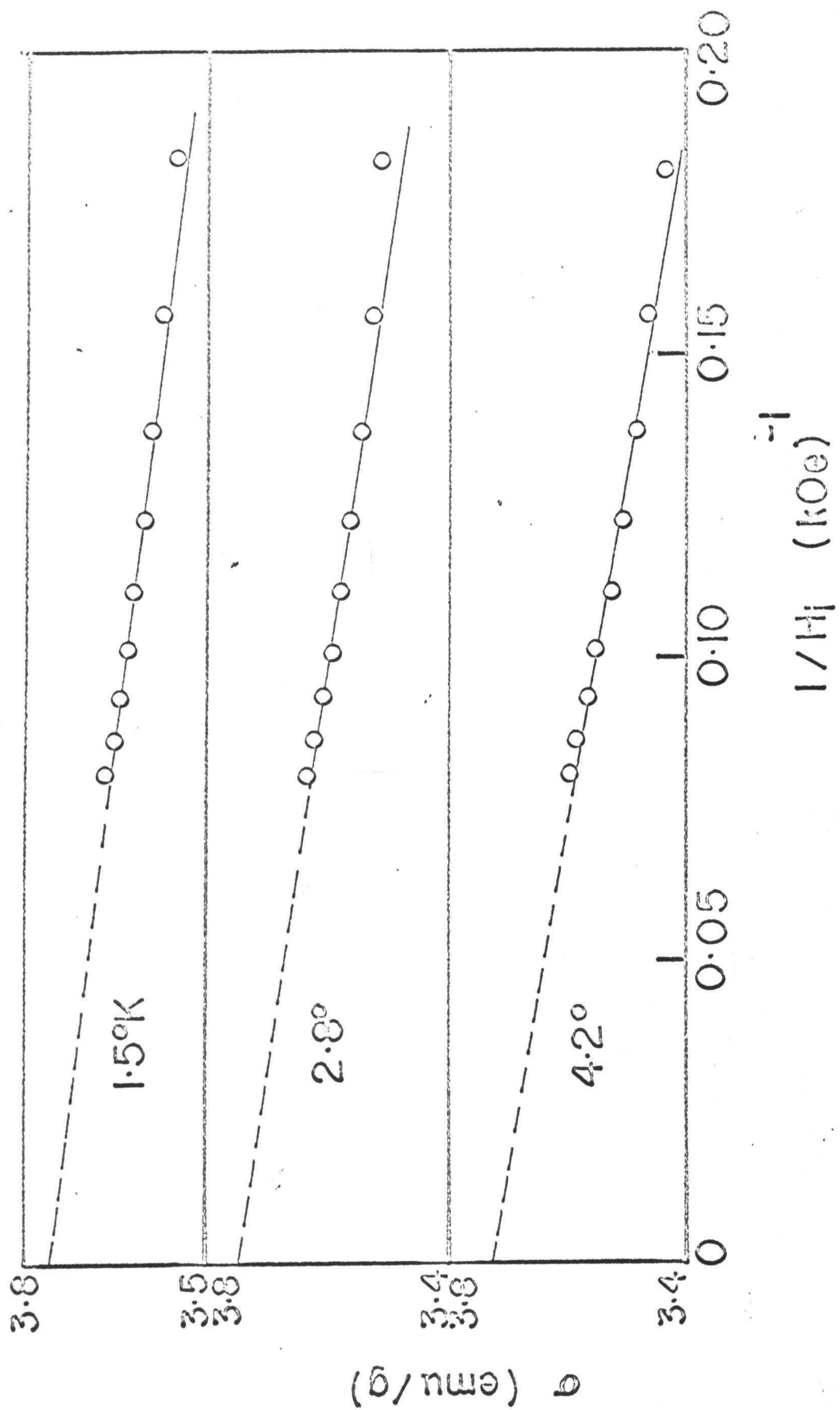




Figure 11.  $\sigma$  vs.  $\frac{1}{H_i}$  graphs for quenched  $\text{Cu}_{0.54}\text{Ni}_{0.46}$ . By extrapolating to  $\frac{1}{H_i} = 0$  values of  $\sigma_{H_i=\infty, T}$  were determined for the different temperatures.



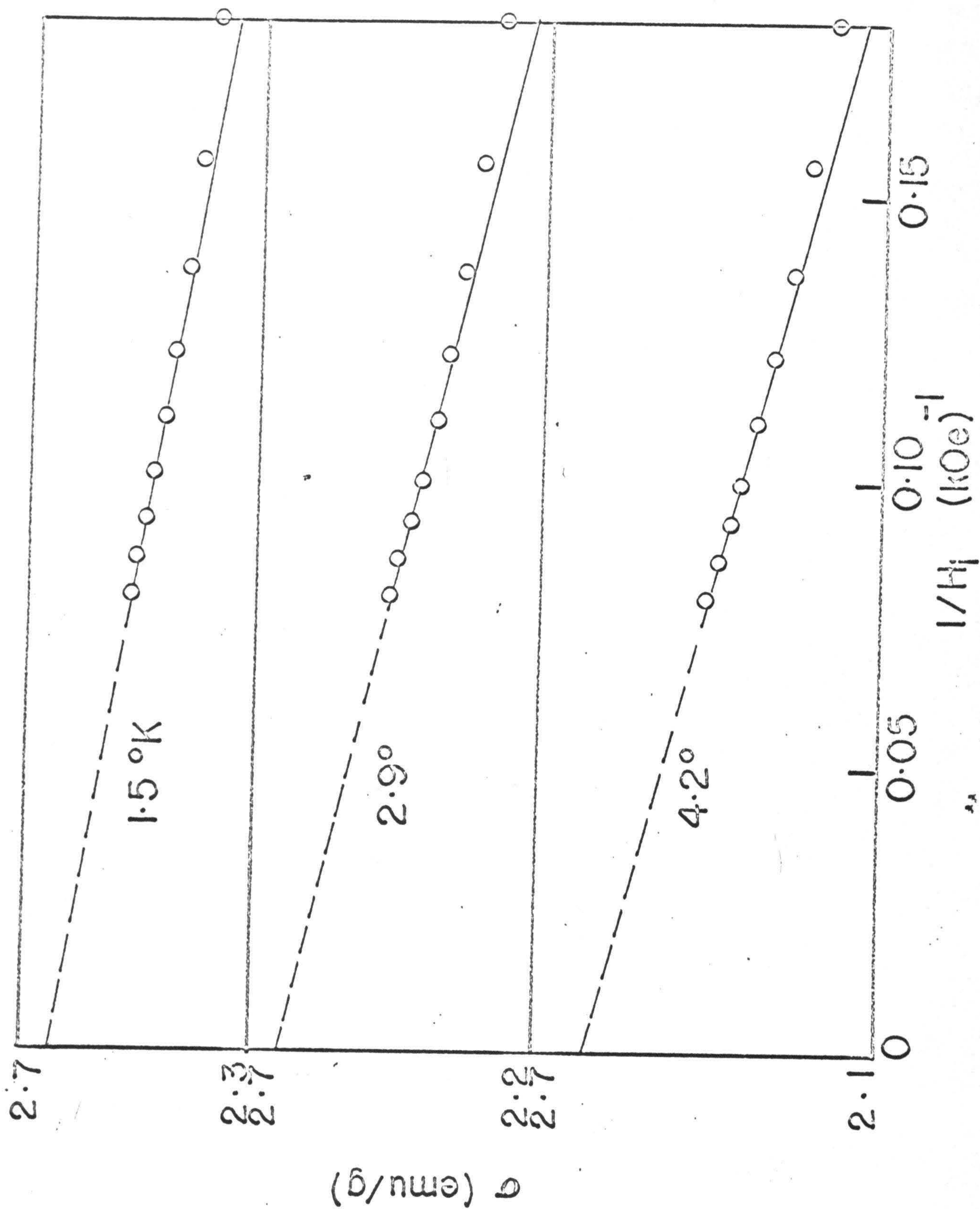




Figure 12.  $\sigma_{H_i=\infty, T}$  vs.  $T$  for quenched  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  (O),  $\text{Cu}_{0.52}\text{Ni}_{0.48}$  ( $\Delta$ ) and  $\text{Cu}_{0.54}\text{Ni}_{0.46}$  ( $\square$ ) alloys. By extrapolating  $\sigma_{H_i=\infty, T}$  to  $T=0$ , the saturation magnetization value  $\sigma_{H_i=\infty, T=0}$  was determined for each alloy.



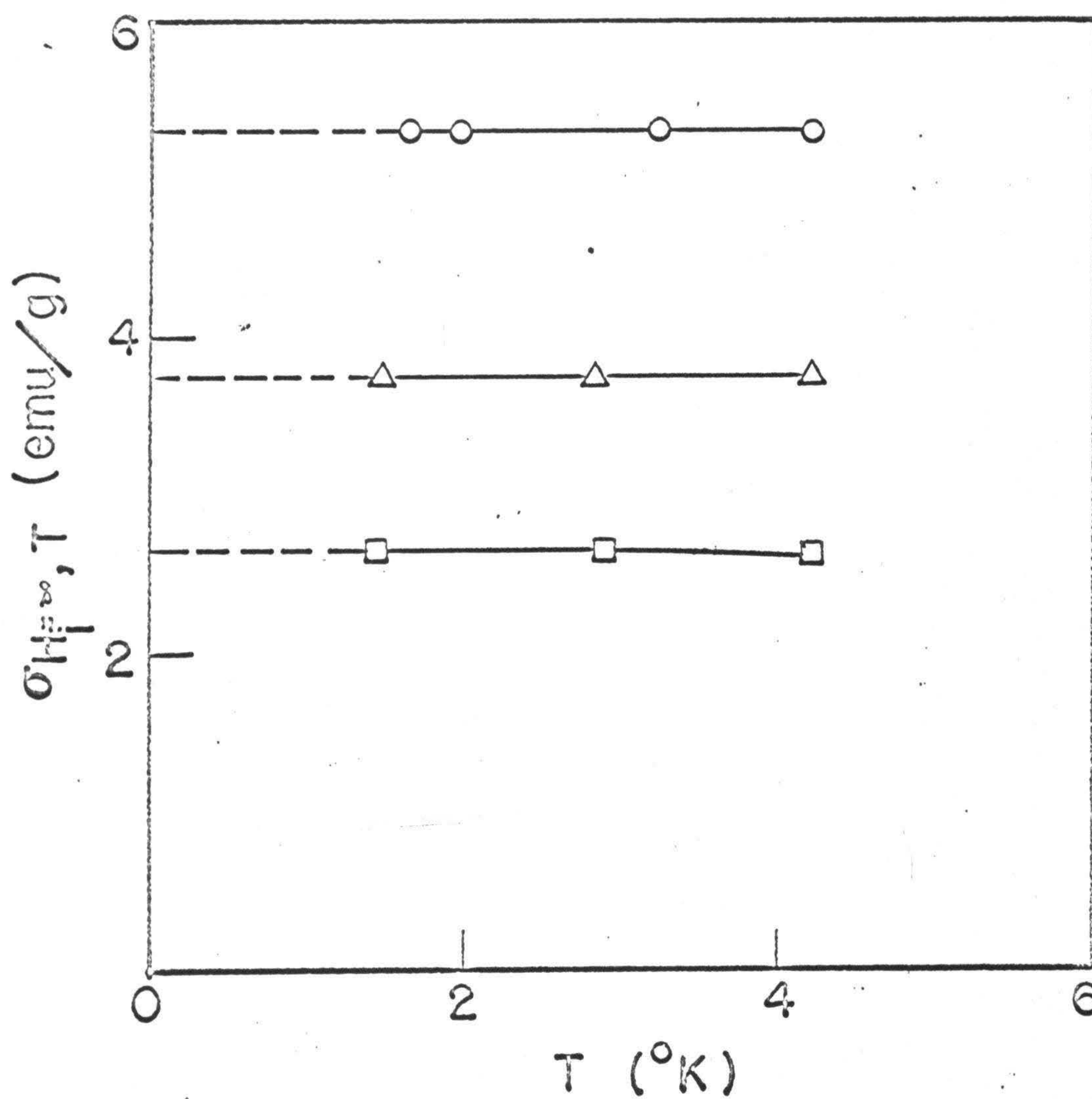




Figure 13. Magnetization data at 4.2°K for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$ . See Table 10.



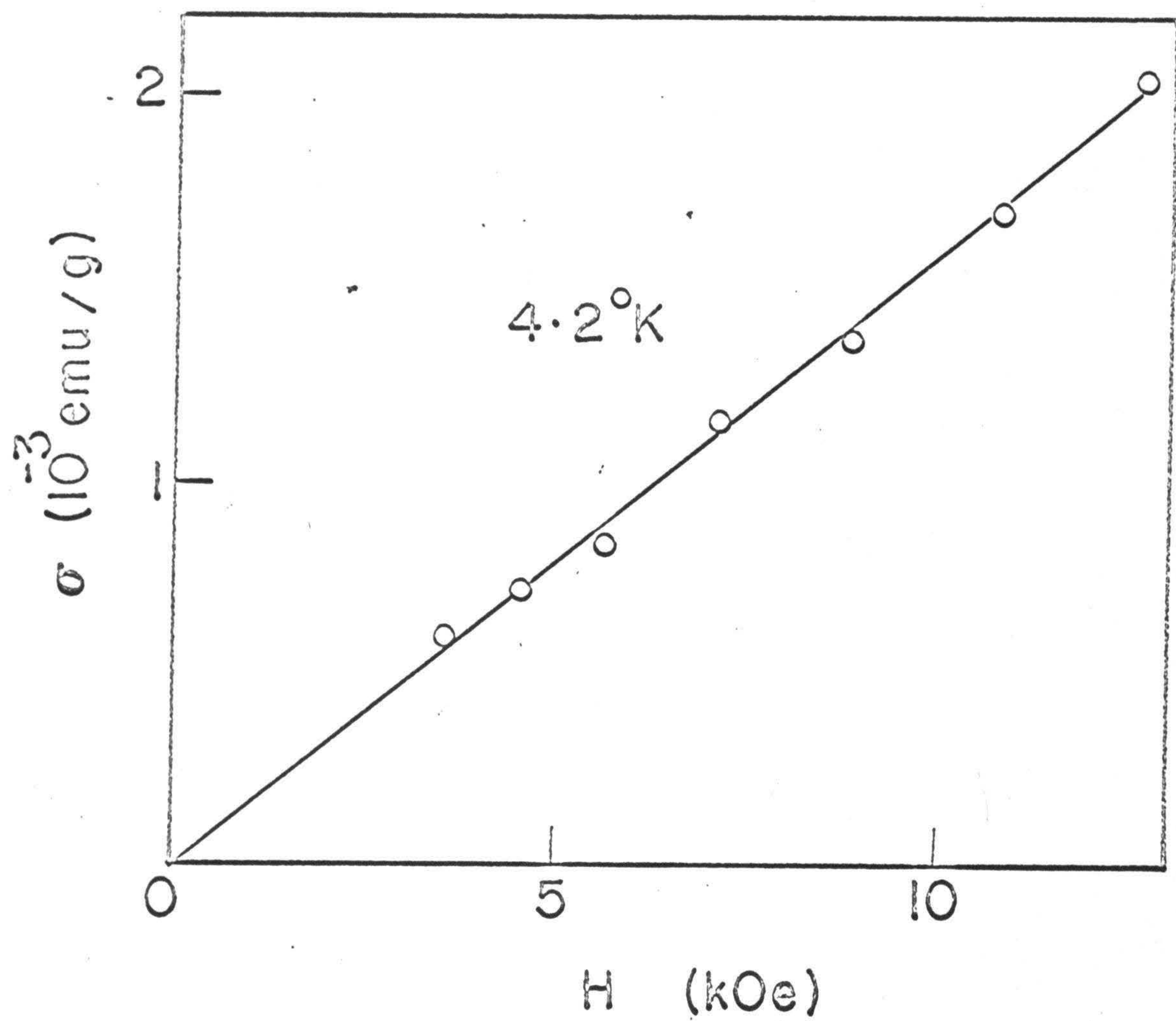
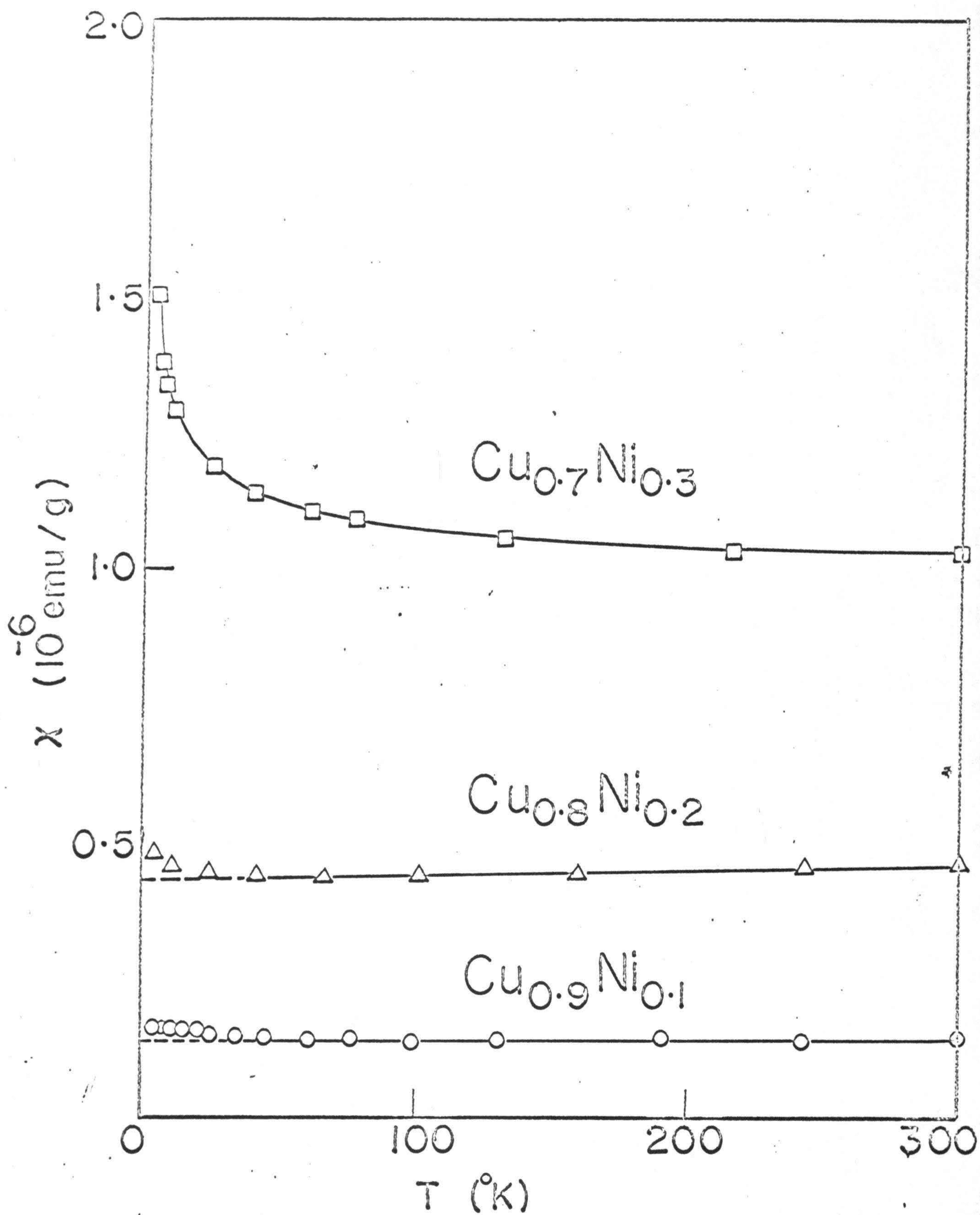




Figure 14.  $\chi$  vs.  $T$  for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$ ,  $\text{Cu}_{0.8}\text{Ni}_{0.2}$   
(from Refs. 1,2), and  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  (from Ref. 1)  
alloys.







which rises slightly with increasing temperature, and a Curie-Weiss component prominent at the lowest temperatures of measurement, but practically disappearing above about 60°K. The band susceptibility  $\chi_b$  follows the expression:  $\chi_b = (\chi_o + bT)$  with  $\chi_o = 0.14 \times 10^{-6}$  emu/g and  $b = 10^{-11}$  emu/g degree. Due to the scatter in the Curie-Weiss component of the susceptibility, it was not possible to determine the Curie-constant. However, from the absolute value of the susceptibility at 4.2°K one may estimate an Fe-impurity content of about ~4 ppm in the alloy. Alternatively, the Curie-Weiss component of the susceptibility may also be interpreted as due to small magnetic Ni-rich clusters, as has been done for a  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy.<sup>2</sup>

$\text{Cu}_{0.7}\text{Ni}_{0.3}$ : In an earlier report<sup>1</sup> the susceptibility data for the quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy, as a function of temperature between 4.2°K and ~80°K, and the magnetization data at 4.2°K in fields up to 12.6 kOe were interpreted in terms of small Ni-rich clusters with the average magnetic moment per cluster  $\mu < 3\mu_B$ . The susceptibility data in the earlier report<sup>1</sup> were graphically represented by the following Curie-Weiss type of expression:

$$\chi \text{ (emu/g)} = \chi_o + \frac{N_o c p^2 (\mu_B)^2}{3 M k (T-\theta)} \quad (7)$$

where  $\chi_o$  is the field- and temperature-independent susceptibility in emu/g,  $N_o$  ( $= 6.02 \times 10^{23}$ /mole) is Avogadro's number,  $c$  is the concentration of magnetic dipoles in atom fraction, i.e., per alloy, atom,  $p$  is the effective magnetic moment per dipole in Bohr magnetons,  $M$  is the average gram atomic weight of the alloy,



$k$  ( $= 1.38 \times 10^{-16}$  ergs/ $^{\circ}\text{K}$ ) is Boltzmann's constant, and  $\theta$  is the Weiss interaction temperature in  $^{\circ}\text{K}$ . Note that,

$$p^2 = \mu (\mu + g) \quad (8)$$

where  $\mu = gJ$  is the permanent moment/dipole in Bohr magnetons,  $g$  being the Lande splitting factor.  $J$  is the total angular momentum quantum number, i.e., the sum of the spin quantum number  $S$  and of the orbital angular momentum quantum number  $L$ . We assume  $L \ll S$ , i.e.,  $J \approx S$ ; in such a case  $g \approx 2$ .

Equation 7 was found to fit the susceptibility data between  $4.2^{\circ}\text{K}$  and  $\sim 80^{\circ}\text{K}$  with  $cp^2 = 2.62 \times 10^{-3}/\text{atom}$ ,  $\chi_0 = 1.03 \times 10^{-6}$  emu/g and  $\theta \approx -9^{\circ}\text{K}$ .

During the course of the present investigation high field magnetization measurements at  $4.2^{\circ}\text{K}$  (Table 11) were made for the same alloy, i.e., quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ . Here the  $\sigma$  vs.  $H$  graph showed a slight curvature (Fig. 15). The  $4.2^{\circ}\text{K}$  isothermal data were analyzed together with the susceptibility data in the entire temperature range of  $4.2^{\circ}\text{K}$  to  $300^{\circ}\text{K}$ , by least squares fitting of the following equation with the help of a computer program (Appendix A).

$$\sigma \text{ (emu/g)} = \chi_0 H + \frac{N_0}{M} c \mu \mu_B B \left( \mu, \frac{H}{T-\theta} \right) \quad (9)$$

where  $H$  is the applied field in Oe and  $B \left( \mu, \frac{H}{T-\theta} \right)$  is the Brillouin function, which for  $g=2$  is given by,

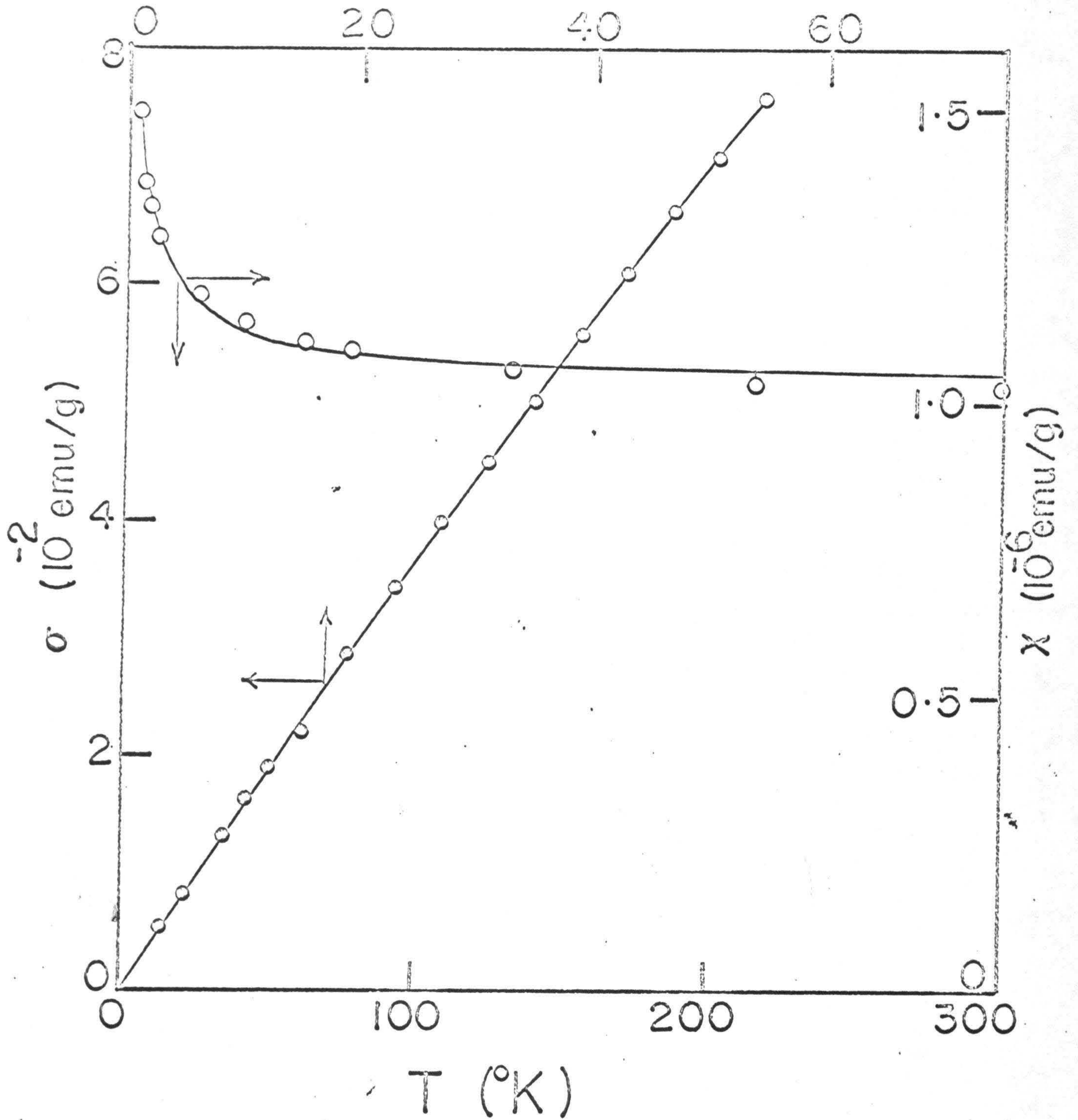


Figure 15.  $\chi$  vs.  $T$  (from Ref. 1) and  $\sigma$  vs.  $H$  at  $4.2^\circ\text{K}$  (see Table 11) for quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ . The empty and filled circles represent measured data points; the solid curves were calculated by using parameter values ( $\mu = 2.76 \mu_B$ ,  $c = 1.297 \times 10^{-4}$  clusters/alloy atom,  $\theta = -3.5^\circ\text{K}$ ,  $\chi_0 = 1.038 \times 10^{-6}$  emu/g) obtained by least squares fitting of Eq. 9.



H (kOe)

120





$$B\left(\mu, \frac{H}{T-\theta}\right) = \frac{\mu+1}{\mu} \operatorname{ctnh} \left[ (\mu+1) \frac{\mu_B H}{k(T-\theta)} \right] - \frac{1}{\mu} \operatorname{ctnh} \left[ \frac{\mu_B H}{k(T-\theta)} \right] \quad (10)$$

and all other quantities were defined in connection with Eq. 9.

The practice of using  $\theta$ , in the argument of the Brillouin function, to represent an interaction temperature has been followed by several investigators.<sup>2,3,18,19,20,21</sup> In a very simple picture  $k\theta$  would represent the energy, i.e., strength of interaction of the magnetic dipole with its magnetic environment. In the region where the  $\sigma$  vs.  $T$  plot is linear, i.e., at low fields and/or at high temperatures, the Brillouin equation of the type used here then reduces to the familiar Curie-Weiss expression (Eq. 7). At higher fields or at lower temperatures, where the  $\sigma$  vs.  $H$  graph is curved,  $\theta$  is proportional to  $\frac{\sigma T}{H}$ ; and it falls off with decreasing temperature or with increasing field. However, the use of a constant  $\theta$  value, in the sense of an average quantity over a range of fields and temperatures, has been found to be very suitable for describing magnetization data in a number of alloy systems.<sup>2,18,19</sup>

The parameter values obtained for the quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy are:  $\mu = 2.76 \mu_B$ ,  $c = 1.297 \times 10^{-4}$  clusters/alloy atom,  $\theta = -3.50^\circ\text{K}$  and  $\chi_0 = 1.038 \times 10^{-6}$  emu/g. The rmsd was  $0.026 \times 10^{-2}$  emu/g and the degree of fit (the rmsd as expressed as a percentage of the highest magnetization value used in the fitting) was  $\sim 0.34\%$ . The resultant fit is illustrated in Fig. 15.



The permanent average moment  $\bar{\mu}$  per alloy atom is estimated to be  $\approx 0.00036 \mu_B$ . Also the value of  $cp^2$ , calculated from the values of  $\mu$  and  $c$  is  $\approx 1.71 \times 10^{-3} (\mu_B)^2/\text{alloy atom}$ . The differences in the  $cp^2$  and  $\theta$  values obtained by fitting of Eq. 9, from the corresponding values obtained earlier<sup>1</sup> by fitting of Eq. 7 arise from the fact that in the earlier analysis only the susceptibility data in a narrow temperature range, i.e.,  $4.2^\circ\text{K}$  to  $\sim 80^\circ\text{K}$  were used.

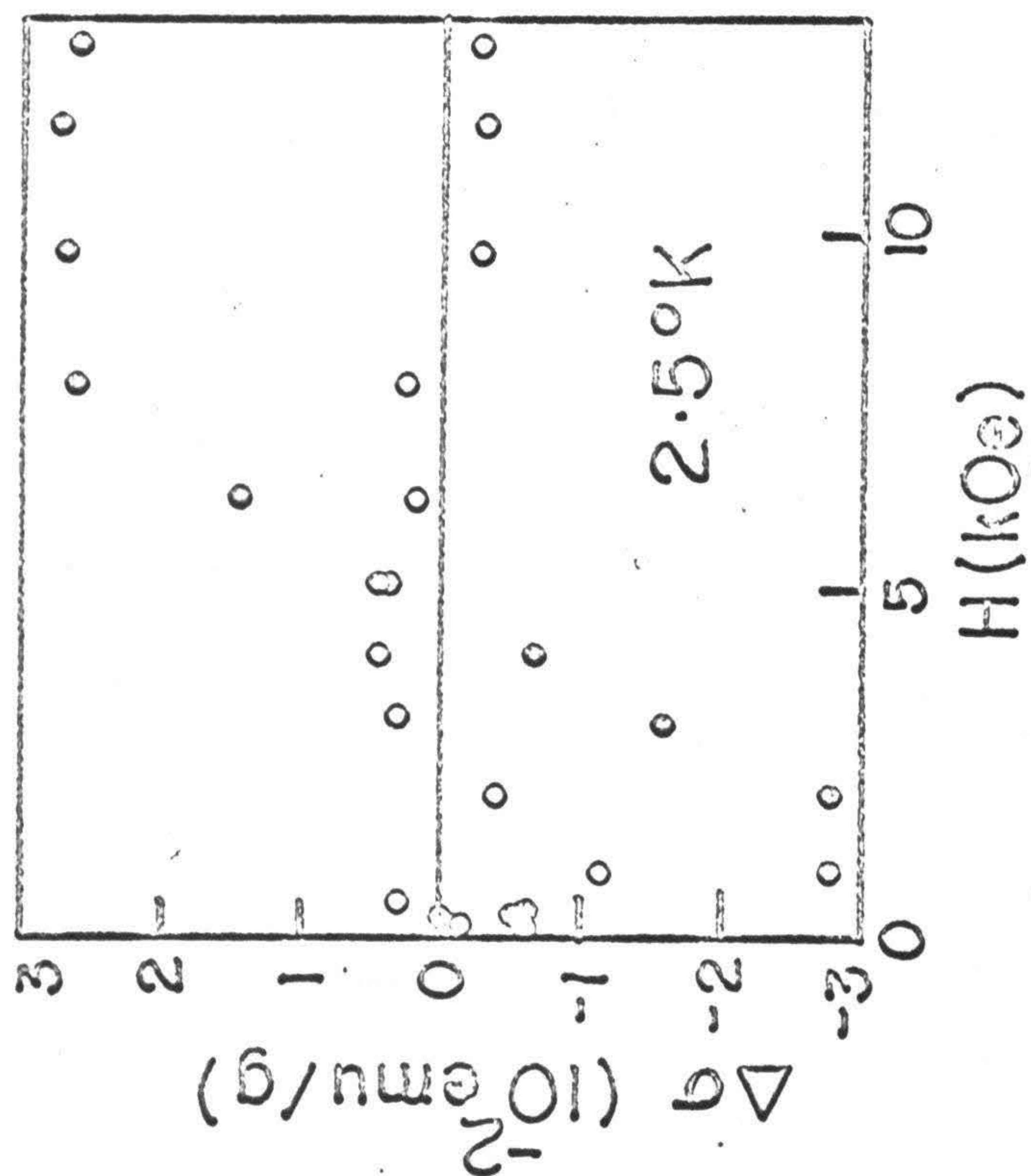
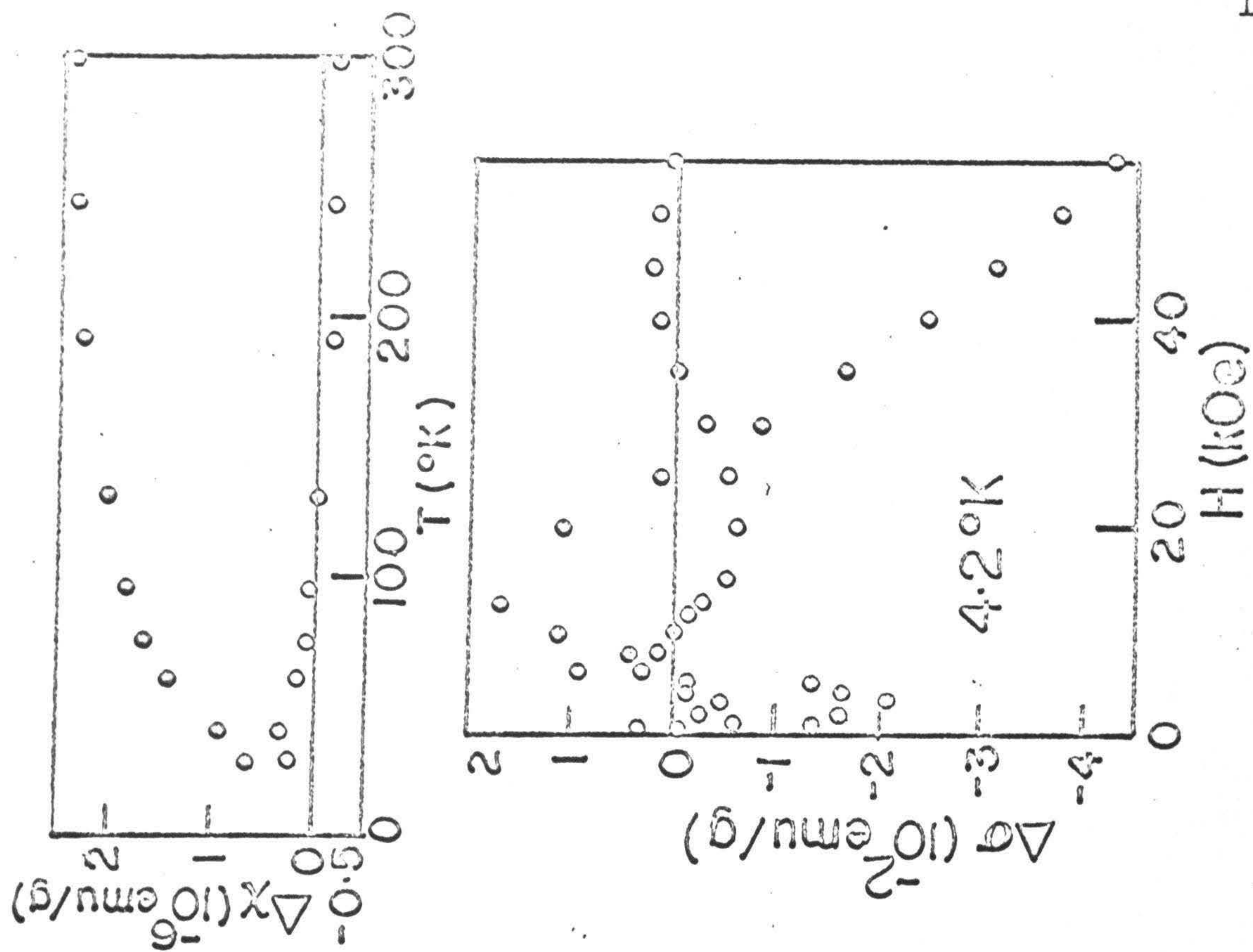
Cu<sub>0.6</sub>Ni<sub>0.4</sub>: On fitting Eq. 9 to the data for quenched Cu<sub>0.6</sub>Ni<sub>0.4</sub> the following parameter values were obtained:  $\mu = 17.1 \mu_B$ ,  $c = 3.68 \times 10^{-4}$  clusters/alloy atom,  $\theta = -0.51^\circ\text{K}$ ,  $\chi_0 = 4.25 \times 10^{-6}$  emu/g. The rmsd was, however, very high ( $1.96 \times 10^{-2}$  emu/g) and the degree of fit very poor (= 2.4%). Large systematic deviations ( $\Delta\sigma = \sigma_{\text{calculated}} - \sigma_{\text{measured}}$ ;  $\Delta\chi = \chi_{\text{calculated}} - \chi_{\text{measured}}$ ) were found between the calculated and the measured values of  $\sigma$  and  $\chi$  (at high temperatures, i.e.,  $T > 30^\circ\text{K}$ ,  $\sigma$  is proportional to  $H$  and  $\chi = \frac{\sigma}{H}$ ) at all temperatures between  $1.49^\circ\text{K}$  and  $\sim 300^\circ\text{K}$ . The deviations in  $\sigma$  at  $2.52^\circ\text{K}$  and  $4.2^\circ\text{K}$  as a function of field and the deviations in  $\chi$  as a function of temperature are illustrated in Fig. 16. A much better fit was obtained by least squares fitting of the following equation

$$\sigma = \chi_0 H + \frac{N_O}{M} c_1 \mu_1 \mu_B^B \left( \mu_1, \frac{H}{T - \theta_1} \right) + \frac{N_O}{M} c_2 \mu_2 \mu_B^B \left( \mu_2, \frac{H}{T - \theta_2} \right) \quad (11)$$



Figure 16.  $\Delta\sigma$  ( $= \sigma_{\text{calculated}} - \sigma_{\text{measured}}$ ) vs. H at 2.52°K and 4.2°K, and  $\Delta\chi$  ( $= \chi_{\text{calculated}} - \chi_{\text{measured}}$ ) vs. T for quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ . Filled circle: deviations obtained from least squares fitting of Eq. 9; empty circle: deviations obtained from least squares fitting of Eq. 11.







where  $\mu_1$  and  $\mu_2$ ,  $c_1$  and  $c_2$ ,  $\theta_1$  and  $\theta_2$  represent two average moments in  $\mu_B$ , the concentrations of the two moments in atom fractions and the corresponding Weiss temperatures in  $^{\circ}\text{K}$ . The resulting parameter values are listed in Table 35. The accuracy of  $\mu_1$  and  $\mu_2$  is estimated to be roughly  $\pm 2\%$  and  $\pm 5\%$  respectively; similar uncertainties are involved in the values of  $c_1$  and  $c_2$ . The value of  $\chi_0$  is within about  $\pm 10\%$ . As seen in Fig. 16 the systematic deviations in  $\sigma$  and  $\chi$  are reduced considerably by using Eq. 11 instead of Eq. 9. The measured and calculated results for this alloy (i.e., quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ ) are shown in Fig. 17 up to 12.6 kOe and up to 55 kOe in Fig. 18. Above about  $30^{\circ}\text{K}$  the  $\sigma$  vs.  $H$  isotherms are linear and the corresponding susceptibility values are given in Fig. 19 as a function of temperature. It is seen in Figs. 17, 18, and 19 that in the temperature range between  $\sim 2.5^{\circ}\text{K}$  and  $\sim 130^{\circ}\text{K}$  the calculated values fit the experimental data points well. The systematic deviations at  $1.49^{\circ}\text{K}$  may be interpreted as due to dipole-dipole interaction effects.

Equation 11 was also fitted to the data for the aged  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy. The parameter values are listed in Table 35, and the results shown in Figs. 18, 19, and 20. Here again a similarly good fit was obtained for a wide range of temperatures, i.e.,  $4.2^{\circ}\text{K}$  to  $\sim 300^{\circ}\text{K}$  (for the aged alloy the deviations were so large at  $1.49^{\circ}\text{K}$  that the data for  $1.49^{\circ}\text{K}$  were eliminated from the final stages of the least squares fitting operation).



Table 35. Results of analysis of data for quenched, and aged  
 $\text{Cu}_{0.6}\text{Ni}_{0.4}$

| Parameter                                                   | As-quenched<br>Condition | Aged<br>Condition      |
|-------------------------------------------------------------|--------------------------|------------------------|
| (a) Brillouin Analysis (Eq. 11)                             |                          |                        |
| Temperature range ( $^{\circ}\text{K}$ )                    | 1.49 to $\sim 300$       | 2.52 to $\sim 300$     |
| $\mu_1$ ( $\mu_B$ )                                         | 5.3                      | 5.3                    |
| $\mu_2$ ( $\mu_B$ )                                         | 23.2                     | 29.0                   |
| $c_1$ (atom fraction)                                       | $1.04 \times 10^{-3}$    | $1.11 \times 10^{-3}$  |
| $c_2$ (atom fraction)                                       | $1.83 \times 10^{-4}$    | $1.93 \times 10^{-4}$  |
| $\theta_1$ ( $^{\circ}\text{K}$ )                           | - 5.2                    | - 2.8                  |
| $\theta_2$ ( $^{\circ}\text{K}$ )                           | + 0.1                    | + 0.5                  |
| $\chi_0$ (emu/g)                                            | $1.80 \times 10^{-6}$    | $1.00 \times 10^{-6}$  |
| rmsd (emu/g)                                                | $4.519 \times 10^{-3}$   | $5.634 \times 10^{-3}$ |
| rmsd (%) <sup>*</sup>                                       | 0.55%                    | 0.56%                  |
| (b) Curie-Weiss Analysis (Eq. 7)                            |                          |                        |
| $cp^2$ in (Bohr<br>magneton) <sup>2</sup><br>per alloy atom | 0.157                    | 0.204                  |
| $\theta$ ( $^{\circ}\text{K}$ )                             | - 0.27                   | + 0.71                 |
| $\chi_0$ (emu/g)                                            | $1.612 \times 10^{-6}$   | $1.154 \times 10^{-6}$ |
| rmsd (emu/g)                                                | $2.669 \times 10^{-6}$   | $1.558 \times 10^{-6}$ |
| rmsd (%) <sup>*</sup>                                       | 1.48%                    | 0.29%                  |

\* The rmsd as expressed in percents of the highest magnetization (or, susceptibility) value used in the fitting.



Figure 17. Magnetization vs. field (Table 12) at temperatures indicated for quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ . Empty circles: measured data; lines were calculated with parameters values from least squares fitting and listed in Table 35a.



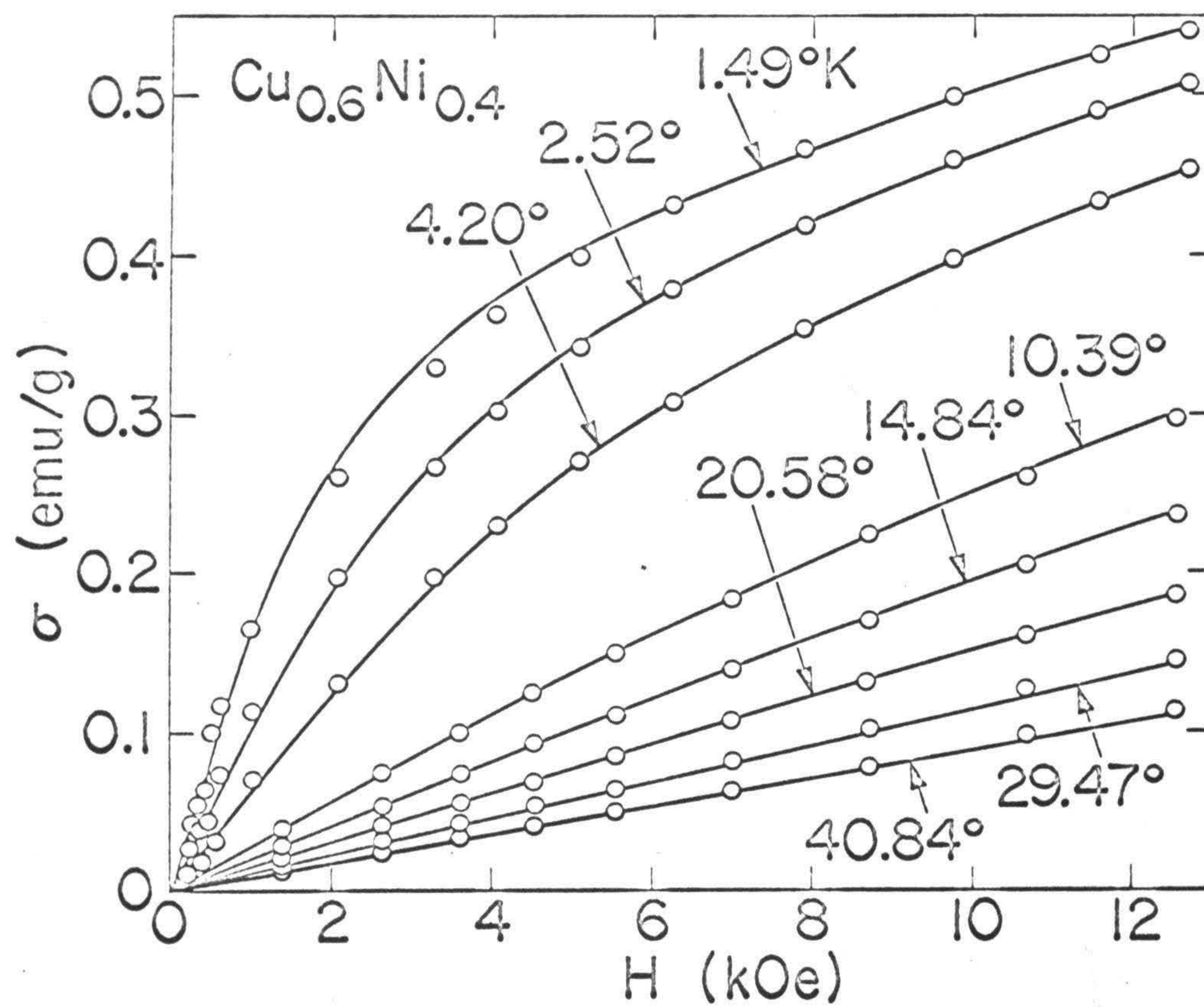




Figure 18. Magnetization vs. field up to 55 kOe at 4.2°K in both the as-quenched and the aged condition for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  (Tables 12 and 13). Open circles show measured data points in the as-quenched condition, filled circles in the aged condition. Lines were calculated with parameter values (Table 35[a]) from least squares fitting of Eq. 11.



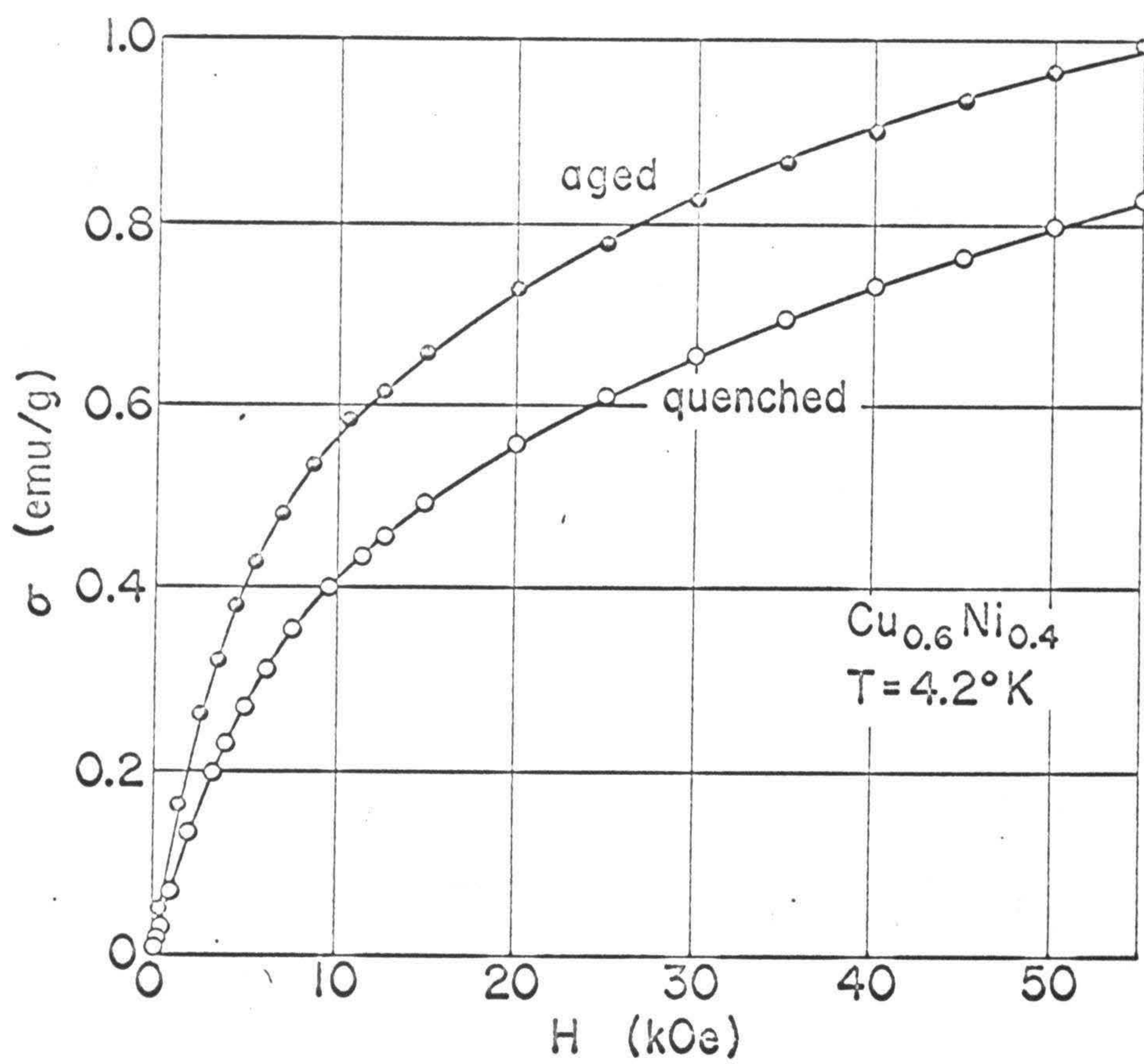




Figure 19. Susceptibility vs. temperature for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  in both the as-quenched and aged condition. Filled and empty circles show measured values, lines were calculated with parameter values (Table 35[a]) from least squares fitting of Eq. 11.



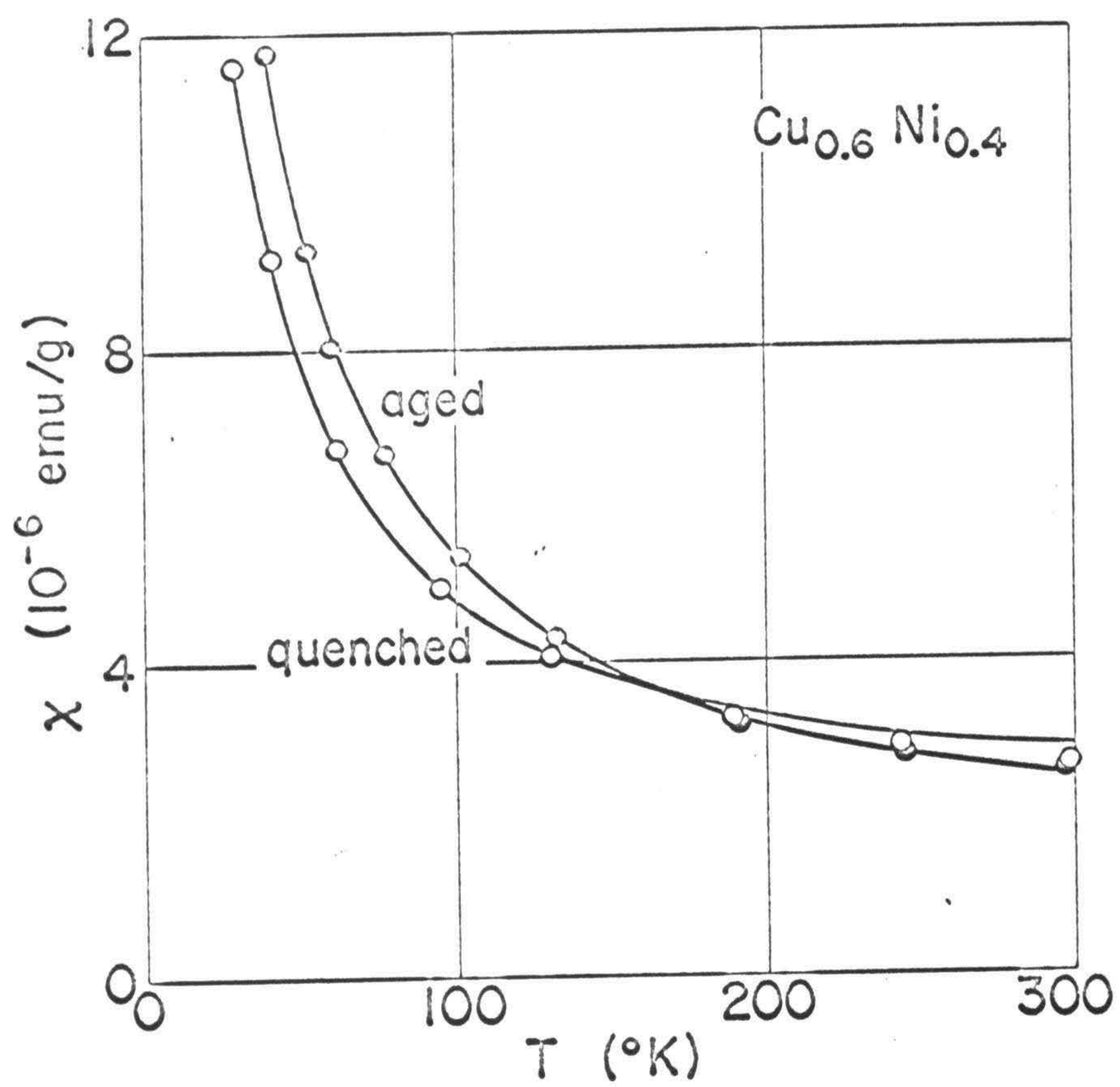
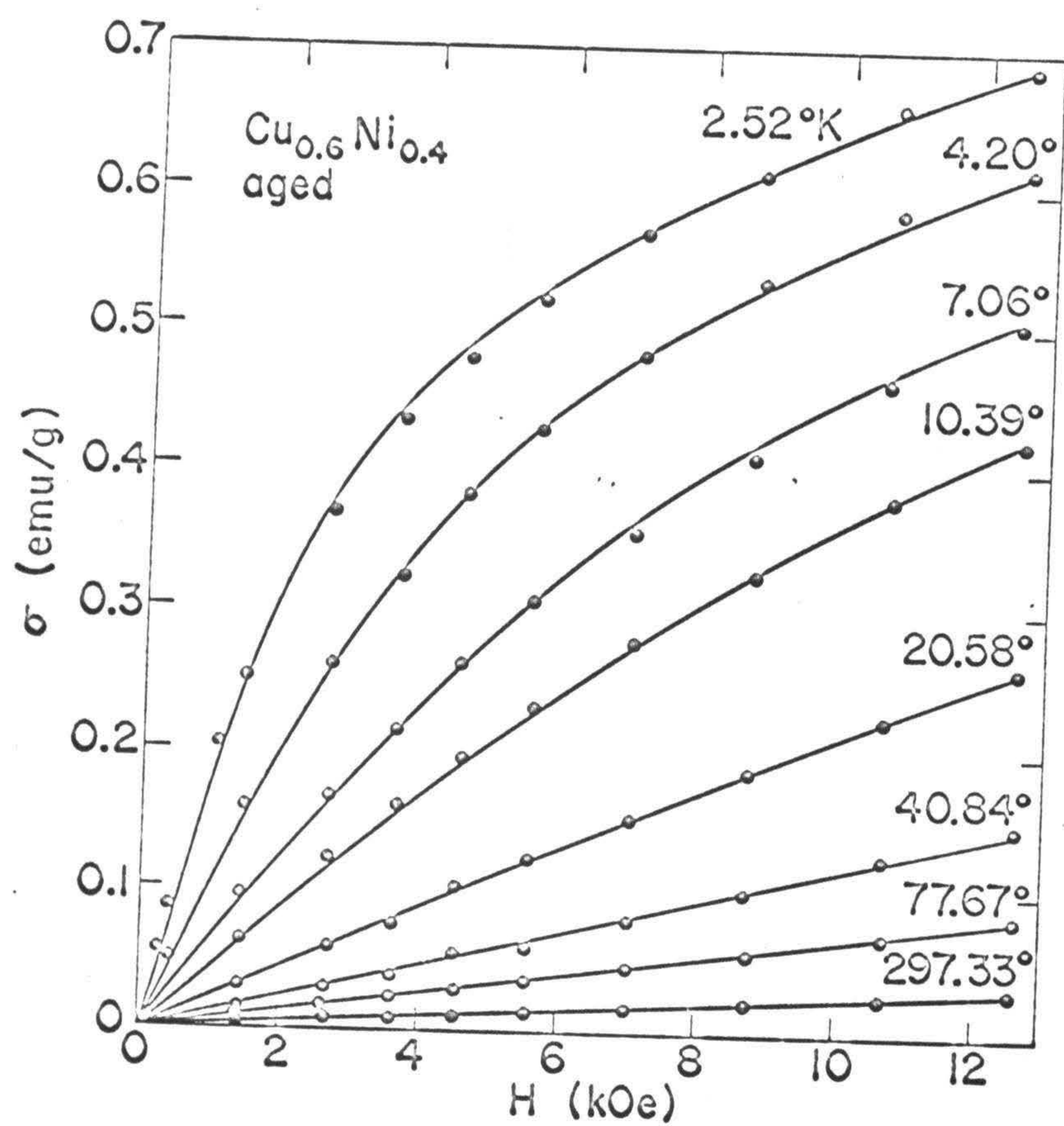




Figure 20. Magnetization vs. field at temperatures indicated, for aged  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ . Filled circles show experimental data (Table 13), lines calculated with parameter values (Table 35[a]) from least squares fitting of Eq. 11.







An important question that arises now is whether the results from the fitting of Eq. 11 to the data for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  represent a true bimodal cluster distribution as shown in Fig. 21(a). One may argue that a better rmsd and less systematic deviations were obtained in this case, than when Eq. 10 was fitted, simply because more parameters were used, even though the cluster distribution for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  is actually symmetrical, e.g., Gaussian, as shown in Fig. 21(b). To examine this possibility, a Gaussian distribution of the type sketched in Fig. 21(b) was assumed. The normalized Gaussian function has the form:

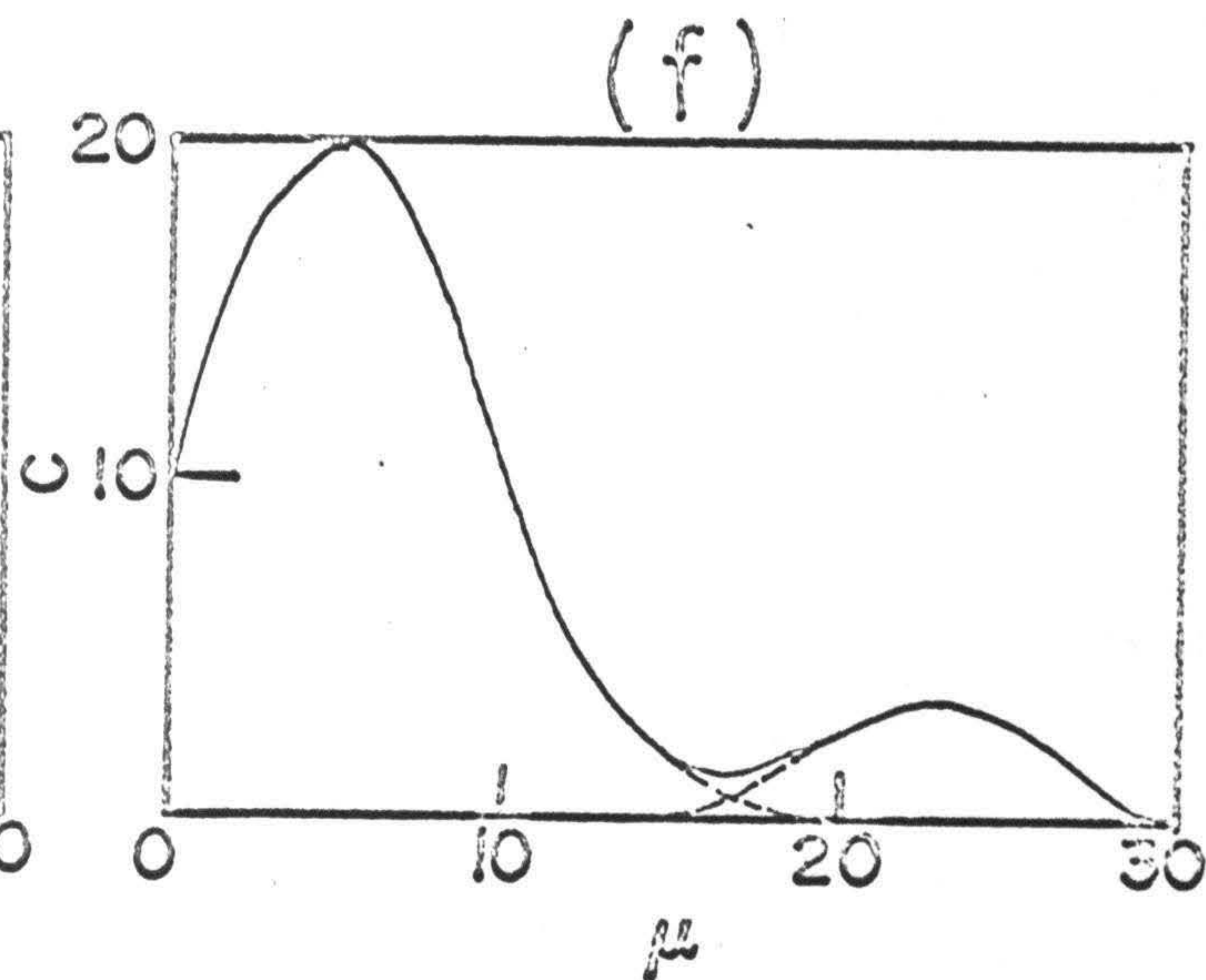
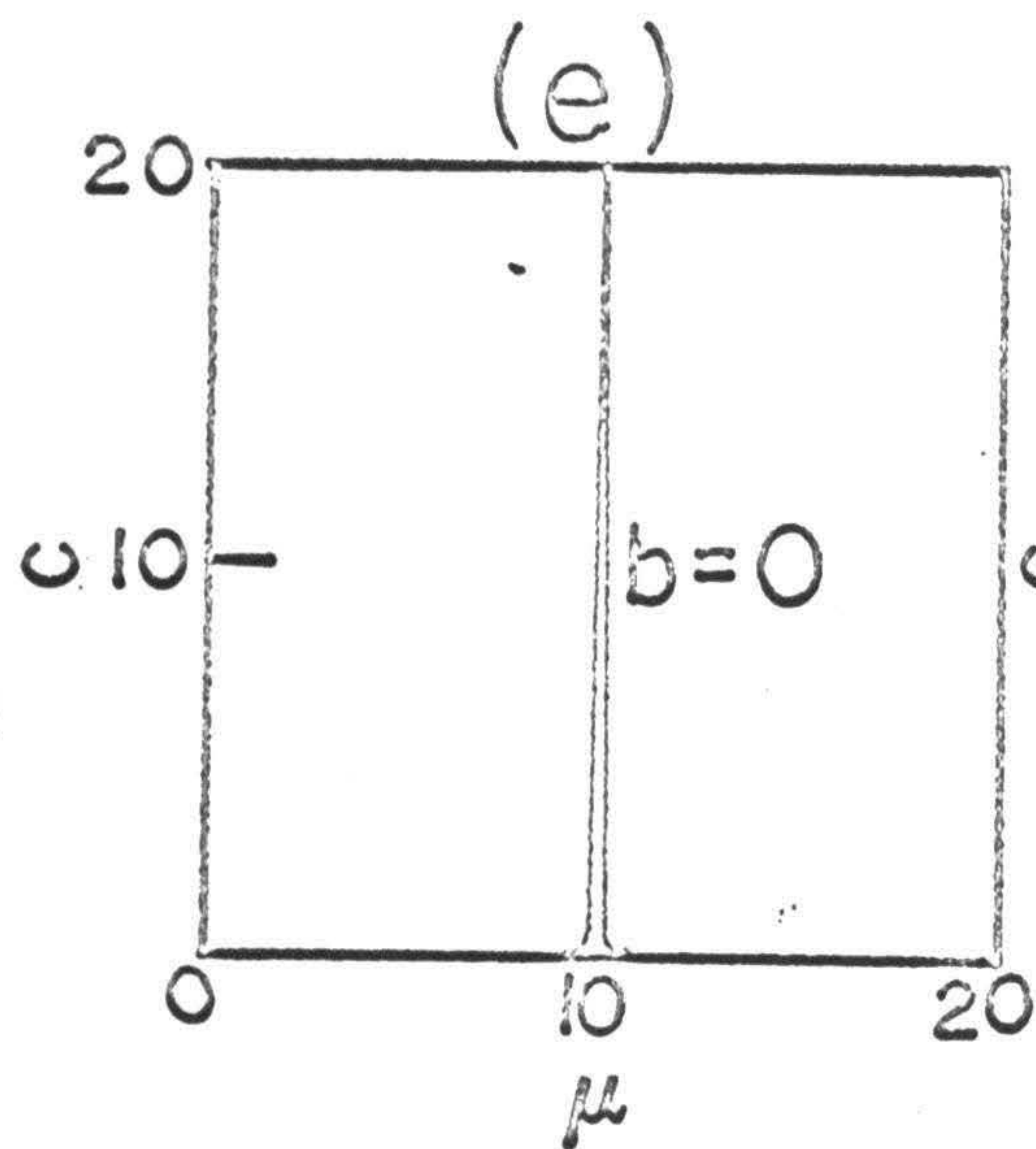
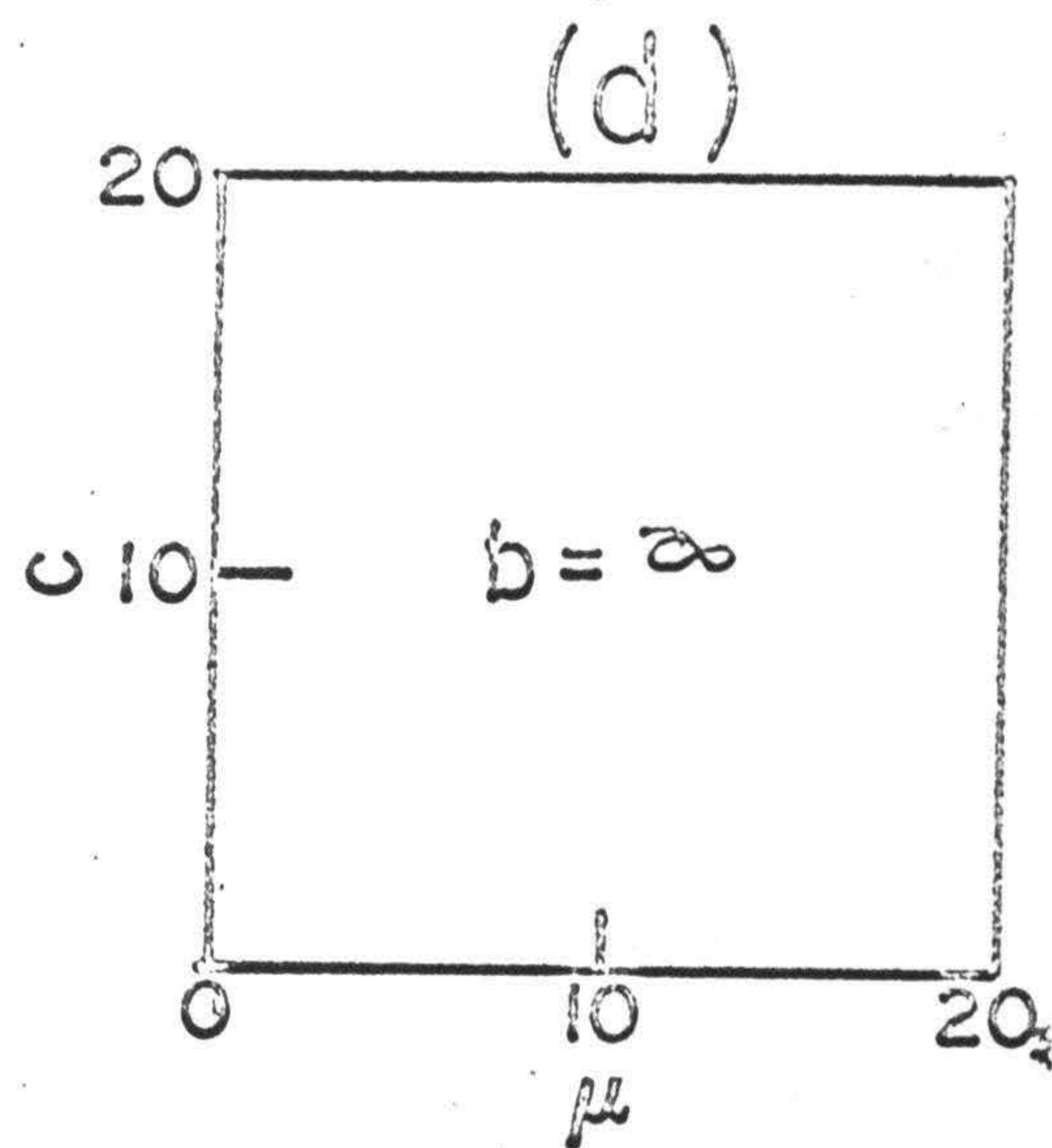
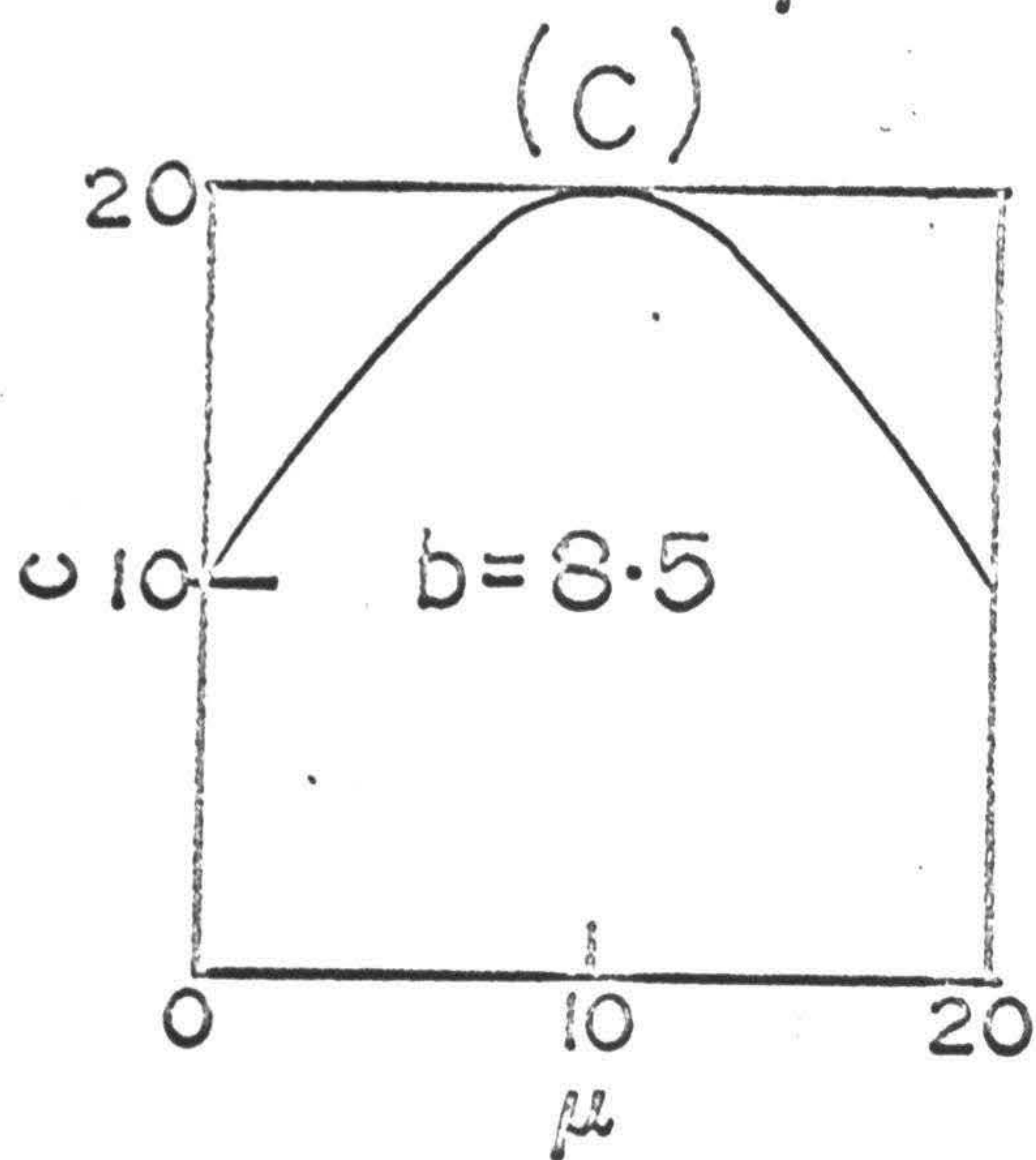
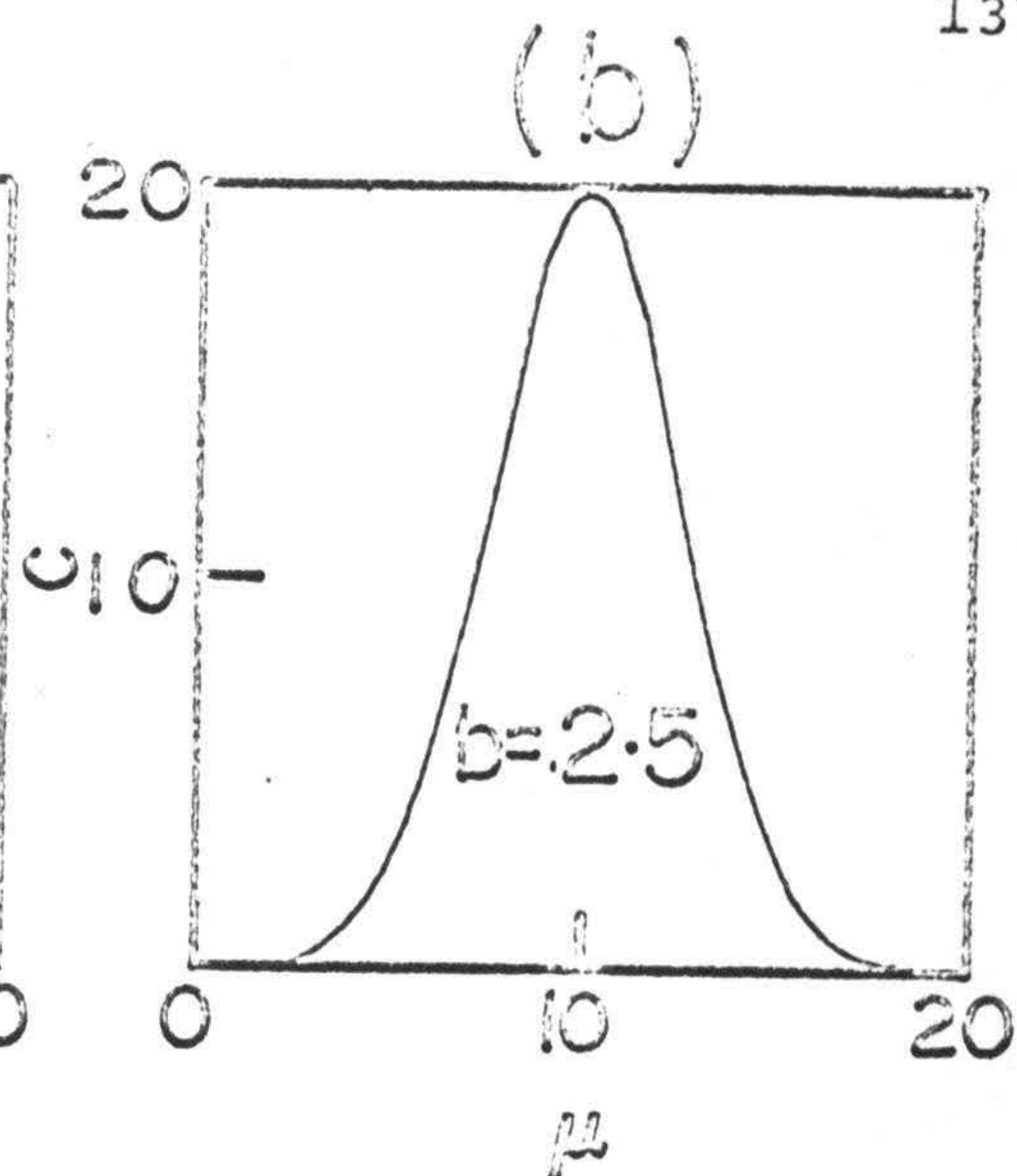
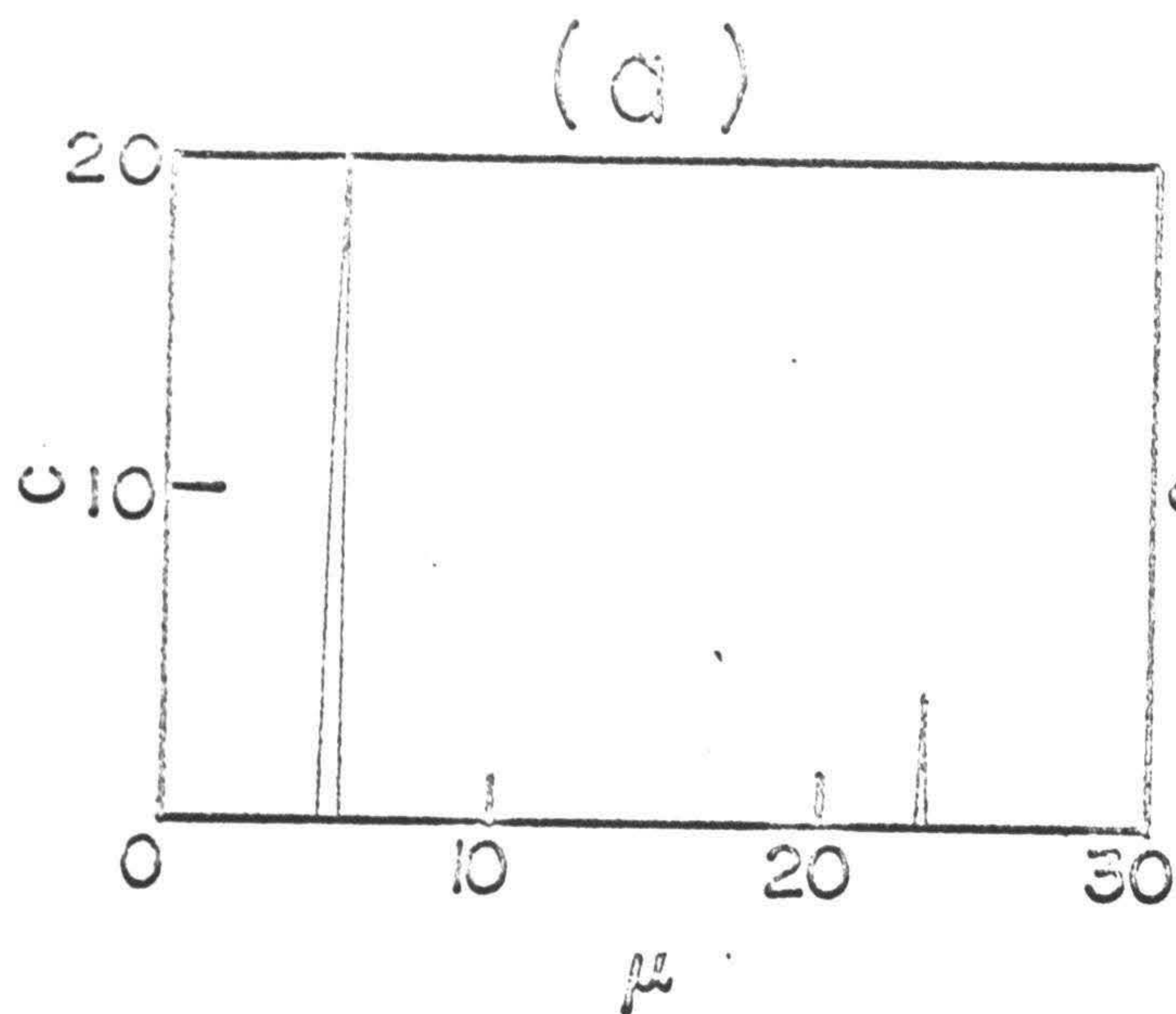
$$c = f(\mu) = \frac{1}{b\sqrt{2\pi}} \exp \left[ -\frac{1}{2} \frac{(\mu-a)^2}{b^2} \right] \quad (12)$$

where  $b$  is the standard deviation and  $a$  is the distance of the center of symmetry from the origin. The Gaussian, for the present purpose, was taken to be symmetrical about  $\mu = 10 \mu_B$  (Giant moments of this size have been reported by Kouvel et al.<sup>22</sup> for paramagnetic Cu-Ni alloys for Ni concentrations between 44 and 32 at%). The standard deviation  $b$  was chosen to be 2.5, so that the value of the Gaussian (i.e., the concentration) is nearly equal to zero for  $\mu = 0$  and  $\mu = 20$ . Magnetization curves at  $T = 1^\circ\text{K}$ ,  $10^\circ\text{K}$  and  $100^\circ\text{K}$  were synthesized for fields up to 50 kOe. First Eq. 9 (single moment) and then Eq. 11 (two moments) were fitted to these synthesized magnetization curves. The rmsd and the systematic deviations were found to be considerably lower in the second case. Clearly, a better rmsd value,



Figure 21. Schematic representation of various possible types of cluster distribution. (a) bimodal; (b) Gaussian (standard deviation,  $b = 2.5$ ); (c) Gaussian, ( $b = 8.5$ ); (d) Gaussian in the limit,  $b = \infty$ ; (e) Gaussian in the limit,  $b = 0$ ; (f) suggested cluster distribution in quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ .







obtained with the use of Eq. 11 instead of Eq. 9, does not in itself necessarily imply a bimodal distribution. The ratio of  $\mu_2 : \mu_1$  was found in the above analysis with Eq. 11 to be  $\sim 1.7$ . This value is significantly smaller than the corresponding value of  $\sim 4.4$  for the as-quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy. To examine whether a larger  $\mu_2 : \mu_1$  ratio can be obtained by changing the standard deviation  $b$ , a cluster distribution of the type shown in Fig. 21(c) ( $b = 8.5$ ) was assumed. For this case the ratio of  $\mu_2 : \mu_1$  was found to be  $\sim 1.6$ . In one limiting case, when  $b \approx \infty$  (Fig. 21(d)), a very interesting result was obtained; the values of  $\mu_1$  and  $\mu_2$  obtained from the fitting of Eq. 11 approached each other and the value of  $\mu$  obtained from the fitting of Eq. 9, i.e.,  $\mu_1 = \mu_2 = \mu$ . The other limiting case of the Gaussian, when  $b \approx 0$ , is illustrated in Fig. 21(e) and this corresponds again to the condition  $\mu_1 = \mu_2 = \mu$ . From the above examples, it does not seem likely that in the case of  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ , where a large  $\mu_2/\mu_1$  ratio was obtained by least squares fitting, a single Gaussian can suitably describe the cluster distribution. It is more plausible that  $\mu_1$  and  $\mu_2$  represent average moments for two symmetrical distributions. In Fig. 21(f) the ratio of the areas under the two symmetrical distributions shown roughly corresponds to the ratio of  $c_1$  and  $c_2$  in Table 35(a) and the values  $\mu_1$  and  $\mu_2$  also correspond to those obtained for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ . Whether or not the actual moment distribution in the alloy has two maxima, as in Fig. 21(f) can not be decided on the basis of the fitting, since the widths of the two symmetrical distributions are not known.



The average moment per alloy atom  $\bar{\mu} = c_1\mu_1 + c_2\mu_2$ . With the parameter values in Table 35(a) for the as-quenched state one obtains  $\bar{\mu} = 0.0097 \mu_B$ . The corresponding value for the aged condition is  $0.0115 \mu_B$ .

As noted earlier, fitting of Eq. 11 to the data gives a value of  $\chi_0$ , the temperature and field independent susceptibility. This term  $\chi_0$ , because of the fact that it contributes only a small amount to the total magnetization at low temperatures, is not very accurately determined from a fitting (of Eq. 11) in which a large number of data points taken at low temperatures is used. The value of  $\chi_0$  was determined much more accurately by fitting of Eq. 7 to the susceptibility vs. temperature data (Fig. 22). The corresponding parameter values are listed in Table 35(b). The  $\chi_0$  values so obtained are slightly different from those obtained by fitting Eq. 11 (Table 35[a]).

## 2. Cu-Ni-Fe ( $\sim 1$ at % Fe; 0, 10, 20 at % Ni).

The results of magnetization measurements for the quenched  $\text{Cu}_{0.99}\text{Fe}_{0.01}$ ,  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$ , and  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  alloys are given in Tables 14, 15, and 16.  $\sigma^2$  vs.  $\frac{H_i}{\sigma}$  graphs at low applied fields (down to  $\sim 16$  Oe) indicate for the  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  alloy a remanence temperature  $T_r \approx 2.8 \pm 1.4^\circ\text{K}$  as seen in Fig. 23. In the case of the  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$  alloy, measurements were made at applied fields as low as 32 Oe and the remanence temperature is estimated to be  $3.1 \pm 1.1^\circ\text{K}$  (Fig. 24). For the  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  alloy (Fig. 25) no remanence is observable, down to  $1.57^\circ\text{K}$ .



Figure 22.  $\frac{1}{X_i - X_0}$  vs. T graphs for quenched and aged  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ . The straight line represents values calculated by using the parameters listed in Table 35b. These parameters were obtained from least squares fitting to Eq. 7. The value of  $X_0$  was so adjusted in each case as to give a linear  $\frac{1}{X_i - X_0}$  vs. T plot.



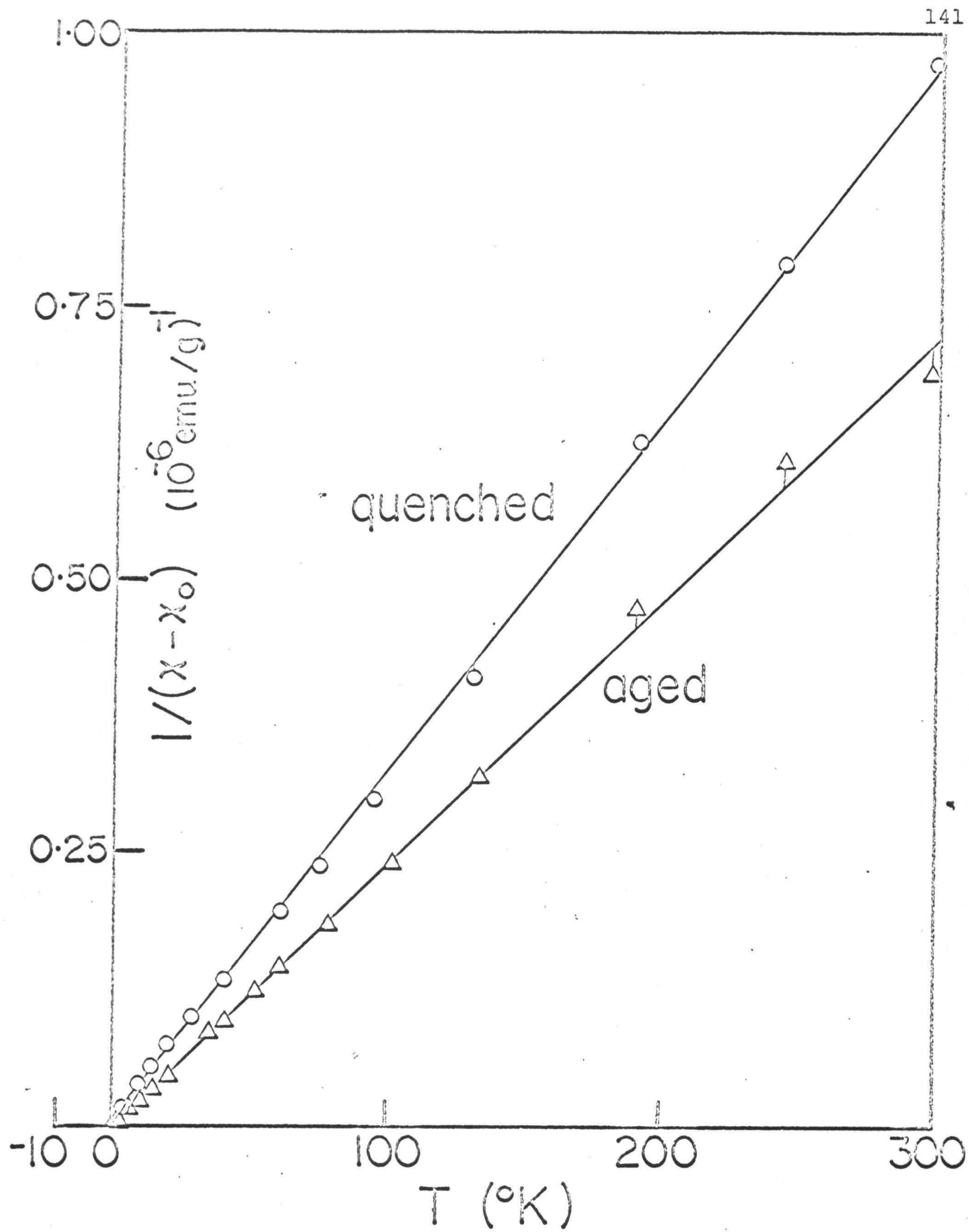




Figure 23.  $\sigma^2$  vs.  $\frac{H_i}{\sigma}$  graphs for  $\text{Cu}_{0.99}\text{Fe}_{0.01}$ . The remanence temperature  $T_r$  is estimated to be  $2.8 \pm 1.4^\circ\text{K}$ .



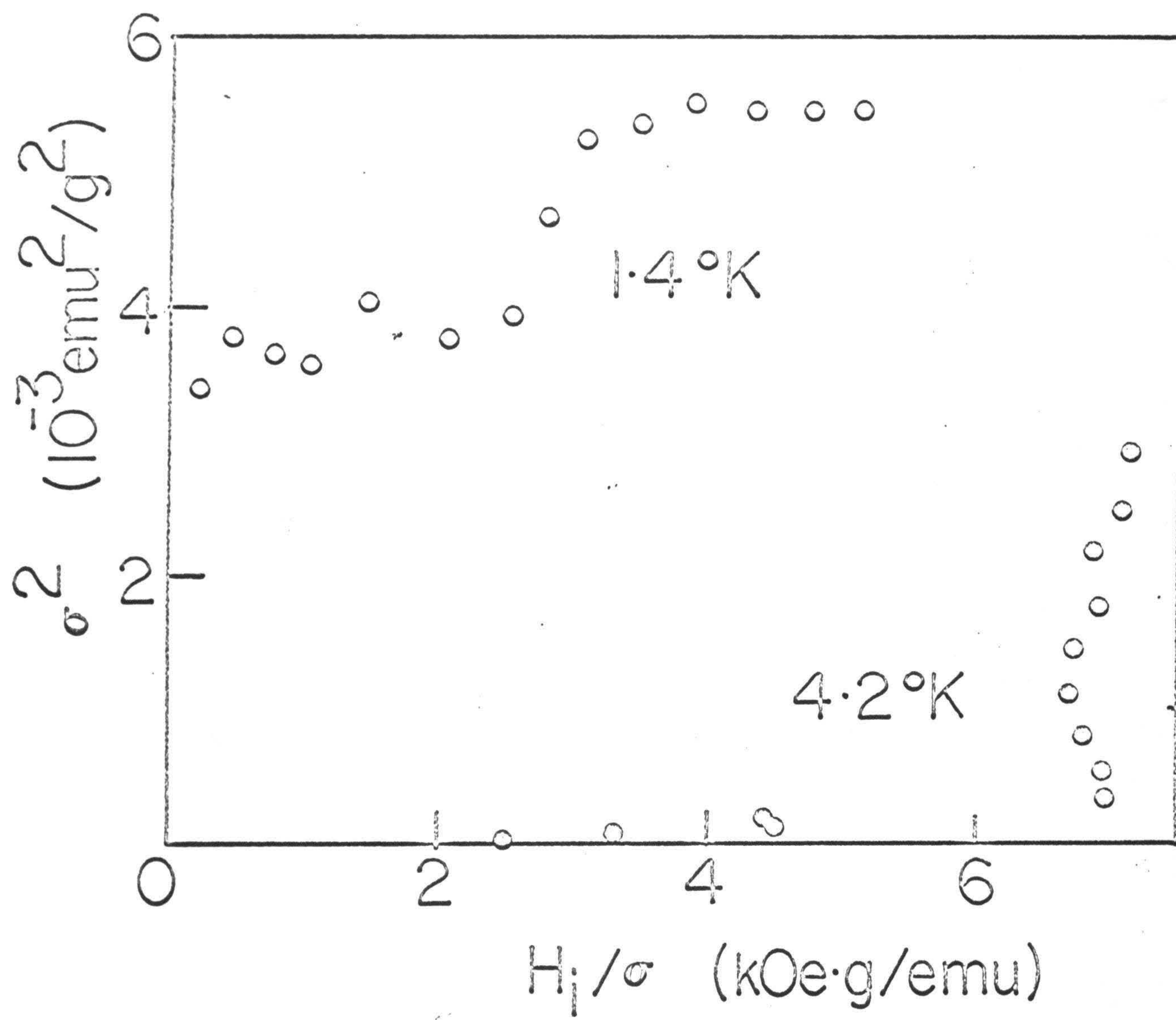




Figure 24.  $\sigma^2$  vs.  $\frac{H_i}{\sigma}$  graphs for quenched  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$ .  
The remanence temperature is estimated to be  
 $3.1 \pm 1.1^\circ\text{K}$ .



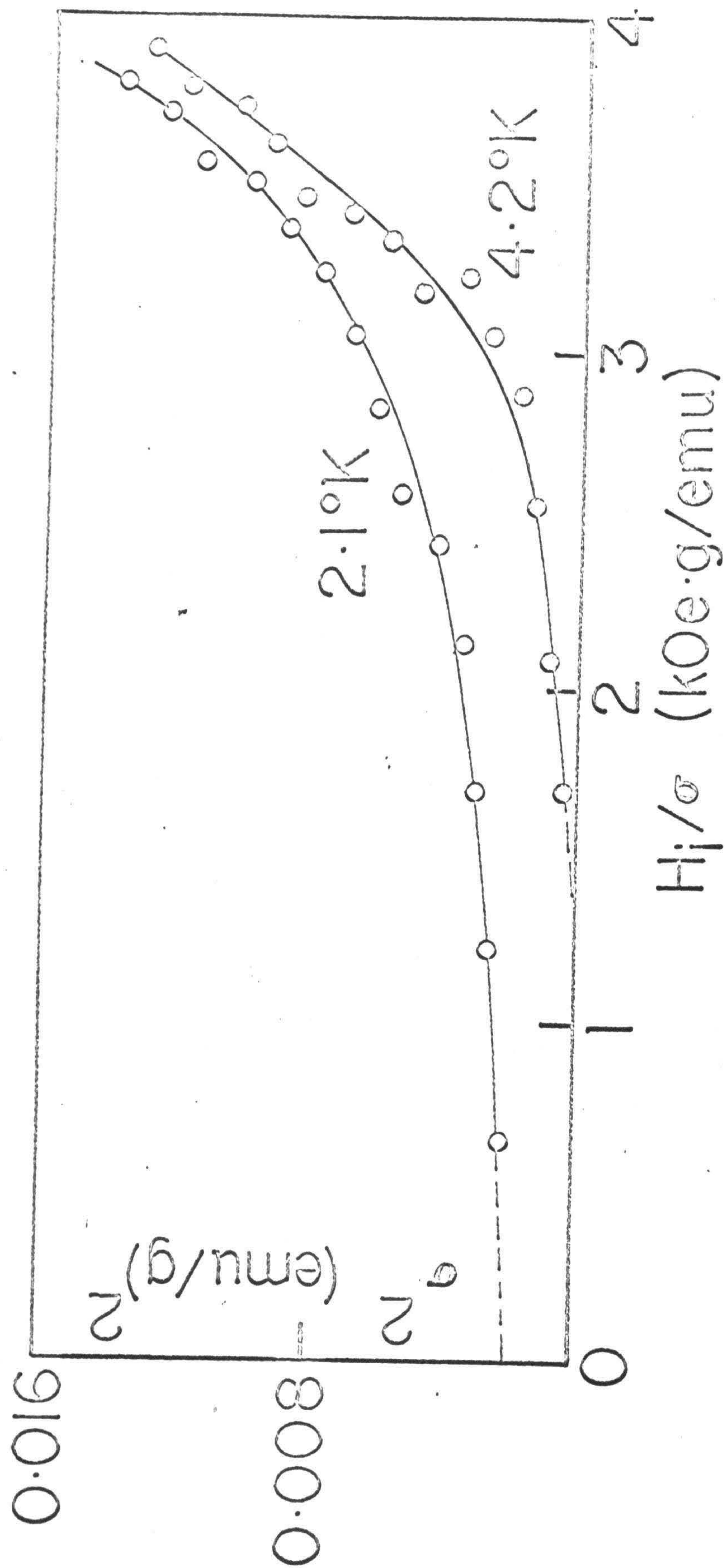
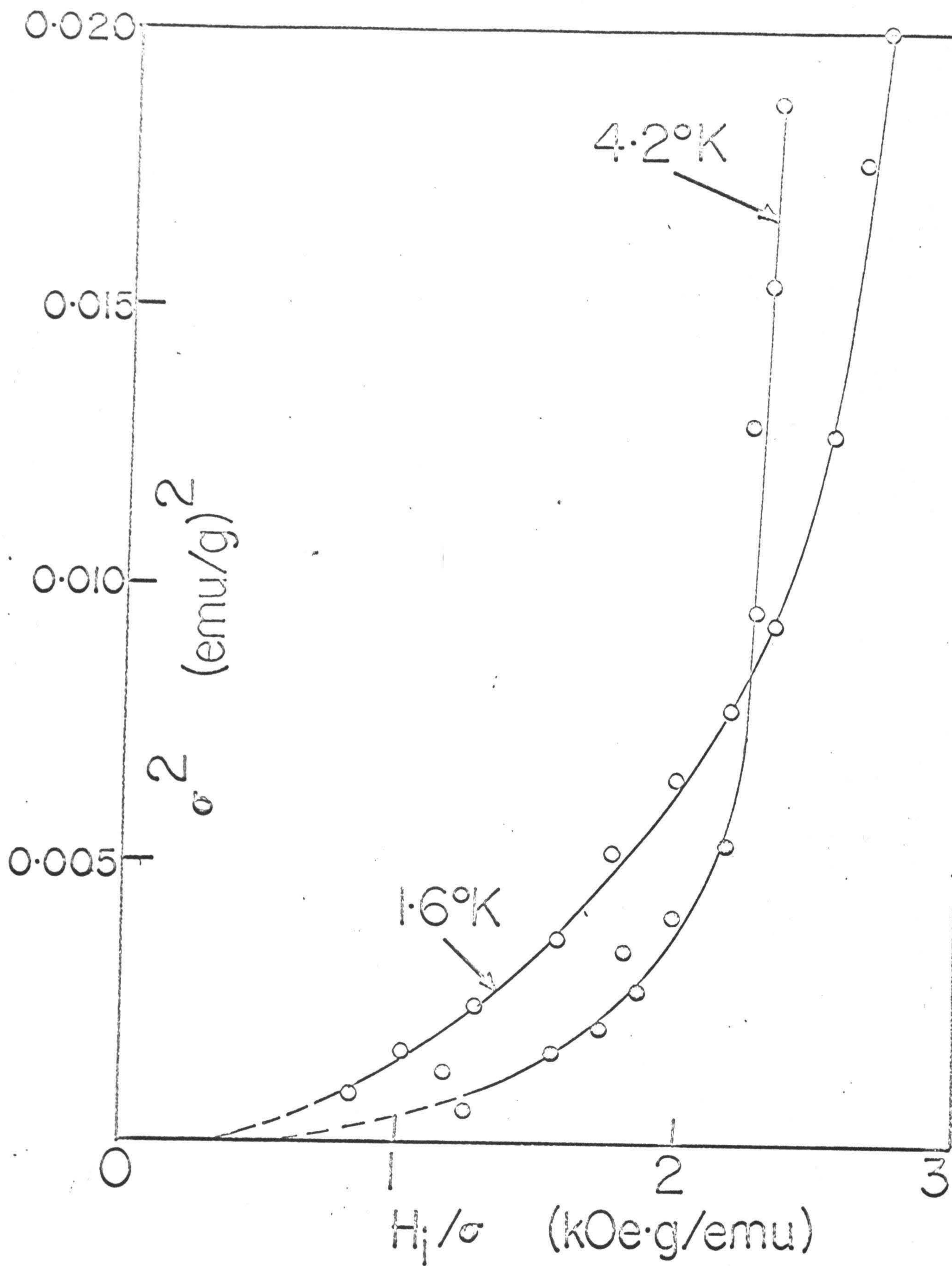




Figure 25.  $\sigma^2$  vs.  $\frac{H_i}{\sigma}$  graphs for quenched  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$ .  
No remanence is observed, in fields as low as 26 Oe,  
even at 1.57°K.







For all three alloys, the  $\sigma$  vs.  $H$  graphs show curvature at low temperatures ( $T < 30^\circ\text{K}$ ; Figs. 26, 27, 28) indicating the presence of magnetic clusters.

A maximum in the magnetization of the  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  alloy (Fig. 29) is found around  $4.3^\circ\text{K}$  when measured in an applied field of 1000 Oe. At lower temperatures the magnetization values measured after cooling in a magnetic field are characteristically higher than those obtained after the specimen was cooled in zero field. For the  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$  alloy, the magnetization data between  $4.2$  and  $1.45^\circ\text{K}$  in an applied field of 700 Oe are also systematically higher (Fig. 30) when measured after cooling the specimen in the field than after cooling it in zero applied field. A flat maximum is found in the magnetization for the  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  alloy around  $3^\circ\text{K}$  (Fig. 31) in an applied field of 1000 Oe. However, the measurements do not show any difference, within the experimental accuracy, between the magnetization values obtained after cooling the specimen in a magnetic field and those obtained after cooling in zero field.

### 3. Cu-Fe ( $\sim 100$ to $\sim 500$ ppm).

The magnetization data for a Cu-Fe alloy with 108 ppm Fe, in the temperature range of  $1.3^\circ$  to  $32.5^\circ\text{K}$  and in fields up to  $H = 70$  kOe, were supplied to us by Dr. R. Tournier<sup>6</sup> in graphical form. Thirty points were taken from the graphs, at various temperatures and fields, to construct five isotherms. These data



Figure 26.  $\sigma$  vs.  $H$  for quenched  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  at temperatures indicated. The data, at a given temperature, were obtained by cooling the specimen in an applied field of 12.6 kOe and then going down in field. See Table 14(a).



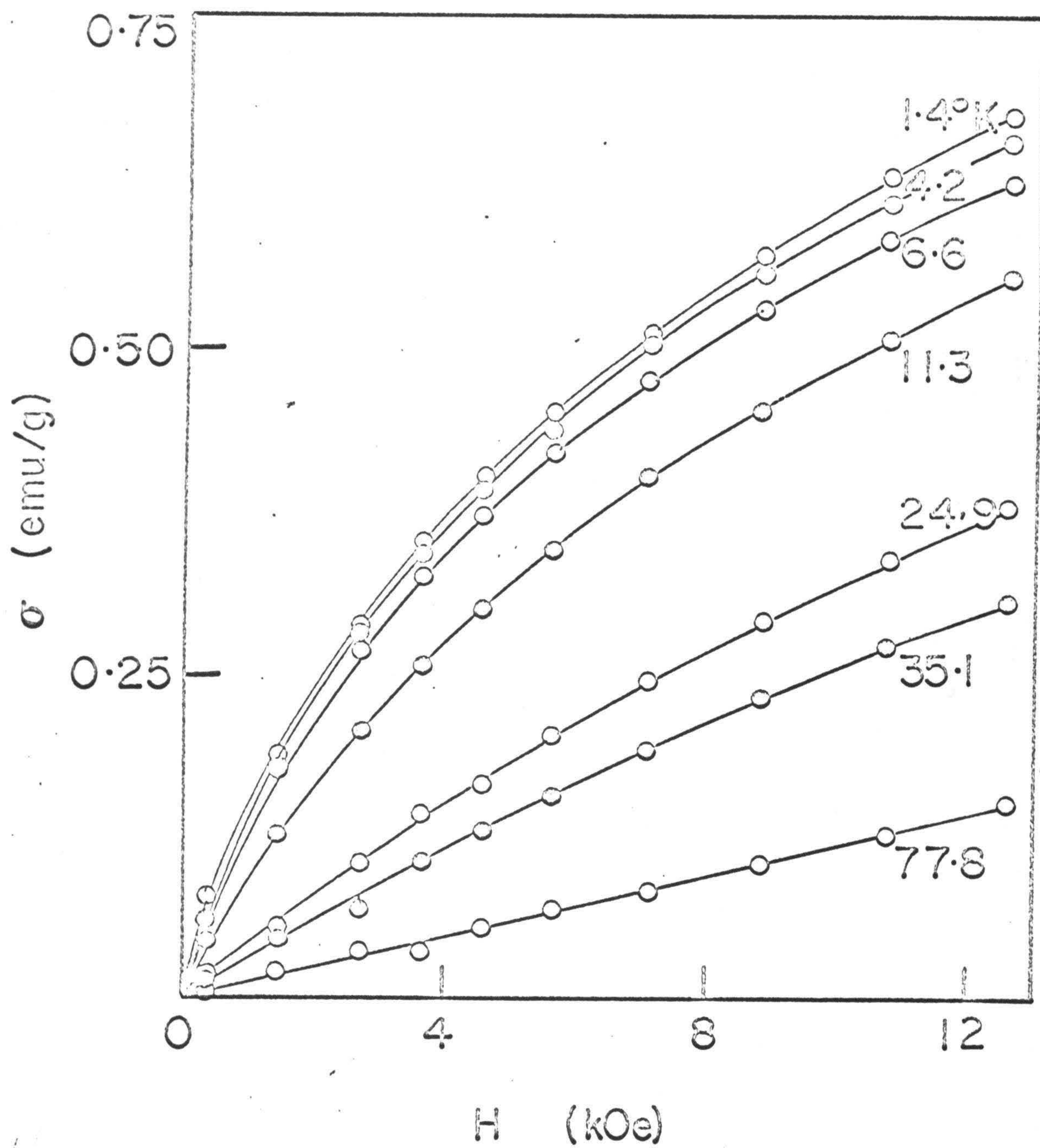




Figure 27.  $\sigma$  vs.  $H$  for quenched  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$  at temperatures indicated. The data, at a given temperature, were obtained by cooling the specimen in an applied field of 12.6 kOe and then going down in field. See Table 15(a).



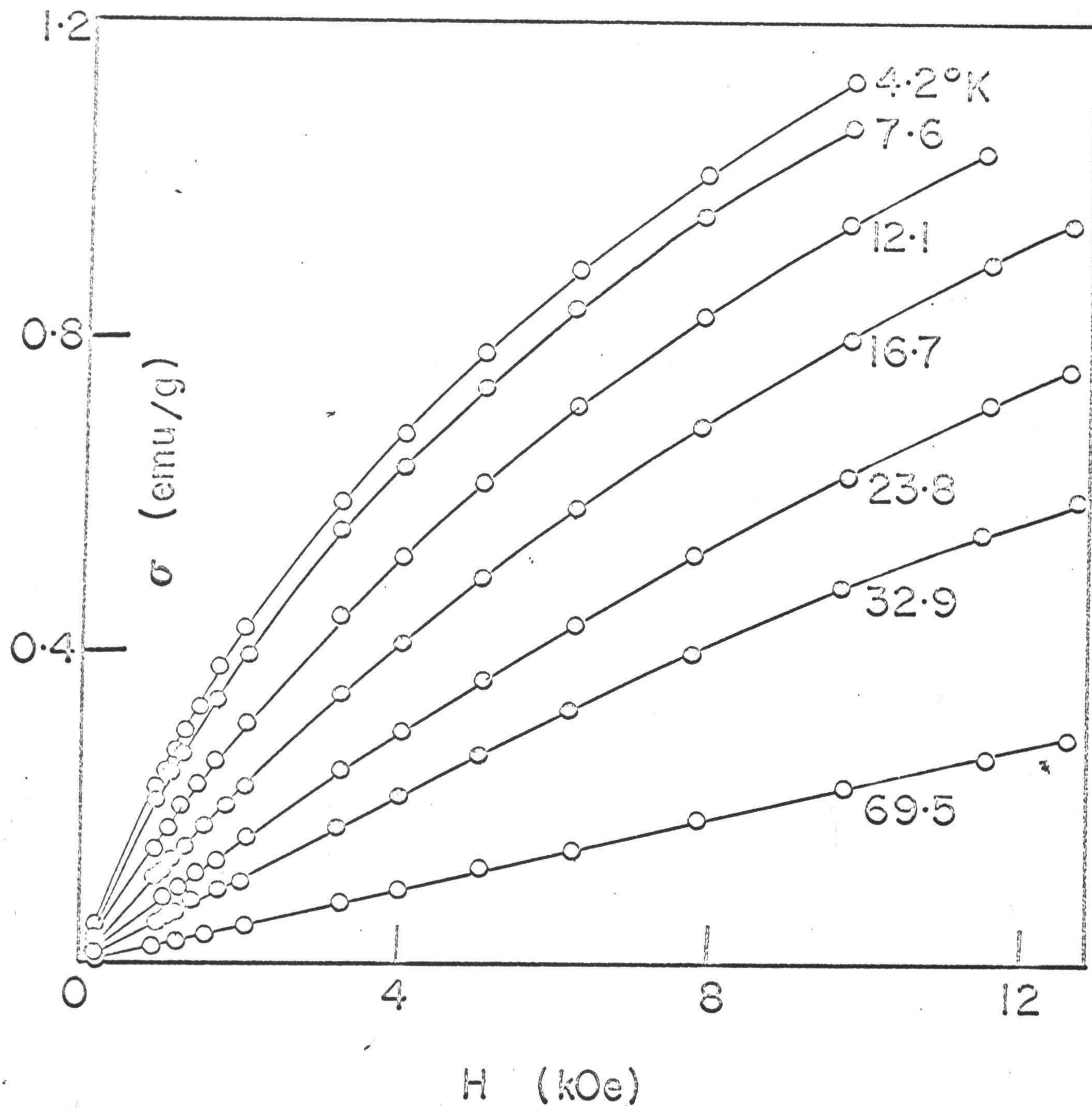




Figure 28.  $\sigma$  vs.  $H$  for quenched  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  at temperatures indicated. The data, at a given temperature, were obtained by cooling the specimen in an applied field of 12.6 kOe and then going down in field. See Table 16(a).



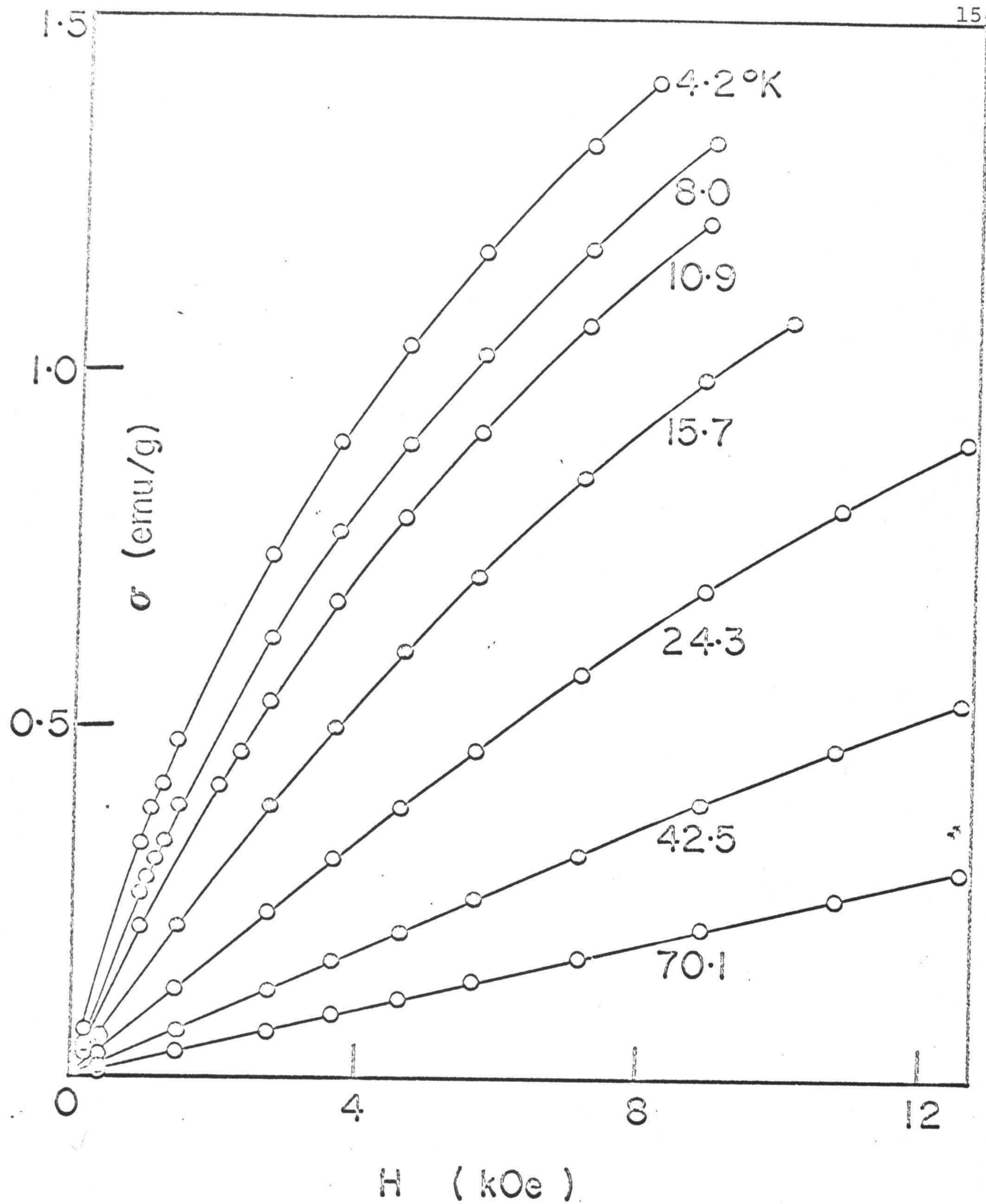




Figure 29.  $\sigma$  vs.  $T$  at  $H=1000$  Oe for quenched  $\text{Cu}_{0.99}\text{Fe}_{0.01}$ .  
Measured after cooling in 1000 Oe field: empty  
circle; measured after cooling to 1.3°K in zero  
field: filled circle. See Tables 14(b) and 14(c).



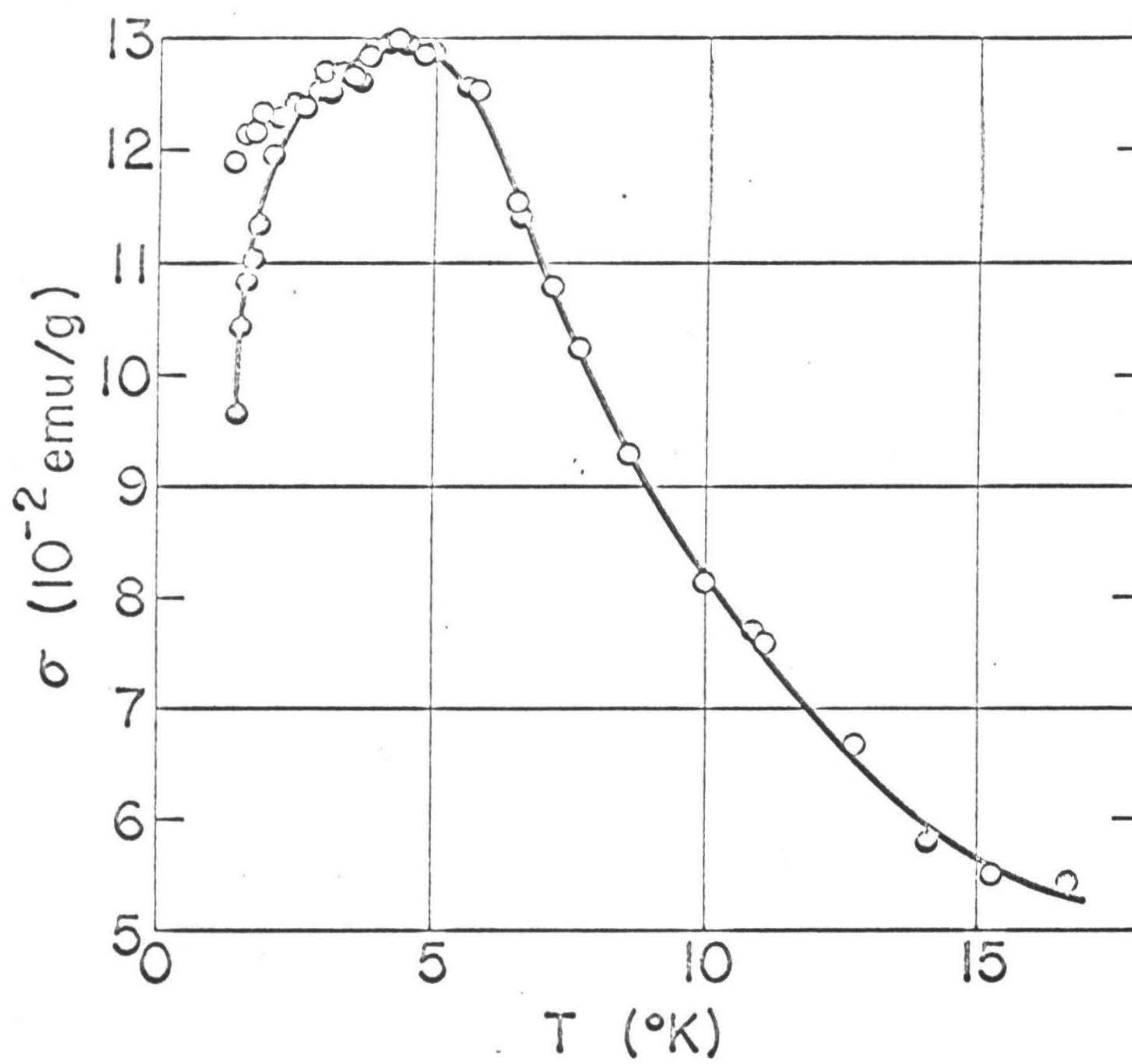




Figure 30.  $\sigma$  vs.  $T$  at  $H = 700$  Oe for quenched  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$ . Measured after cooling in 700 Oe field: empty circle; measured after cooling to  $1.3^\circ\text{K}$  in zero field: filled circle. See Tables 15(b) and 15(c).



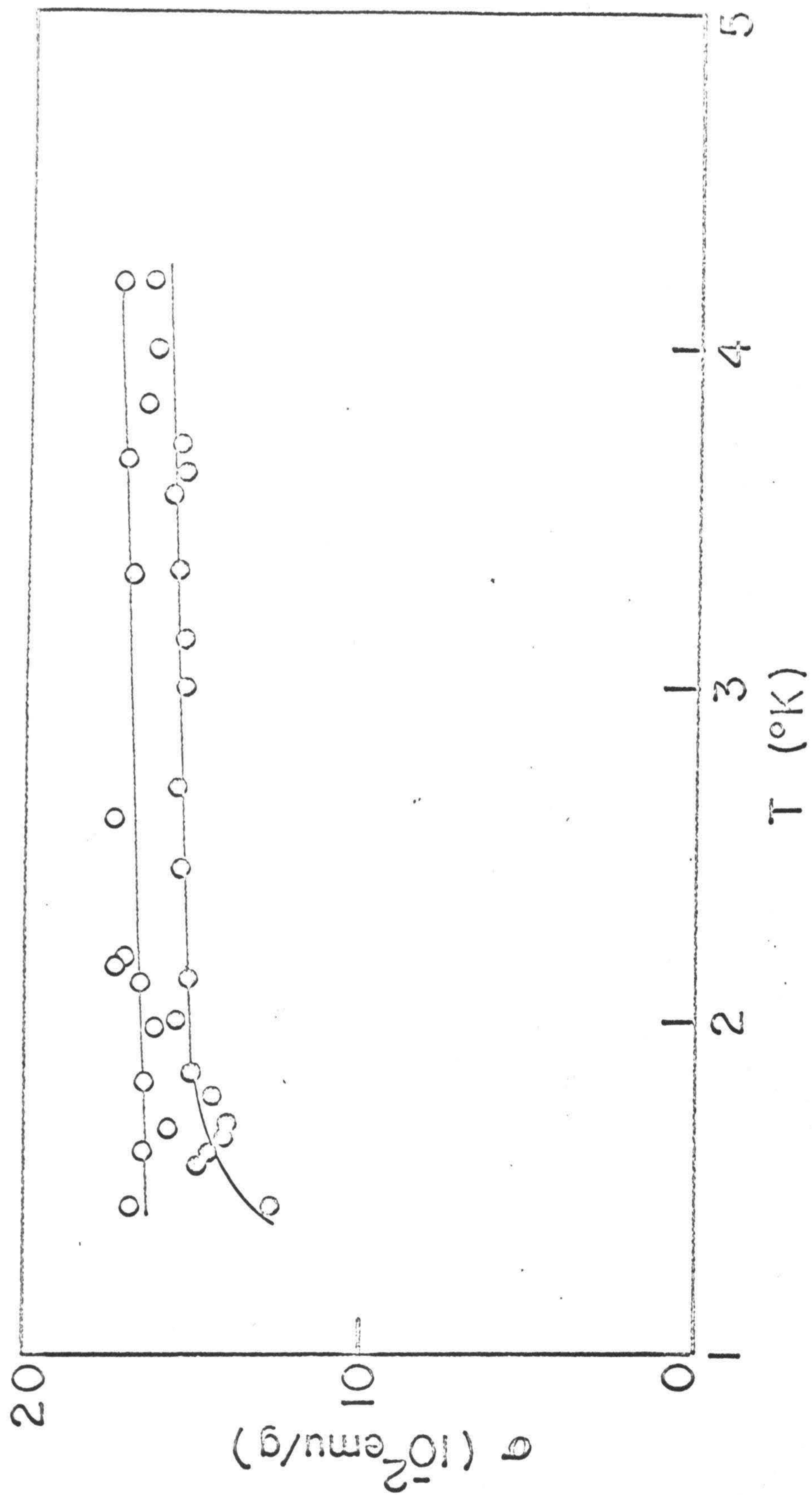
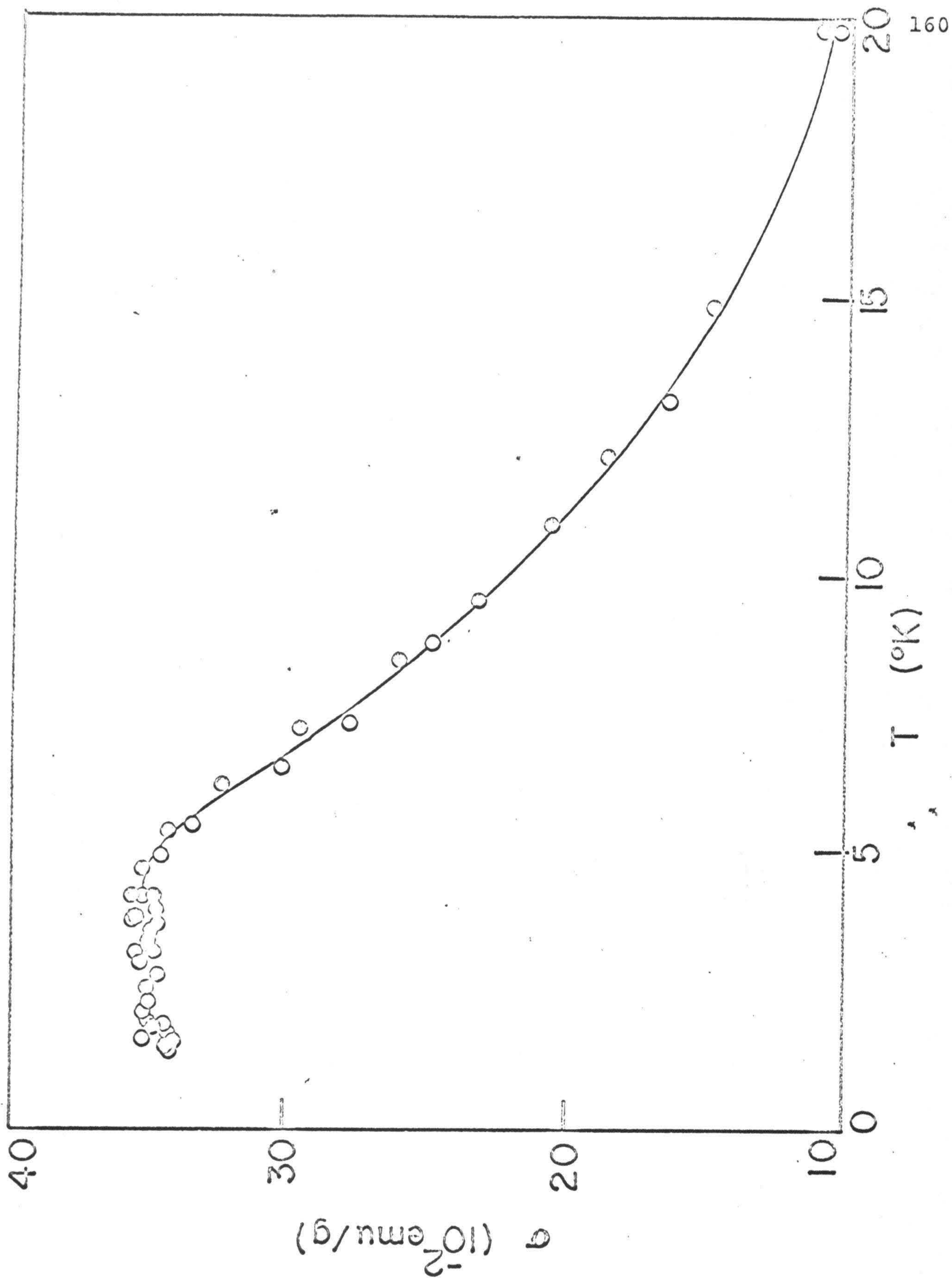




Figure 31.  $\sigma$  vs.  $T$  at  $H=1000$  Oe for quenched  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$ . Measured after cooling in 1000 Oe field: empty circle; measured after cooling to 1.3°K in zero field: filled circle. See Tables 16(b) and 16(c).







a reanalysis of the data was carried out by fitting with an equation containing four Brillouin terms:

$$\sigma = \chi_0 H + \frac{N_O}{M} c_1 \mu_1 \mu_B B(\mu_1, \frac{H}{T-\theta_1}) + \frac{N_O}{M} c_2 \mu_2 \mu_B B(\mu_2, \frac{H}{T-\theta_2}) \\ + \frac{N_O}{M} c_3 \mu_3 \mu_B B(\mu_3, \frac{H}{T-\theta_3}) + \frac{N_O}{M} c_4 \mu_4 \mu_B B(\mu_4, \frac{H}{T-\theta_4}) \quad (14)$$

and by assuming that  $\mu_1$ ,  $c_1$  and  $\theta_1$  have the same values as obtained from the above three-moment analysis, but not placing any restrictions on the other parameters. A slightly better rmsd was obtained with this analysis. The resulting parameter values are listed in Table 36. The values of  $\mu_1$ ,  $\mu_2$ ,  $\mu_3$  and  $\mu_4$  are now found to be fairly close to the ratio 1 : 2 : 3 : 4. The total concentration of Fe atoms  $Z = c_1 + 2c_2 + 3c_3 + 4c_4$  is  $\sim 78$  ppm. The magnetization values interpolated from experimental data, and the calculated magnetization values are compared in Fig. 32.

Magnetization data for Cu-Fe alloys containing 102 to 478 ppm Fe, at temperatures between 0.01°K and 0.4°K and in fields of 0.97 Oe to 217 Oe, were supplied to us by Dr. E. C. Hirschhoff and Prof. J. C. Wheatley.<sup>9</sup> The magnetization values in their tables were expressed in Gauss but they were converted for the sake of convenience to emu/g units using the relation  $\sigma$  (emu/g) =  $M(\text{Gauss})\rho$  (g/cc).  $\rho$  is the density of the alloy, and was assumed to be that of copper, i.e., 8.95 g/cc. It was decided to analyze the data for a Cu-Fe alloy containing 112 ppm



Table 36. Parameters from least squares fitting of Eq. 14 to magnetization data for Cu-Fe alloy, Tholence and Tournier<sup>6</sup> and Hirschkoﬀ et al.<sup>9</sup>

| Alloy                     | 108 ppm Fe in Cu <sup>6</sup>                                                | 112 ppm Fe in Cu <sup>9</sup>                             |
|---------------------------|------------------------------------------------------------------------------|-----------------------------------------------------------|
| Temp. range (°K)          | 1.3 to 32.5                                                                  | 0.01 to 0.4                                               |
| Moments ( $\mu_B$ )       | $\mu_1 = 2.44, \mu_2 = 4.86,$<br>$\mu_3 = 7.22, \mu_4 = 10.17$               | $\mu_1 = 7.0, \mu_2 = 9.8,$<br>$\mu_3 = 29.5$             |
| Concentrations (ppm)      | $c_1 = 56.7, c_2 = 5.29,$<br>$c_3 = 1.49, c_4 = 1.56$                        | $c_1 = 0.55, c_2 = 0.022,$<br>$c_3 = 0.003$               |
| Characteristic Temp. (°K) | $\theta_1 = -21.5, \theta_2 = -17.9,$<br>$\theta_3 = -17.9, \theta_4 = -8.9$ | $\theta_1 = -0.039, \theta_2 = +0.008,$<br>$\theta_3 = 0$ |
| $\chi_0$ (emu/g)          | $0.48 \times 10^{-8}$                                                        | $8.7 \times 10^{-8}$                                      |
| rmsd (emu/g)              | $0.044 \times 10^{-3}$                                                       | $0.028 \times 10^{-4}$                                    |
| rmsd (%)*                 | 0.78                                                                         | 1.03                                                      |

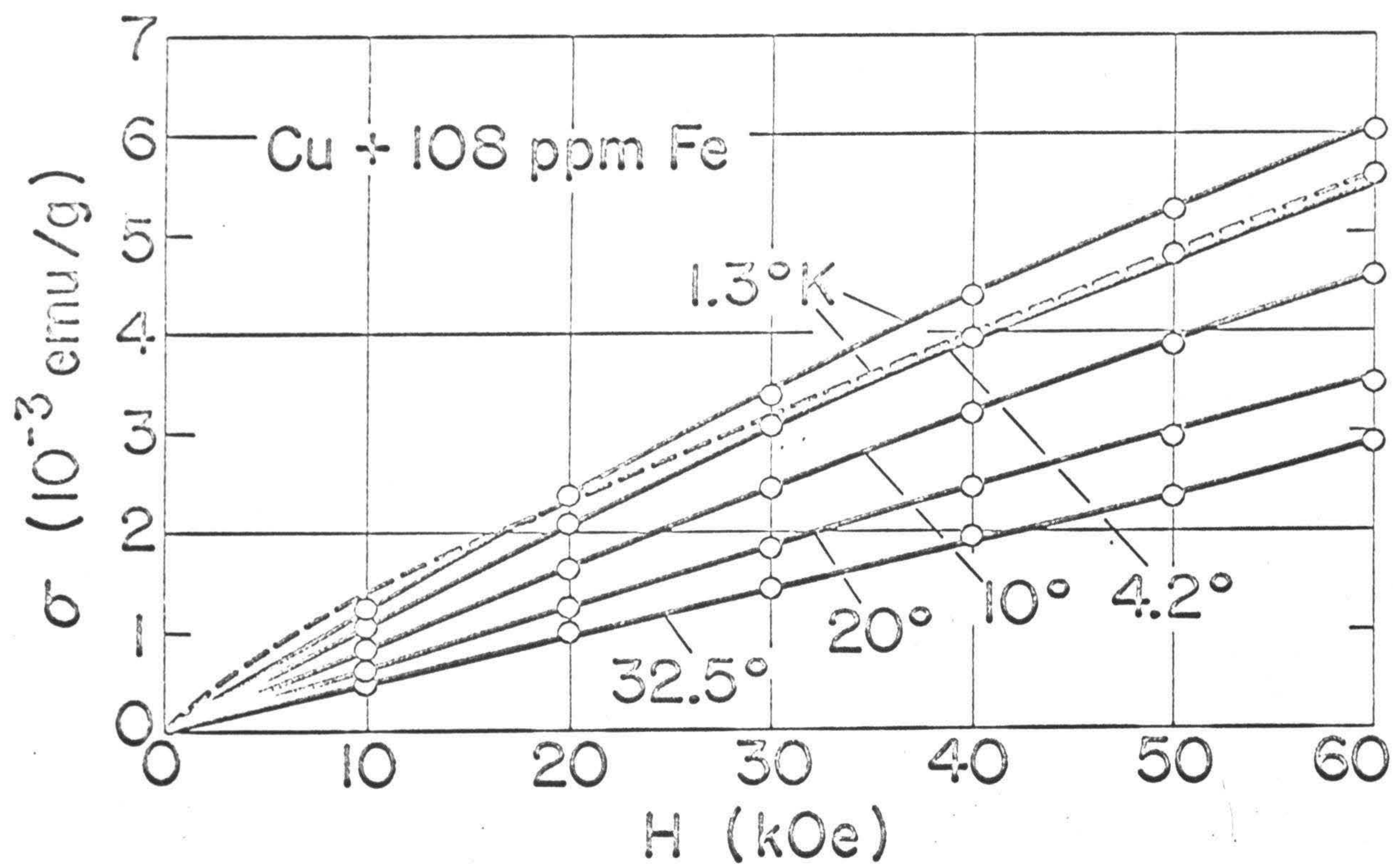
\*The rmsd as expressed in percents of the highest magnetization value used in the fitting.

Note: The accuracy with which  $\mu_1, \mu_2, \mu_3$  and  $\mu_4$  have been determined is estimated to be roughly  $\pm 5\%$ ,  $\pm 10\%$ ,  $\pm 20\%$ , and  $\pm 20\%$  respectively. Similar uncertainties are involved in the values of  $c_1, c_2, c_3, c_4$  and  $\theta_1, \theta_2, \theta_3, \theta_4$ ; the value of  $\chi_0$  is within  $\pm 5\%$ .



Figure 32.  $\sigma$  vs.  $H$  isotherms for 108 ppm Fe in Cu • Points O, interpolated from experimental data by Tholence and Tournier<sup>6</sup> (Table 17); curves calculated from Eq. 14 with parameter values from Table 36. Dashed curve was calculated for 1.3°K according to Ref. 6.







Fe; the selection was based on the relative completeness of the data for this alloy as a function of temperature and field and the similarity in composition to the Cu-Fe alloy of Tholence and Tournier<sup>6</sup> containing 108 ppm Fe which was analyzed in a similar fashion. For the purpose of the fitting thirty-six points (Fig. 33) were obtained by interpolation, at various temperatures and fields to construct six isotherms between 0.012° to 0.2°K. A sufficiently good fit was obtained by least squares fitting of Eq. 13; the parameter values obtained are listed in Table 36. Figure 33 shows the isotherms calculated from these parameter values and the magnetization data used. In Fig. 34 one finds that for  $H = 10$  Oe the  $\sigma$  vs.  $T$  curves calculated from the same parameter values for temperatures from  $\sim 0.01$  to  $\sim 0.4^\circ\text{K}$  represent the actual data points reasonably well. This is also found to be true at all other field values between 0.977 Oe and 217.11 Oe. The fit is very satisfactory in the entire range of fields and temperatures.

At the lowest temperatures the data of Hirschkoﬀ et al.<sup>9</sup> for a Cu-Fe alloy with 478 ppm Fe (Table 19) show appreciable deviations from the Curie-Weiss type behavior. This is shown in Fig. 35, where the dashed line gives the extrapolation below  $0.08^\circ\text{K}$  from the data points above that temperature by means of least squares fitting of:

$$\sigma = \chi_0 H + \frac{N_0 c p^2 \mu_B^2}{3Mk(T-\theta)} H \quad (15)$$



Figure 33.  $\sigma$  vs.  $H$  isotherms for 112 ppm Fe in Cu for temperatures indicated. Points O, interpolated from experimental data by Hirschkoﬀ et al.<sup>9</sup> (Table 18); curves calculated from Eq. 14 with parameter values from Table 36.



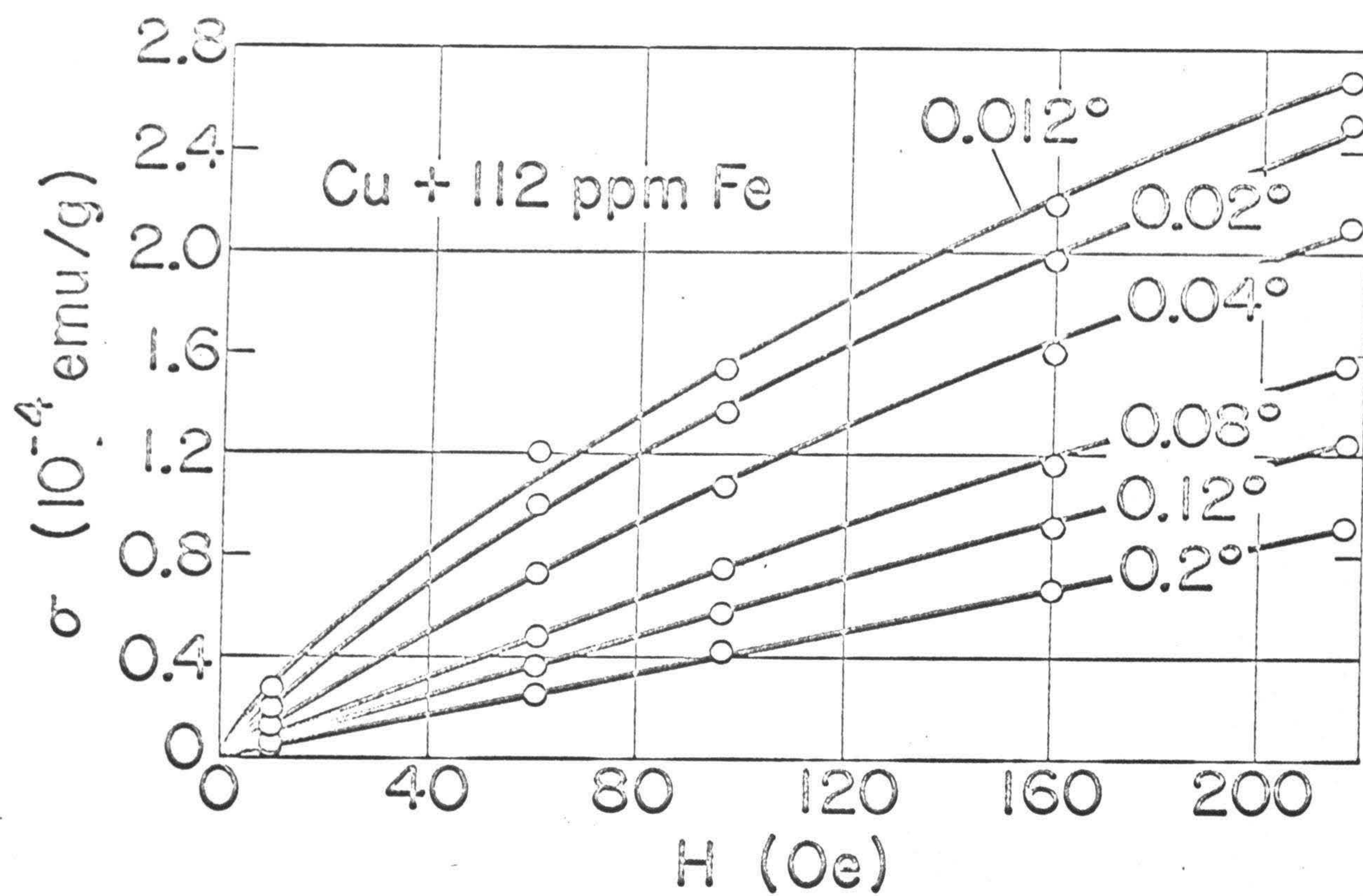




Figure 34.  $\sigma$  vs.  $T$  at  $H=10$  Oe for 112 ppm Fe in Cu. Experimental data by Hirschkoﬀ et al.<sup>9</sup> (Table 18):  $\circ$ ; solid curve was calculated with parameter values from Table 36, using Eq. 14.



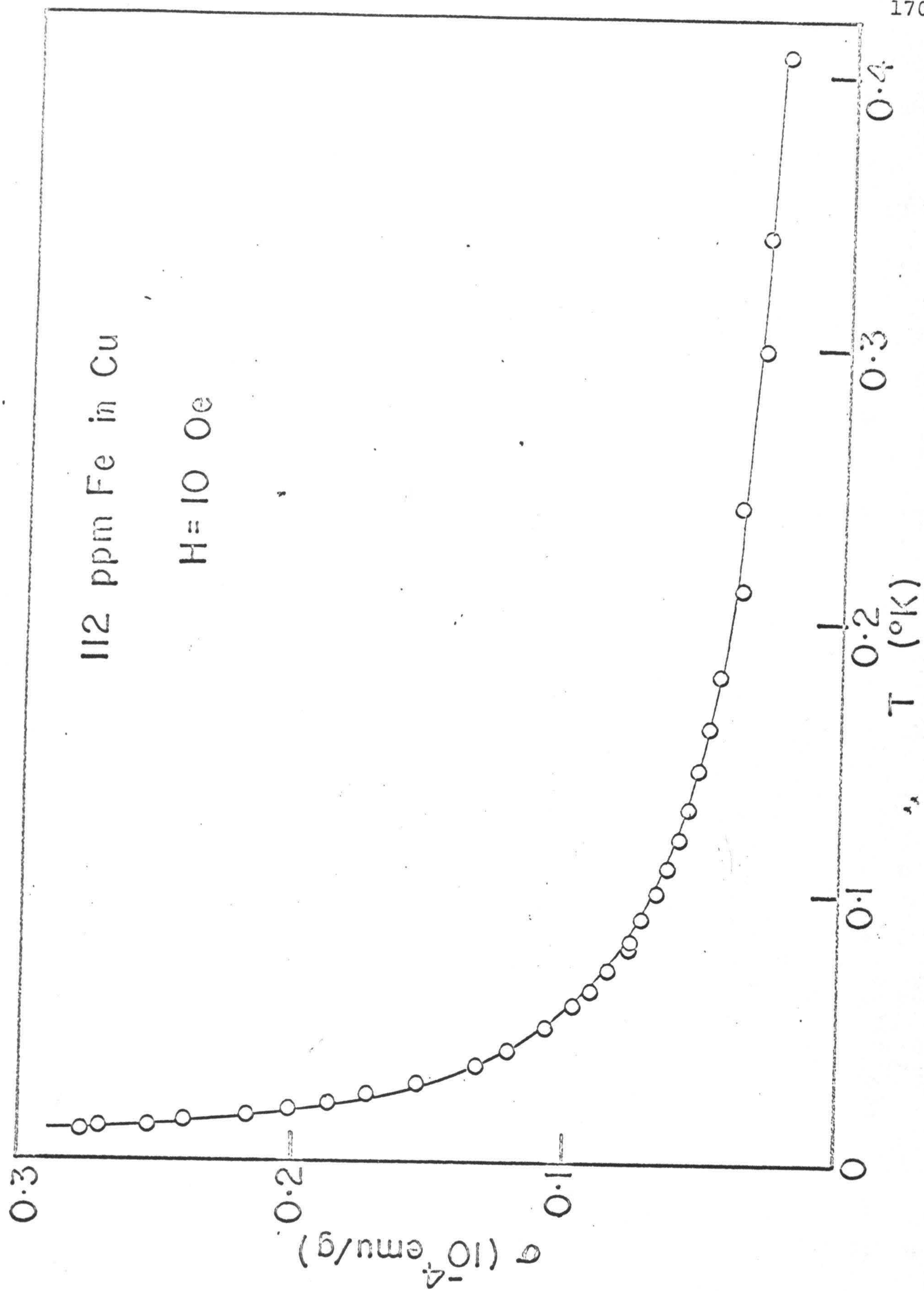
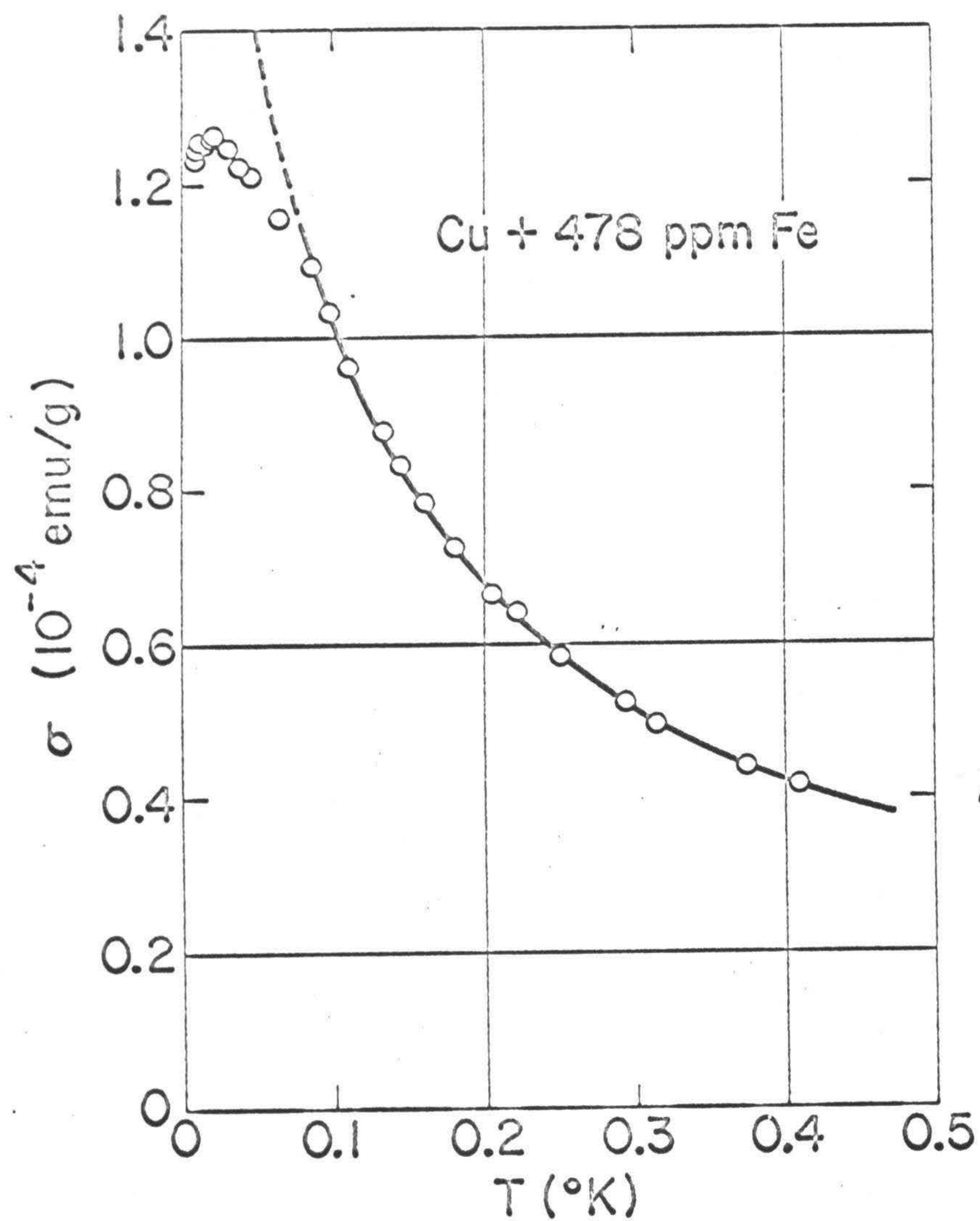




Figure 35.  $\sigma$  vs.  $T$  at  $H=10$  Oe for 478 ppm Fe alloy. Experimental data:  $\circ$ , by Hirschkoﬀ et al.<sup>9</sup> (Table 19); solid curve and dashed line by least squares fitting of Eq. 15 to data at  $T > 0.08^\circ\text{K}$ .







with the parameter values:  $\chi_0 = 6.6 \times 10^{-9}$  emu/g,  $cp^2 = 0.88 \mu_B^2$  per alloy atom, and  $\theta = -0.08^\circ\text{K}$  (rmsd =  $0.52 \times 10^{-6}$  emu/g). The low temperature data themselves show a maximum in the magnetization at approximately  $0.02^\circ\text{K}$ .

#### 4. Cu-Ni-Fe ( $\sim 1000$ ppm Fe; 10, 20, 30 at. % Ni).

The magnetization data for quenched Cu-Ni-Fe alloys containing  $\sim 100$  to  $\sim 1000$  ppm Fe are listed in Tables 20 through 27. The magnetization data for the deformed alloys are listed in Tables 28 through 33.

##### a. Quenched alloys.

The data for each alloy were analyzed by least squares fitting of Eq. 13. To simplify the fitting procedure the following assumptions were made for the quenched alloys:

(1) The total concentration of Fe atoms in all clusters is equal to the nominal concentration ( $z$ ) of Fe in the alloy, i.e.,

$$c_1 + 2c_2 + 3c_3 = z \quad (16)$$

Although samples from some of the Cu-Ni-Fe alloys were analyzed (Table 4) for Fe content, the reliability of these analyses is not known. It would have been desirable to make  $z$  a variable parameter in the least squares fitting of Eq. 13 and to assume that the actual Fe concentration of the alloy is that value of  $z$  for which the best rmsd value and the least systematic



deviation is obtained. However, such a process would have been very laborious and time consuming.

(2) Since all these alloys were quenched from high temperature, i.e., from 1050°C, it is assumed that they are in a state of thermal equilibrium at some temperature.

The thermal equilibrium may not necessarily correspond to that at 1050°C. In fact Mozer et al.<sup>23</sup> have pointed out that practically no cooling rate can quench the local atomic arrangements in a Cu-Ni alloy at ~1000°C and that, on the other hand, any reasonable cooling rate (such as the one used here, i.e., approximately 100°C/sec.) will prevent changes below 500°C. Therefore the thermal equilibrium may be expected to represent some temperature between ~500°C and 1050°C. That in fact the thermal equilibrium at some elevated temperature is quite well retained on quenching to room temperature is indicated by the observation that the magnetization data for the quenched specimen of the Cu<sub>0.8</sub>Ni<sub>0.2</sub> alloy with 1000 ppm Fe were reproducible after quenching a second time from the same temperature.

In an alloy which has retained a state of thermal equilibrium, the concentrations of atomic clusters (in the present case  $c_1$  and  $c_2$ , the concentrations of clusters with one, and with two Fe atoms, respectively) can be estimated from a single parameter  $\text{Fe-Fe}^{\alpha}_1$  defined by the following relation:

$$z_1 = (1 - z) \text{Fe-Fe}^{\alpha}_1 + z \quad (17)$$



where  $z_1$  is the average concentration of Fe in the nearest neighbor shells of all Fe atoms. When the thermal equilibrium corresponds to a situation where the Fe atoms are distributed randomly in the alloy, the value of  $\text{Fe-Fe}^{\alpha}_1$ , often referred to as the short-range-order parameter, is zero. A positive value of  $\text{Fe-Fe}^{\alpha}_1$  expresses a clustering tendency of the Fe atoms.

For a given value of  $z$ , the ratio of the concentrations of isolated Fe atoms and of Fe pairs may be calculated in the following manner. The probabilities  $p_0$  and  $p_1$  for an Fe atom A to have zero ( $n=0$ ), or one ( $n=1$ ), Fe nearest neighbor are calculated from

$$p_n = \frac{12!}{(12-n)! n!} \cdot z_1^n (1 - z_1)^{12-n} \quad (18)$$

with  $n=0$  or  $n=1$ , respectively. The concentration of isolated Fe atoms is,

$$c_1 = zp_0 = z(1 - z_1)^{12} \quad (19)$$

The probability that an Fe atom (say A) has one, and only one, Fe atom (say B) in its nearest neighbor shell is,

$$p_1 = 12z_1(1 - z_1)^{11} \quad (20)$$

The Fe atom B, in its turn, has twelve nearest neighbor sites; the Fe atom A is occupying one of these sites, and of the remaining eleven, four are nearest neighbor sites of the Fe atom A as well. In calculating  $p_1$ , it has already been insured that there is no Fe atom at any of these four common sites. Now, if



there is an Fe atom, at any of the seven other nearest neighbor sites of the atom B, then a triplet or larger cluster configuration would result; if there is no Fe atom at any of these seven sites then an isolated Fe-Fe doublet, i.e., Fe-pair is formed. Therefore the probability of a given Fe atom being part of an isolated doublet, i.e., the fraction of Fe atoms in doublets, is

$$p_{\text{Fe-Fe}} = 12z_1(1-z_1)^{11}(1-z_1)^7 = 12z_1(1-z_1)^{18} \quad (21)$$

The concentrations of such Fe pairs is

$$c_2 = 1/2 z_1 p_{\text{Fe-Fe}} = 6zz_1(1-z_1)^{18} \quad (22)$$

The fraction of Fe atoms in Fe triplets and in clusters involving larger number of Fe atoms is then equal to  $(z - c_1 - 2c_2)$ . Since the quantity  $(z - c_1 - 2c_2)$  was found to be very small when compared to  $c_1$  or  $2c_2$ , even for an alloy containing 1000 ppm Fe ( $z = 1000 \times 10^{-6}$ ), it is reasonable to assume that it is very nearly equal to the fraction of Fe atoms in triplets, i.e., that the fraction of Fe atoms in clusters involving more than three Fe atoms, is negligible. Then the concentration of Fe-triplets is

$$c_3 = (z - c_1 - 2c_2)/3 \quad (23)$$

Thus using Eqs. 19, 22, and 23 one can obtain, for a given value of  $\text{Fe-Fe}^{\alpha_1}$  the values of  $c_1$ ,  $c_2$ , and  $c_3$ .

The data for the following quenched alloys: 1000 ppm Fe in  $\text{Cu}_{0.9}\text{Ni}_{0.1}$ , 500 ppm Fe in  $\text{Cu}_{0.9}\text{Ni}_{0.1}$ , 1000 ppm Fe in  $\text{Cu}_{0.8}\text{Ni}_{0.2}$



and 500 ppm Fe in  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  were analyzed by least squares fitting of Eq. 13 where  $c_1$ ,  $c_2$ , and  $c_3$  were varied simultaneously by varying a single parameter:  $\text{Fe-Fe}^{\alpha_1}$ .

For the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing 100 ppm Fe, the concentration  $c_3$  was extremely small, so that  $c_1 + c_2 \approx z$  and fits of Eq. 11 with two Brillouin terms were found to be very satisfactory. Here again  $c_1$  and  $c_2$  were simultaneously varied by varying a single parameter  $\text{Fe-Fe}^{\alpha_1}$  and keeping the total Fe concentration constant.

The parameter values obtained for the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys, each containing 100, or 500, or 1000 ppm Fe, are presented in Tables 37 and 38, and the fits are illustrated in Figures 36 through 43.

The method of analysis for the quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy with 100 ppm Fe was the same as above, but the magnetization of the binary alloy  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ , to which the Fe was added, was first subtracted from the total measured magnetization of the ternary alloy.

$$\begin{aligned} \Delta\sigma_{\text{Fe}} = & \sigma \text{ (for } \text{Cu}_{0.7}\text{Ni}_{0.3} + 100 \text{ ppm Fe)} \\ & - \sigma \text{ (for } \text{Cu}_{0.7}\text{Ni}_{0.3}) \end{aligned} \quad (24)$$

This procedure was followed in view of the fact that in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  itself there are present small Ni-rich magnetic clusters with an average cluster moment of  $\mu \approx 2.76 \mu_B$ . The term  $\Delta\sigma_{\text{Fe}}$  represents the change in magnetization due to the



Table 37. Parameters from least squares fitting of Eq. 11 or Eq. 13 to magnetization data for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys containing Fe.

| Fe Content (ppm)                   | 100         | 500         | 1000        |
|------------------------------------|-------------|-------------|-------------|
| Temp. range ( $^{\circ}\text{K}$ ) | 1.34 to 300 | 1.51 to 300 | 2.02 to 300 |
| $\mu_1$ ( $\mu_{\text{B}}$ )       | 2.70        | 2.98        | 2.96        |
| $\mu_2$ ( $\mu_{\text{B}}$ )       | 5.41        | 5.51        | 5.76        |
| $\mu_3$ ( $\mu_{\text{B}}$ )       |             | 8.17        | 10.10       |
| $c_1$ (ppm)                        | 92.5        | 375.9       | 694.1       |
| $c_2$ (ppm)                        | 3.7         | 45.9        | 104.0       |
| $c_3$ (ppm)                        |             | 10.7        | 32.6        |
| $\theta_1$ ( $^{\circ}\text{K}$ )  | - 0.83      | - 2.15      | - 4.05      |
| $\theta_2$ ( $^{\circ}\text{K}$ )  | + 0.85      | - 0.15      | 0           |
| $\theta_3$ ( $^{\circ}\text{K}$ )  |             | + 0.55      | 0           |
| $\chi_0$ ( $10^{-6}$ emu/g)        | 0.166       | 0.172       | 0.165       |
| Fe-Fe $^{\alpha_1}$                | 0.007       | 0.023       | 0.029       |
| $c_2/c_1$                          | 0.041       | 0.122       | 0.150       |
| rmsd ( $10^{-3}$ emu/g)            | 0.145       | 0.237       | 0.558       |
| rmsd (%) *                         | 0.94        | 0.38        | 0.48        |

\*The rmsd value as expressed in percents of the highest value of magnetization used in the fitting.



Table 38. Parameters from least squares fitting of Eq. 11 or Eq. 13 to magnetization data for quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing Fe.

| Fe Content (ppm)                   | 100                | 500                | 1000              |
|------------------------------------|--------------------|--------------------|-------------------|
| Temp. range ( $^{\circ}\text{K}$ ) | 2.84 to $\sim 300$ | 2.66 to $\sim 300$ | 1.5 to $\sim 300$ |
| $\mu_1$ ( $\mu_B$ )                | 3.76               | 3.52               | 3.89              |
| $\mu_2$ ( $\mu_B$ )                | 8.35               | 8.53               | 6.46              |
| $\mu_3$ ( $\mu_B$ )                |                    | 15.25              | 14.85             |
| $c_1$ (ppm)                        | 95.9               | 414.6              | 711.4             |
| $c_2$ (ppm)                        | 2.0                | 35.1               | 100.7             |
| $c_3$ (ppm)                        |                    | 5.1                | 29.0              |
| $\theta_1$ ( $^{\circ}\text{K}$ )  | - 0.26             | - 0.08             | - 2.05            |
| $\theta_2$ ( $^{\circ}\text{K}$ )  | + 1.00             | - 0.77             | + 0.46            |
| $\theta_3$ ( $^{\circ}\text{K}$ )  |                    | - 2.70             | - 0.18            |
| $\chi_0$ ( $10^{-6}$ emu/g)        | 0.491              | 0.506              | 0.402             |
| Fe-Fe $^{\alpha}1$                 | 0.0035             | 0.015              | 0.027             |
| $c_2/c_1$                          | 0.021              | 0.085              | 0.141             |
| rmsd ( $10^{-3}$ emu/g)            | 0.149              | 0.230              | 0.947             |
| rmsd (%) <sup>*</sup>              | 0.67               | 0.25               | 0.48              |

\*The rmsd value as expressed in percents of the highest value of the magnetization used in the fitting.



Figure 36.  $\chi$  vs.  $T$  for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys containing various amounts of Fe. The solid curves were calculated using parameter values listed in Table 37.



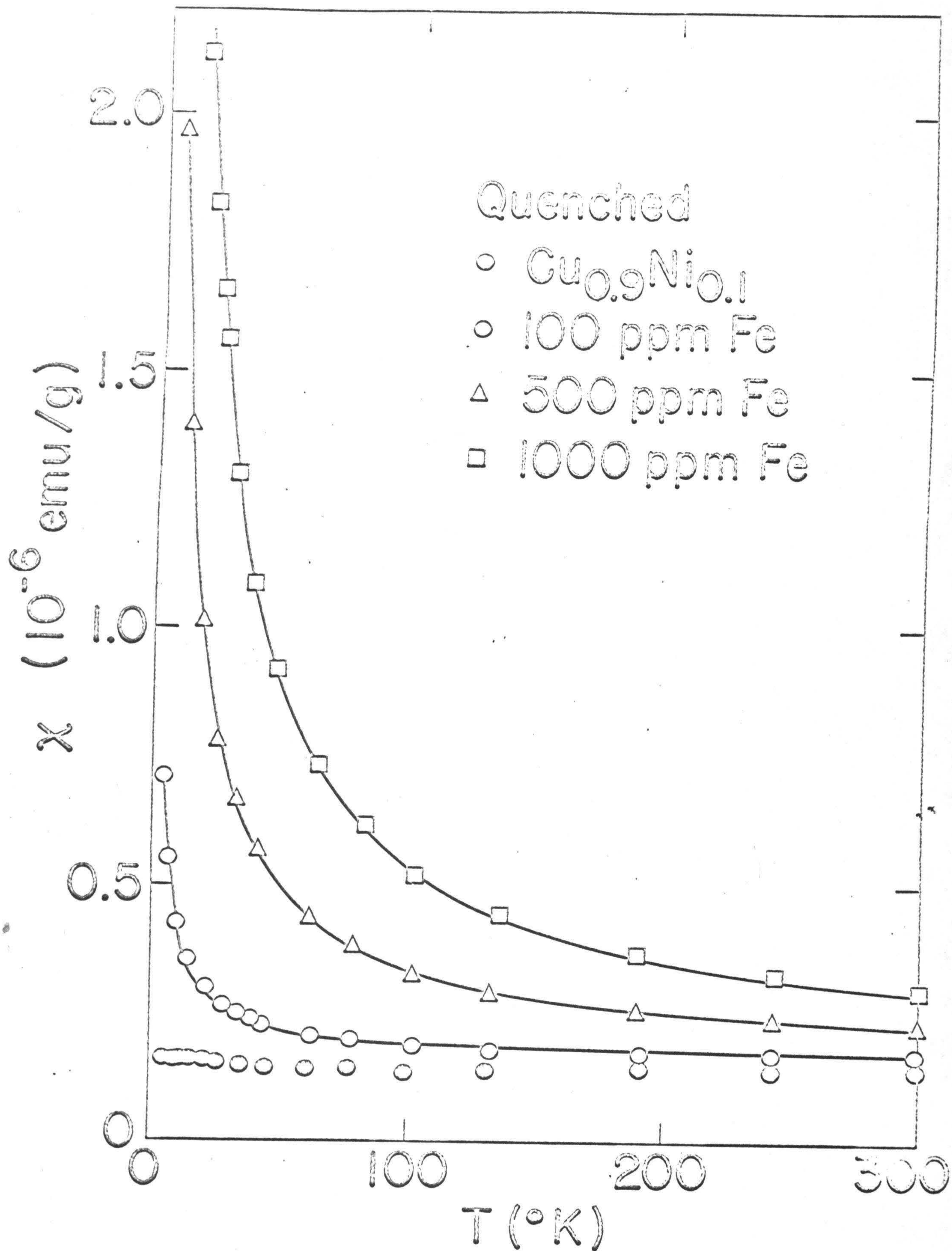




Figure 37. Magnetization vs. field for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  with 100 ppm Fe. The empty and filled circles represent measured data (Table 20). The solid curves were calculated using parameter values in Table 37.



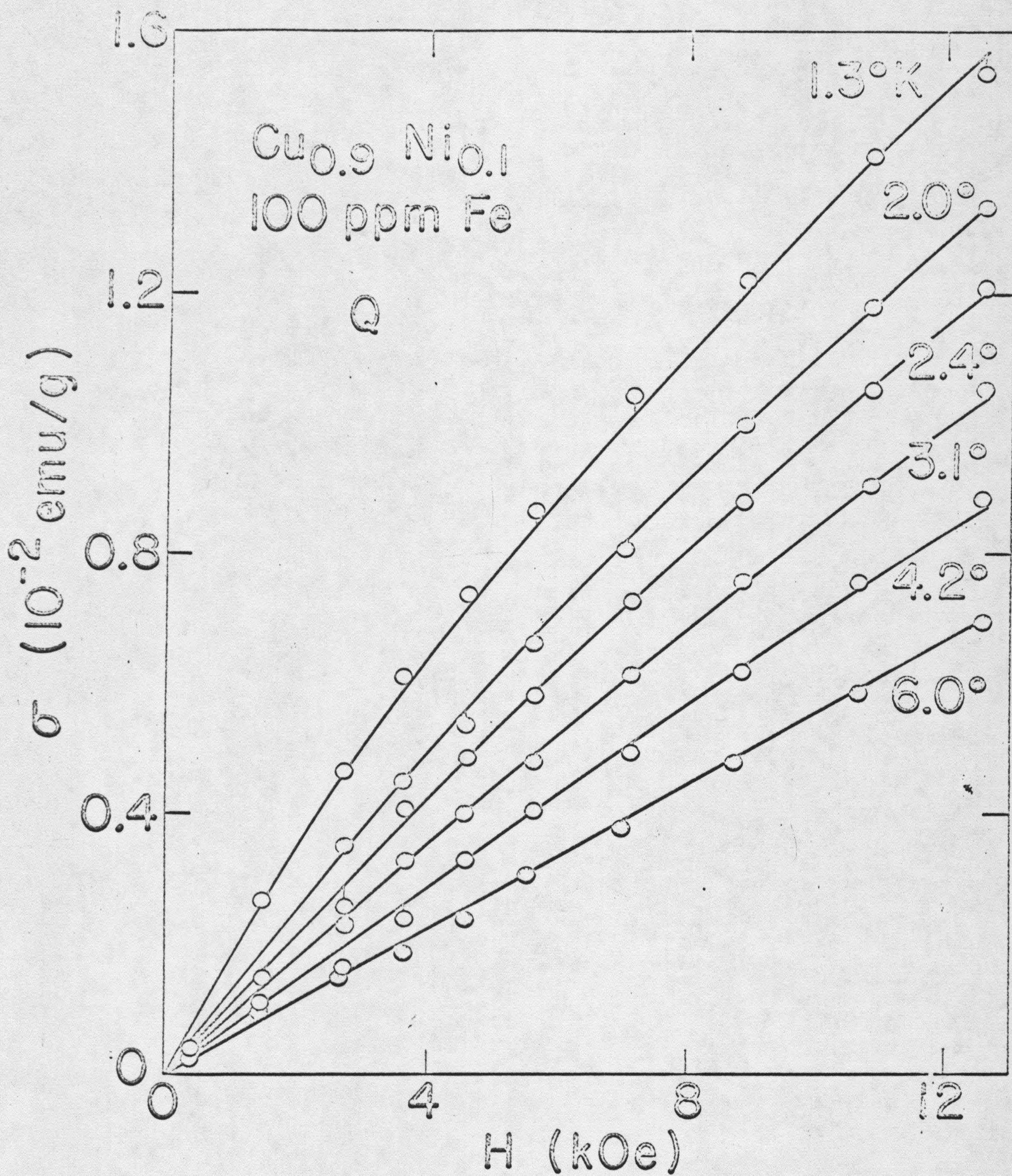




Figure 38. Magnetization vs. field for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  with 500 ppm Fe. The empty and filled circles represent measured data (Table 21). The solid curves were calculated using parameter values listed in Table 37.



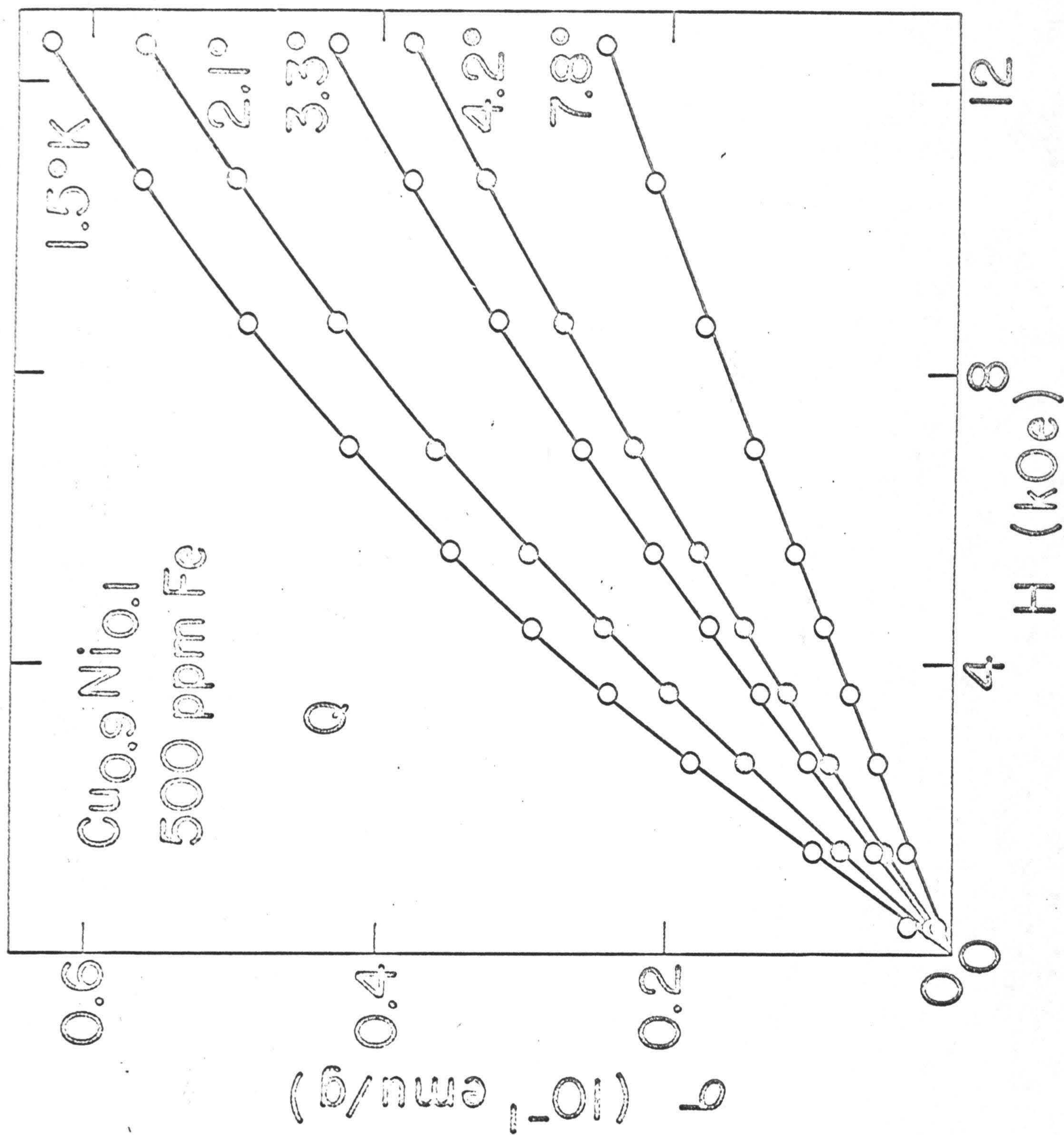




Figure 39. Magnetization vs. field for quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  with 1000 ppm Fe. The empty and filled circles represent measured data (Table 22). The dashed curve and the solid curves were calculated using parameter values (Table 37) obtained by least squares fitting of Eq. 13 to experimental data in the temperature range of  $2.0^\circ$  to  $\sim 300^\circ\text{K}$ .



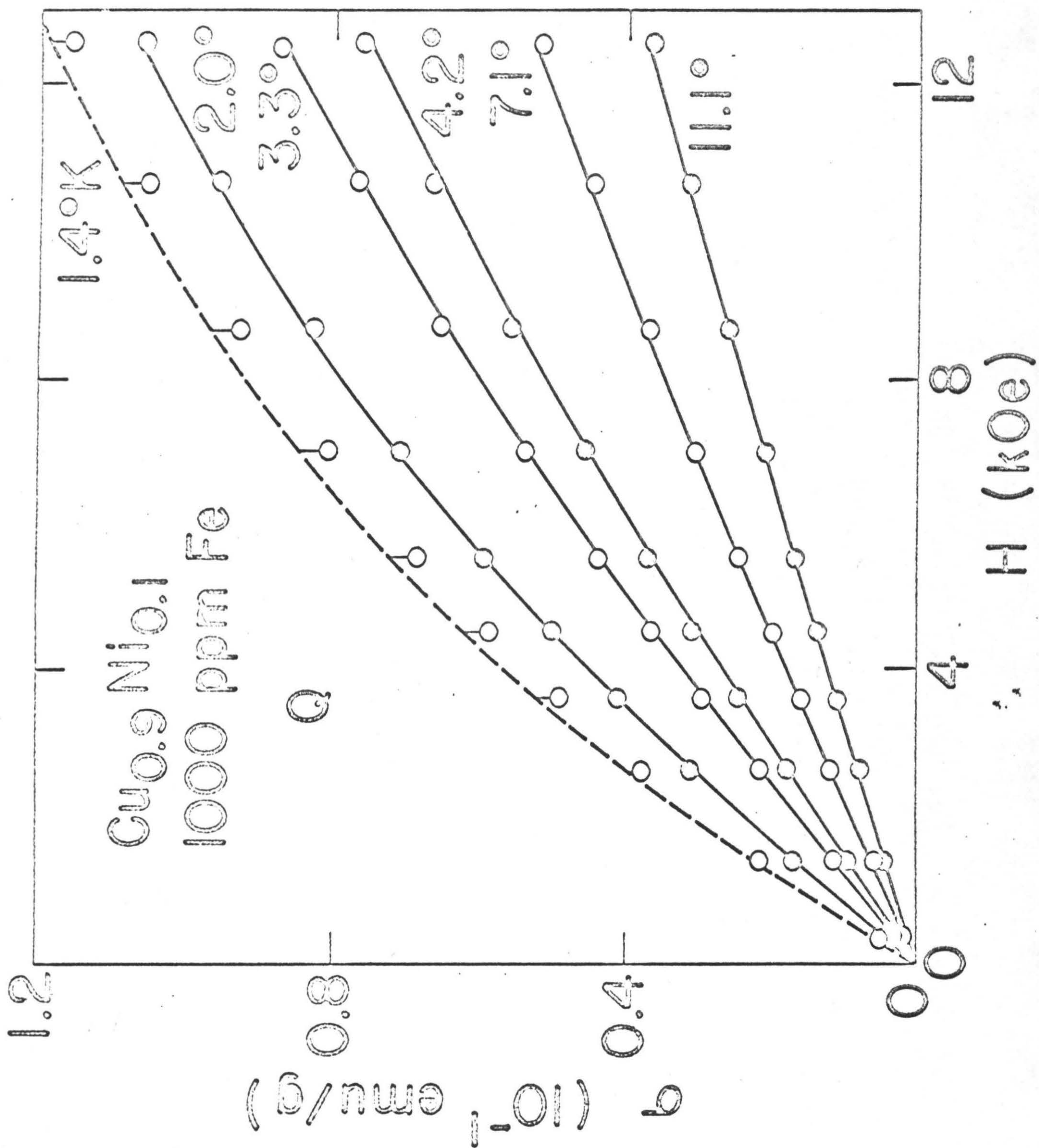




Figure 40.  $\chi$  vs.  $T$  for quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing various amounts of Fe. The solid curves were calculated using parameter values listed in Table 38.



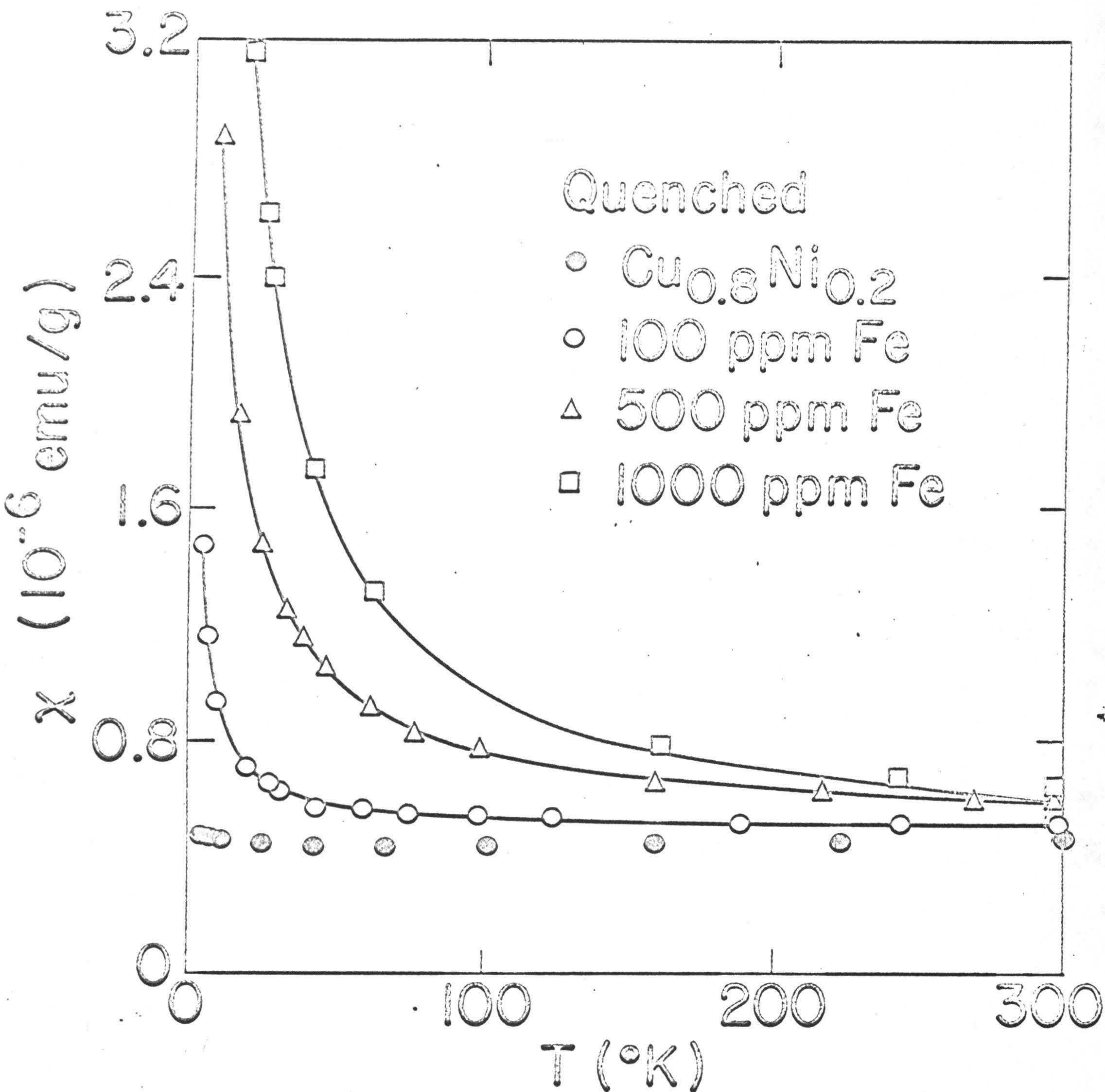




Figure 41. Magnetization vs. field for quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 100 ppm Fe. The empty and filled circles represent experimental data (Table 23). The dashed curve and the solid curves were calculated using parameter values (Table 38) obtained by least squares fitting of Eq. 11 to experimental data in the temperature range of  $2.8^\circ$  to  $\sim 300^\circ\text{K}$ .



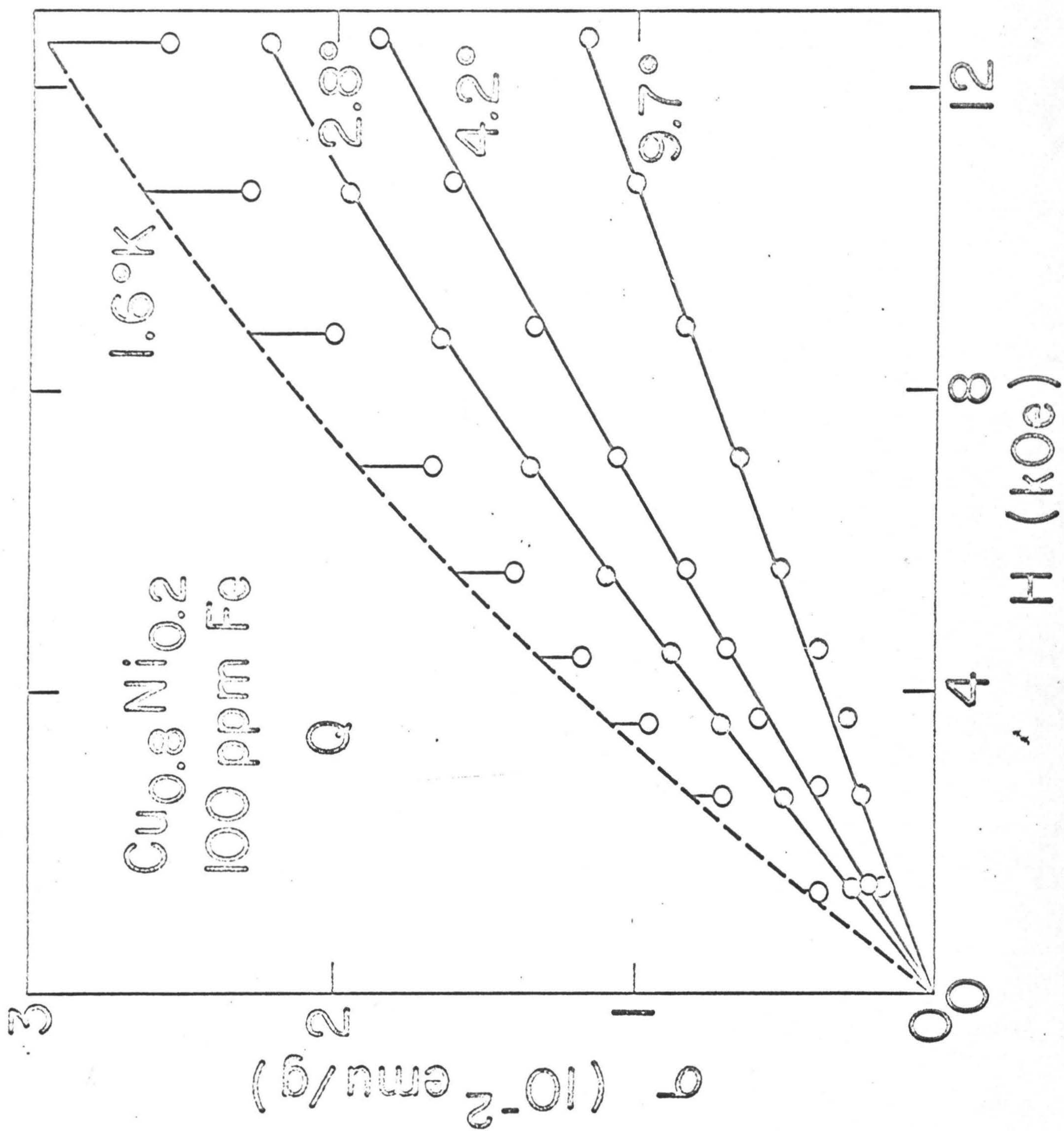




Figure 42. Magnetization vs. field for quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 500 ppm Fe. The empty and filled circles represent measured data (Table 25). The solid curves were calculated using parameter values listed in Table 38.



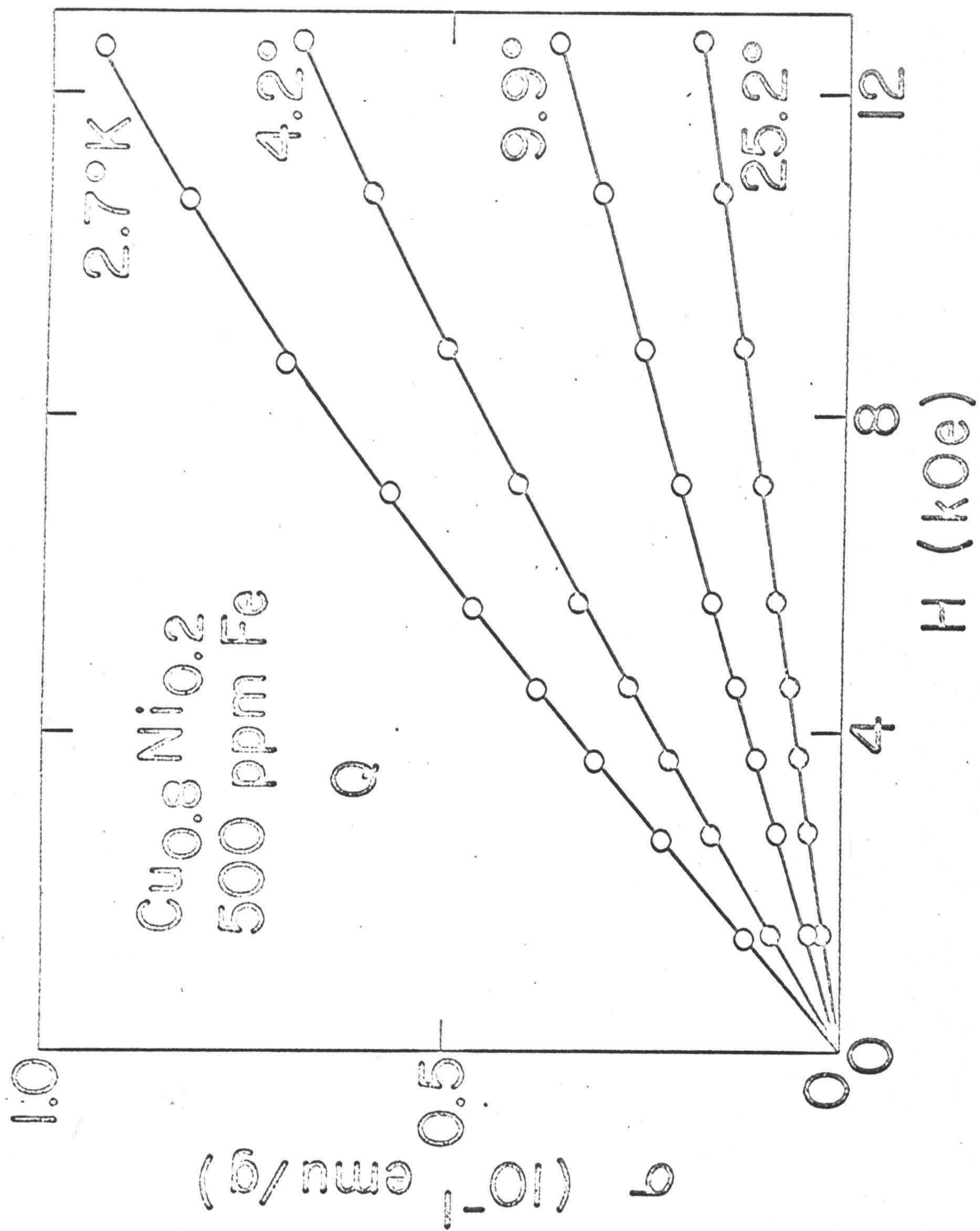
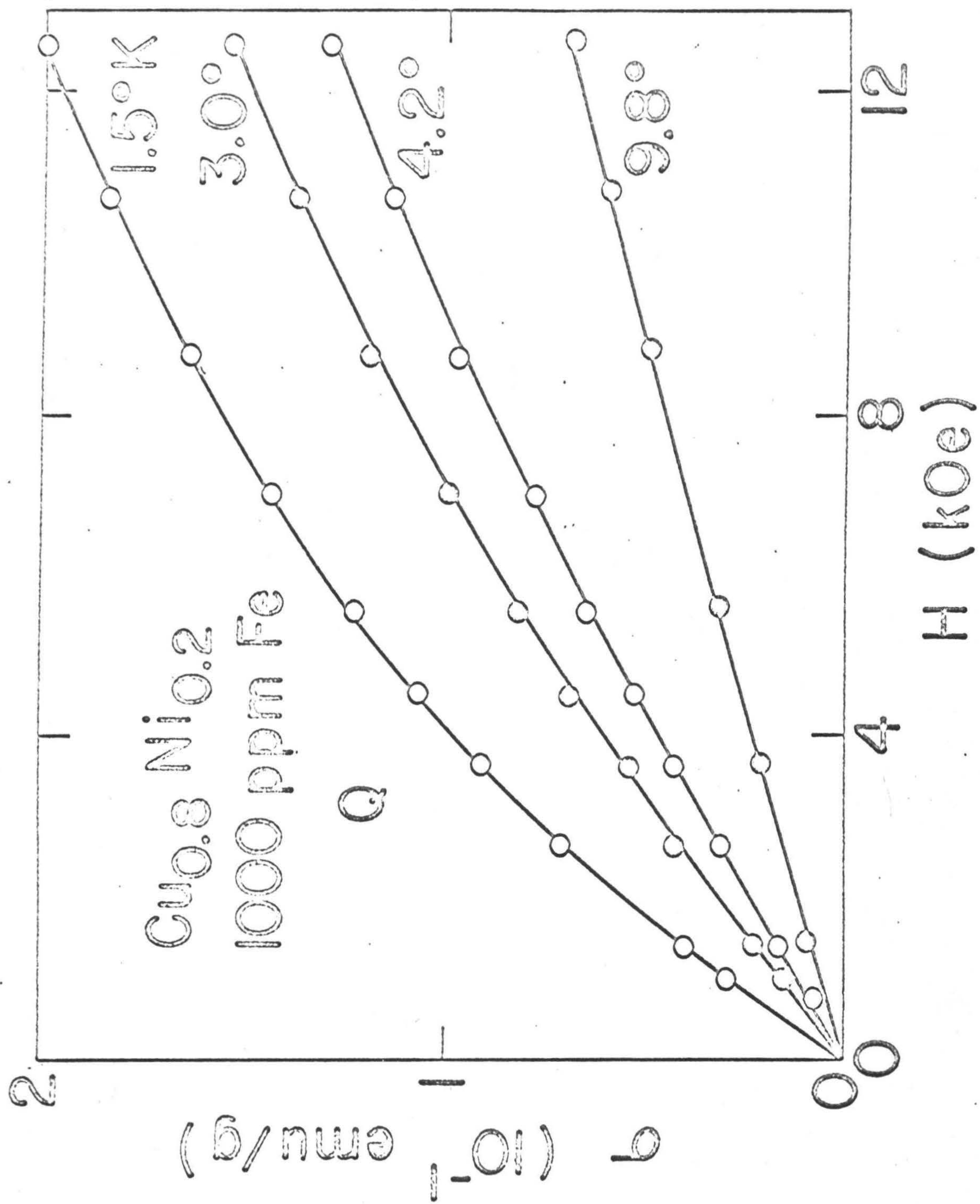




Figure 43. Magnetization vs. field for quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 1000 ppm Fe. The empty and filled circles represent measured data (Table 26). The solid curves were calculated using parameter values listed in Table 38.







addition of Fe. The parameter values obtained by least squares fitting are given in Table 39; the fit is shown in Fig. 44.

b. Deformed alloys.

The analysis of the data for the deformed alloys was more laborious, since in the deformed state the assumption of thermal equilibrium is not appropriate and the concentrations  $c_1$ ,  $c_2$ , and  $c_3$  can not be derived from a single parameter  $\text{Fe-Fe}^{\alpha_1}$  as was done for the quenched alloys. It was therefore necessary to consider two of the concentrations, i.e.,  $c_1$  and  $c_2$  as independent, with only the condition  $c_1 + 2c_2 + 3c_3 = z$  imposed. The deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing either 500 ppm Fe, or 1000 ppm Fe were analyzed in this way, by least squares fitting Eq. 13. The data for the deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing 100 ppm Fe were analyzed, as those for the corresponding quenched alloys, but fitting Eq. 11 in the manner described above. The results for all these alloys are given in Tables 40 and 41 and the fits are presented in Figures 45 through 52.

The effect of deformation in all cases was to decrease the magnetization, at any temperature and field, as compared with that for the quenched alloy. Table 42 lists the percentage decrease in magnetization at 4.2°K for the different alloys. In Fig. 53 the decrease in the magnetization on deforming the quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing 100 and 1000 ppm Fe is well illustrated.



Table 39. Parameters from least squares fitting of Eq. 11 to magnetization of the quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy containing 100 ppm Fe minus the magnetization of  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  without the Fe.

| Temp. Range ( $^{\circ}\text{K}$ ) | 4.2 to $\sim 300$ |
|------------------------------------|-------------------|
| $\mu_1$ ( $\mu_{\text{B}}$ )       | 5.20              |
| $\mu_2$ ( $\mu_{\text{B}}$ )       | 12.95             |
| $c_1$                              | 87.6              |
| $c_2$                              | 6.2               |
| $\theta_1$                         | + 0.25            |
| $\theta_2$                         | -14.1             |
| $\chi_0$ ( $10^{-6}$ emu/g)        | - 0.019           |
| $\text{Fe-Fe}^{\alpha 1}$          | 0.013             |
| $c_2/c_1$                          | 0.071             |
| rmsd ( $10^{-3}$ emu/g)            | 0.179             |
| rmsd (%) <sup>*</sup>              | 0.90              |

<sup>\*</sup>The rmsd as expressed in percents of the highest magnetization value used in the fitting.



Figure 44.  $\Delta\sigma_{\text{Fe}}$  vs.  $H$  at  $4.2^\circ\text{K}$  and  $\Delta\chi_{\text{Fe}}$  vs.  $T$  for quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy with 100 ppm Fe. Measured data points:  $\odot, \circ$ ; curves calculated with parameter values from Table 39.



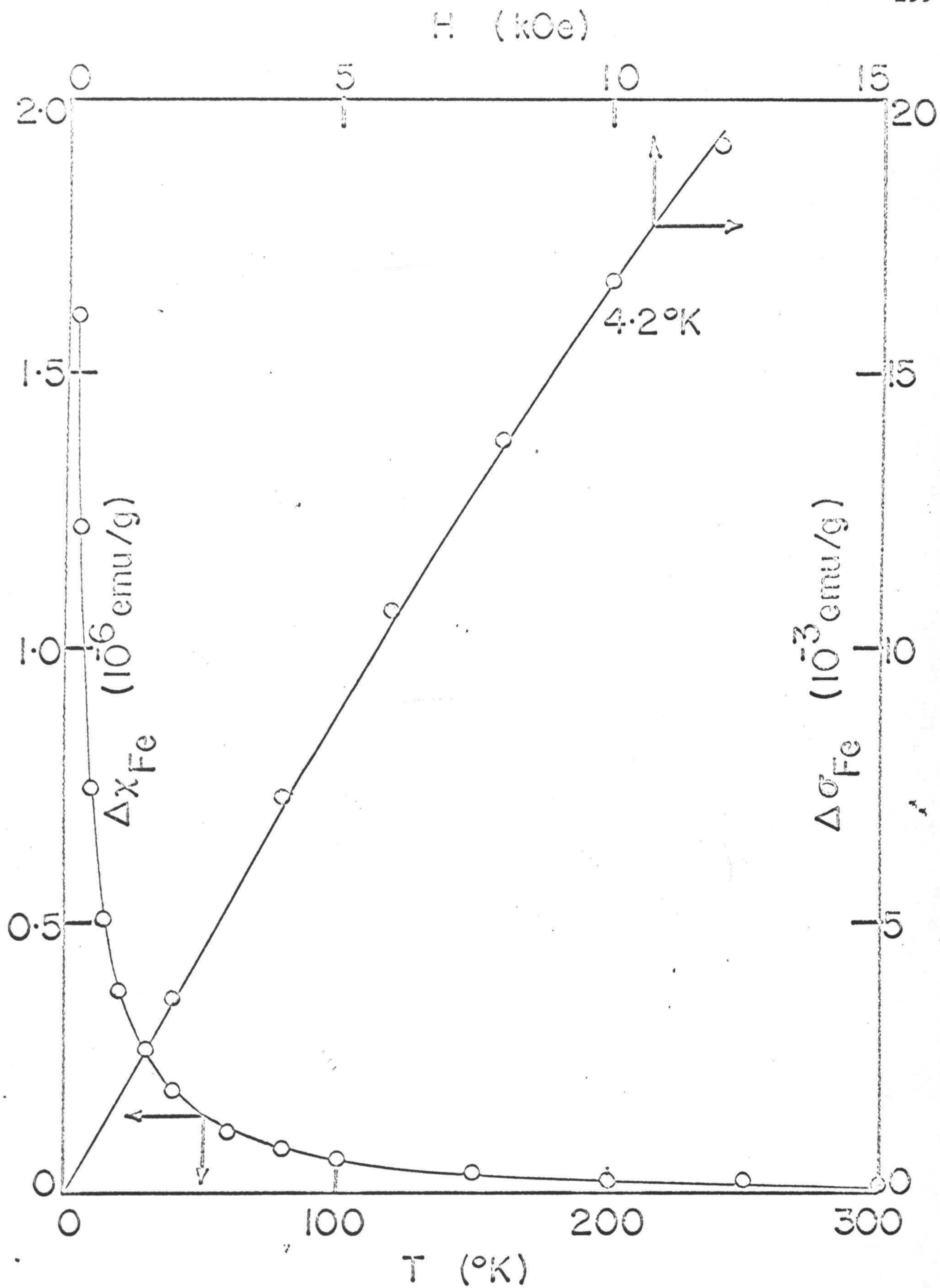




Table 40. Parameters from least squares fitting of Eq. 11 or Eq. 13 to magnetization data for deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys containing Fe.

| Fe Content (ppm)                   | 100                | 500                | 1000               |
|------------------------------------|--------------------|--------------------|--------------------|
| Temp. range ( $^{\circ}\text{K}$ ) | 1.44 to $\sim 300$ | 1.36 to $\sim 300$ | 2.30 to $\sim 300$ |
| $\mu_1$ ( $\mu_B$ )                | 2.50               | 2.50               | 2.62               |
| $\mu_2$ ( $\mu_B$ )                | 4.38               | 6.02               | 5.56               |
| $\mu_3$ ( $\mu_B$ )                |                    | 8.10               | 7.21               |
| $c_1$ (ppm)                        | 95                 | 394                | 699                |
| $c_2$ (ppm)                        | 2.5                | 41                 | 98                 |
| $c_3$ (ppm)                        |                    | 8                  | 35                 |
| $\theta_1$ ( $^{\circ}\text{K}$ )  | - 1.00             | - 2.14             | - 2.06             |
| $\theta_2$ ( $^{\circ}\text{K}$ )  | + 0.84             | - 0.11             | - 2.08             |
| $\theta_3$ ( $^{\circ}\text{K}$ )  |                    | - 0.19             | + 1.33             |
| $\chi_0$ ( $10^{-6}$ emu/g)        | 0.173              | 0.180              | 0.234              |
| $c_2/c_1$                          | 0.026              | 0.104              | 0.140              |
| rmsd ( $10^{-3}$ emu/g)            | 0.094              | 0.202              | 0.480              |
| rmsd (%) <sup>*</sup>              | 0.73               | 0.36               | 0.52               |

<sup>\*</sup>The rmsd value as expressed in percents of the highest magnetization value used in the fitting.



Table 41. Parameters from least squares fitting of Eq. 11 or Eq. 13 to magnetization data for deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing Fe.

| Fe Content (ppm)                   | 100                | 500                | 1000               |
|------------------------------------|--------------------|--------------------|--------------------|
| Temp. range ( $^{\circ}\text{K}$ ) | 1.44 to $\sim 300$ | 3.05 to $\sim 300$ | 1.47 to $\sim 300$ |
| $\mu_1$ ( $\mu_B$ )                | 3.75               | 3.44               | 3.66               |
| $\mu_2$ ( $\mu_B$ )                | 7.37               | 8.64               | 6.50               |
| $\mu_3$ ( $\mu_B$ )                |                    | 14.22              | 10.72              |
| $c_1$                              | 93                 | 420                | 703                |
| $c_2$                              | 3.5                | 31                 | 96                 |
| $c_3$                              |                    | 6                  | 35                 |
| $\theta_1$                         | - 0.96             | - 0.36             | - 2.31             |
| $\theta_2$                         | + 0.55             | - 3.04             | + 0.45             |
| $\theta_3$                         |                    | + 0.47             | + 0.20             |
| $\chi_0$ ( $10^{-6}$ emu/g)        | 0.479              | 0.480              | 0.423              |
| $c_2/c_1$                          | 0.037              | 0.074              | 0.136              |
| rmsd ( $10^{-3}$ emu/g)            | 0.253              | 0.199              | 0.969              |
| rmsd (%) <sup>*</sup>              | 0.98               | 0.26               | 0.54               |

\*The rmsd value as expressed in percents of the highest magnetization value used in the fitting.



Figure 45.  $\chi$  vs.  $T$  for deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys containing various amounts of Fe. The solid curves were calculated using parameter values listed in Table 40.



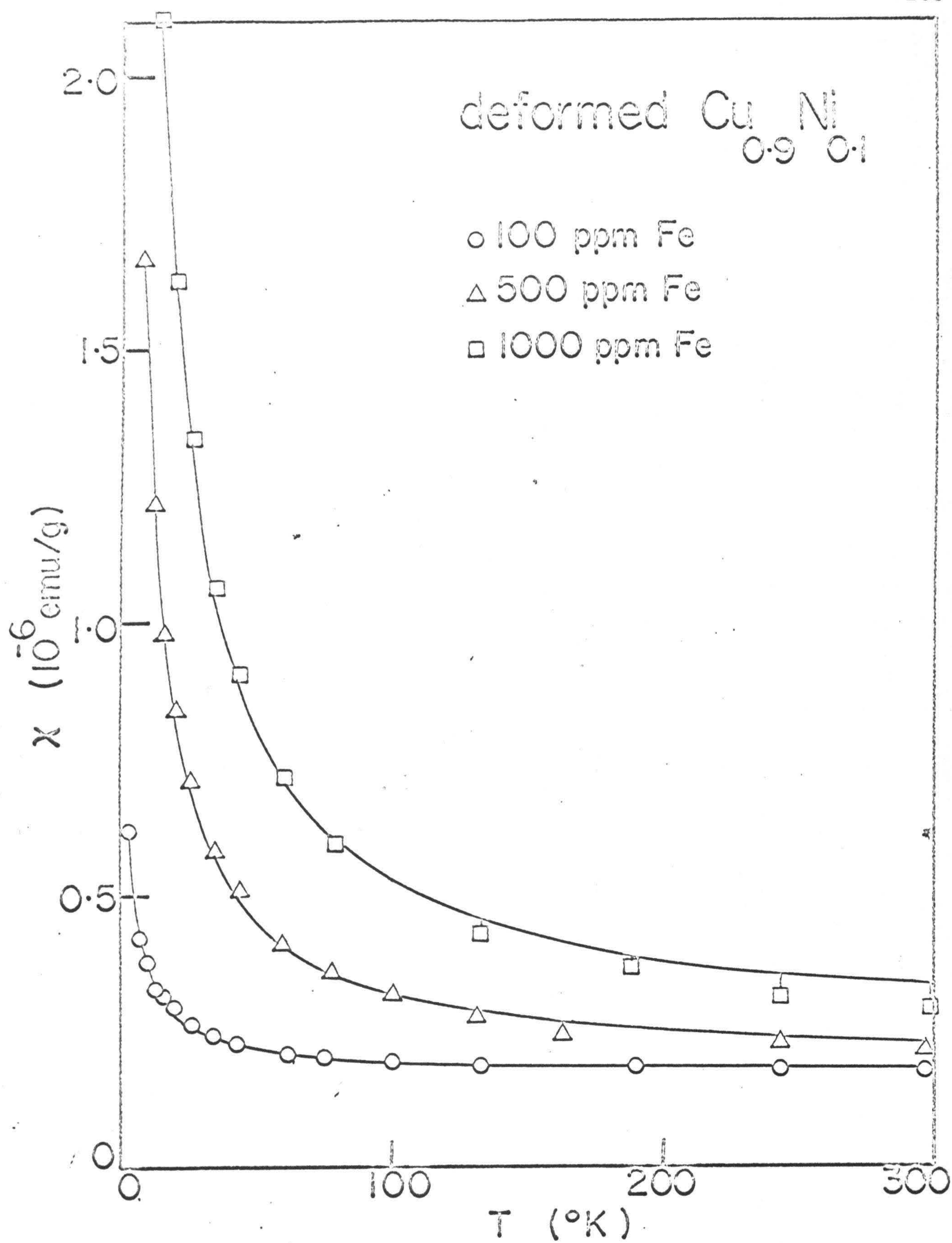




Figure 46. Magnetization vs. field for deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  with 100 ppm Fe. The empty and filled circles represent experimental data (Table 28). The solid curves were calculated using parameter values listed in Table 40.



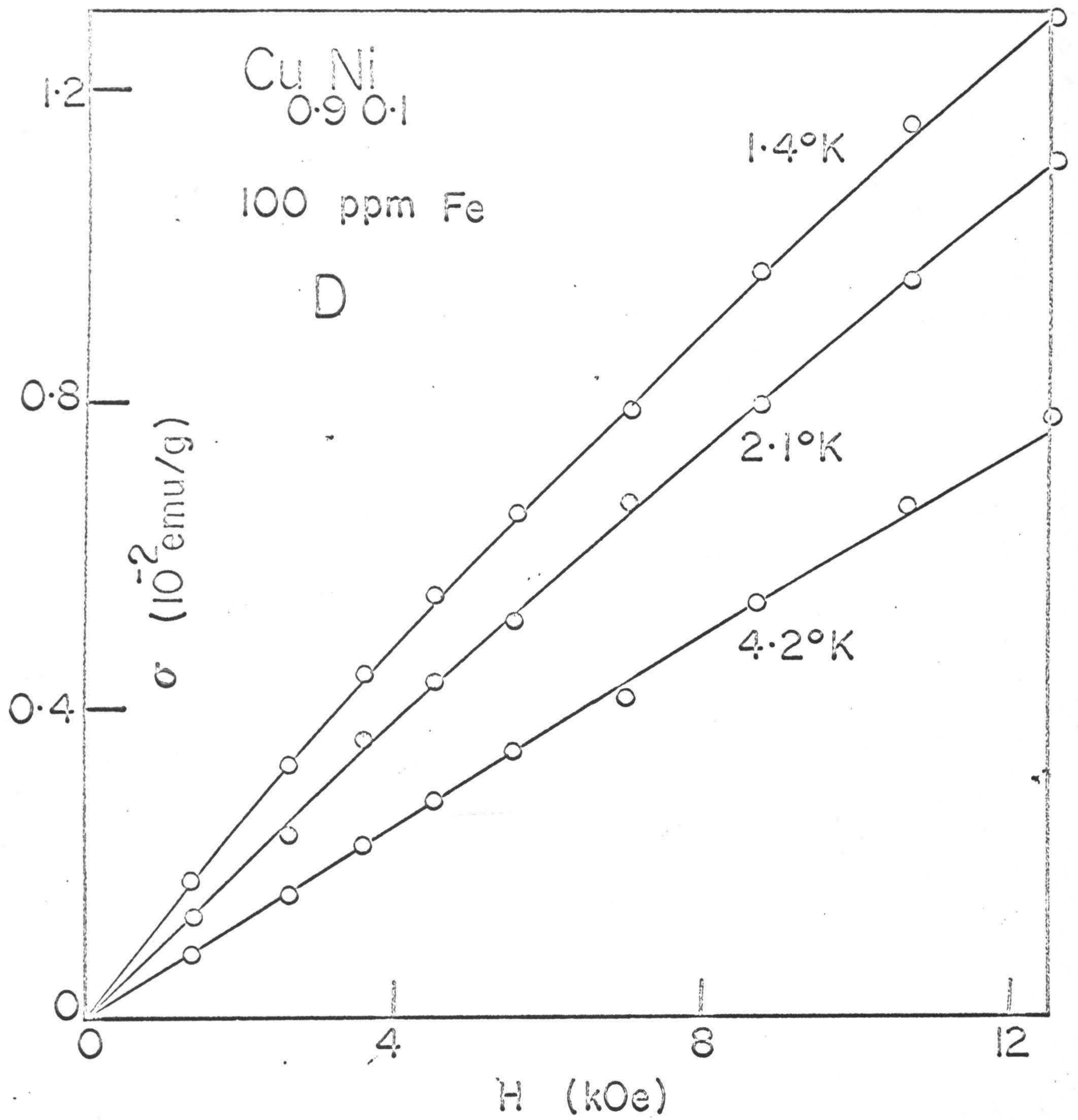




Figure 47. Magnetization vs. field for deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  with 500 ppm Fe. The empty and filled circles represent experimental data (Table 29). The solid curves were calculated using parameter values listed in Table 40.



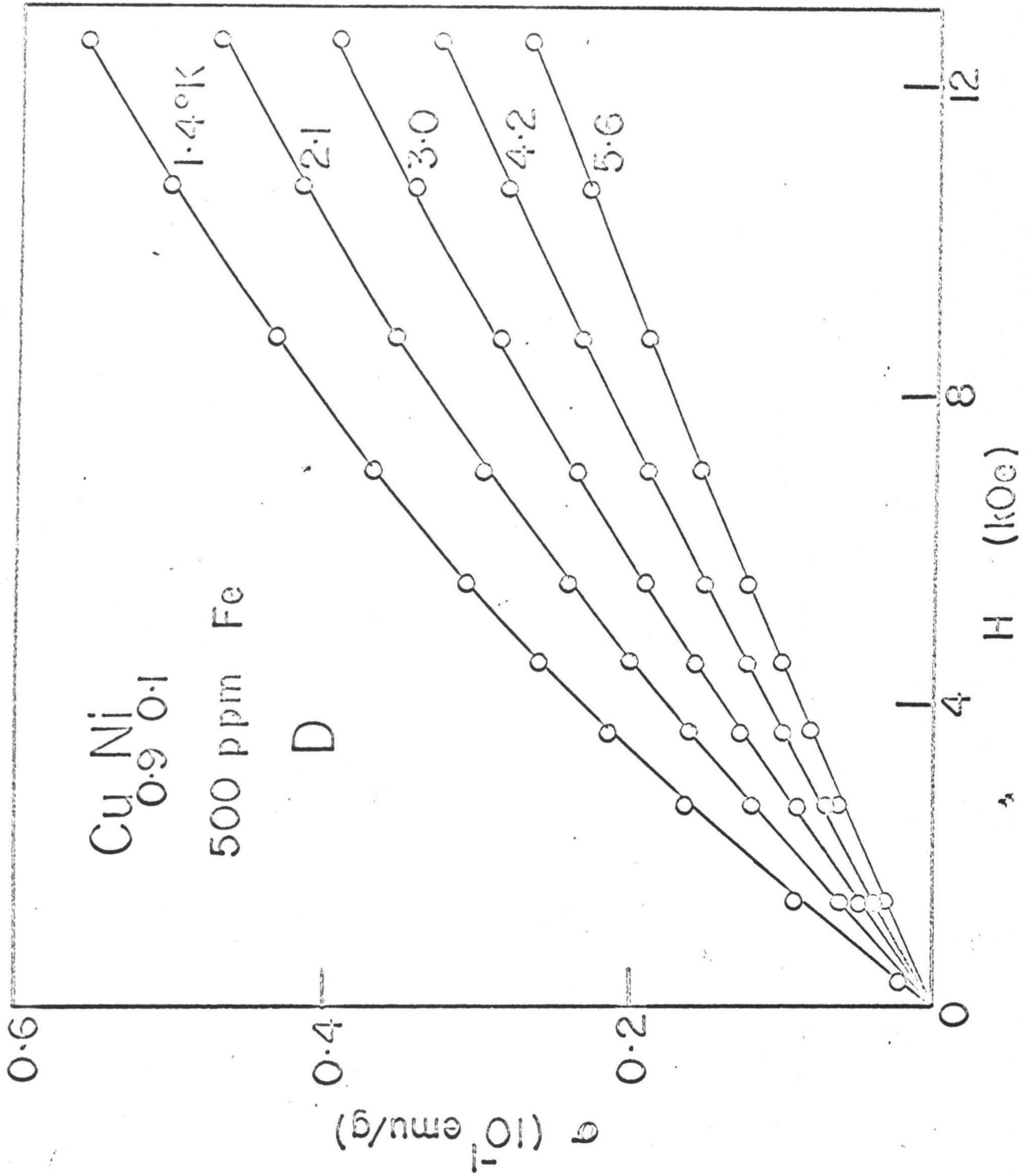




Figure 48. Magnetization vs. field for deformed  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  with 1000 ppm Fe. The empty and filled circles represent experimental data (Table 30). The dashed curve and the solid curves were calculated using parameter values (Table 40) obtained by least squares fitting of Eq. 13 to experimental data in the temperature range of  $2.3^\circ$  to  $\sim 300^\circ\text{K}$ .



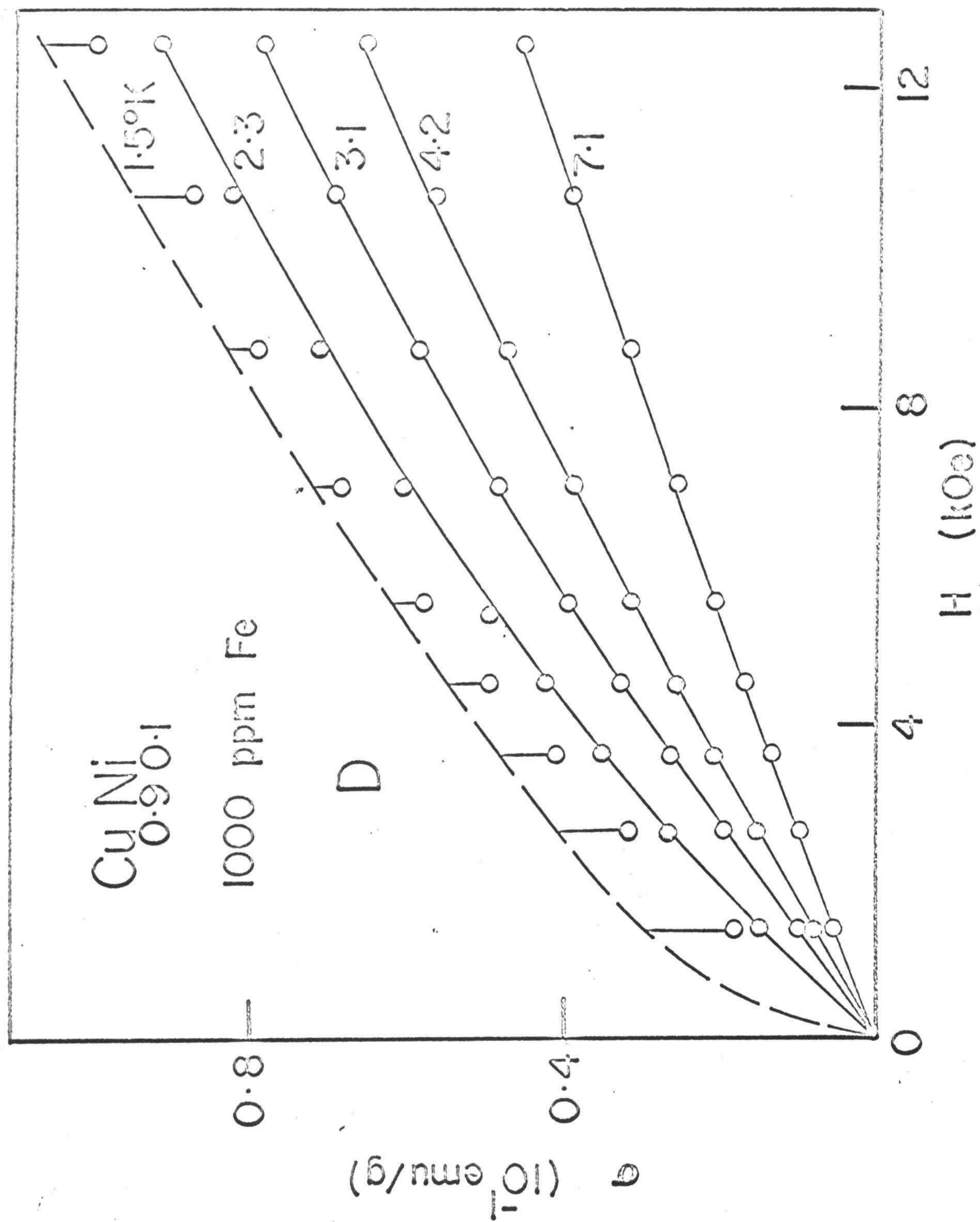




Figure 49.  $\chi$  vs.  $T$  for deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing various amounts of Fe. The solid curves were calculated using parameter values listed in Table 41.



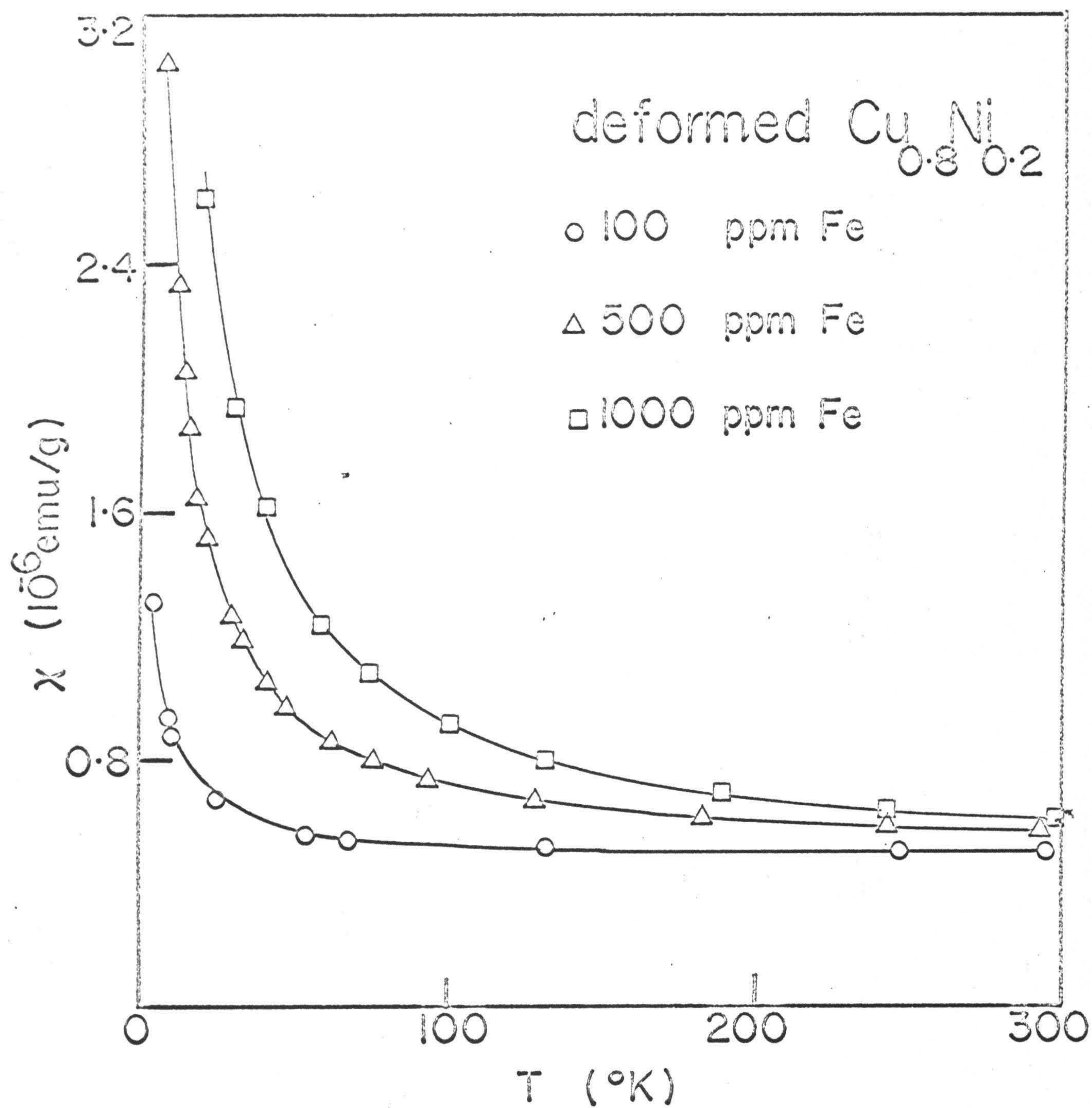




Figure 50. Magnetization vs. field for deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 100 ppm Fe. The empty and filled circles represent experimental data (Table 31). The solid curves were calculated using parameter values listed in Table 41.



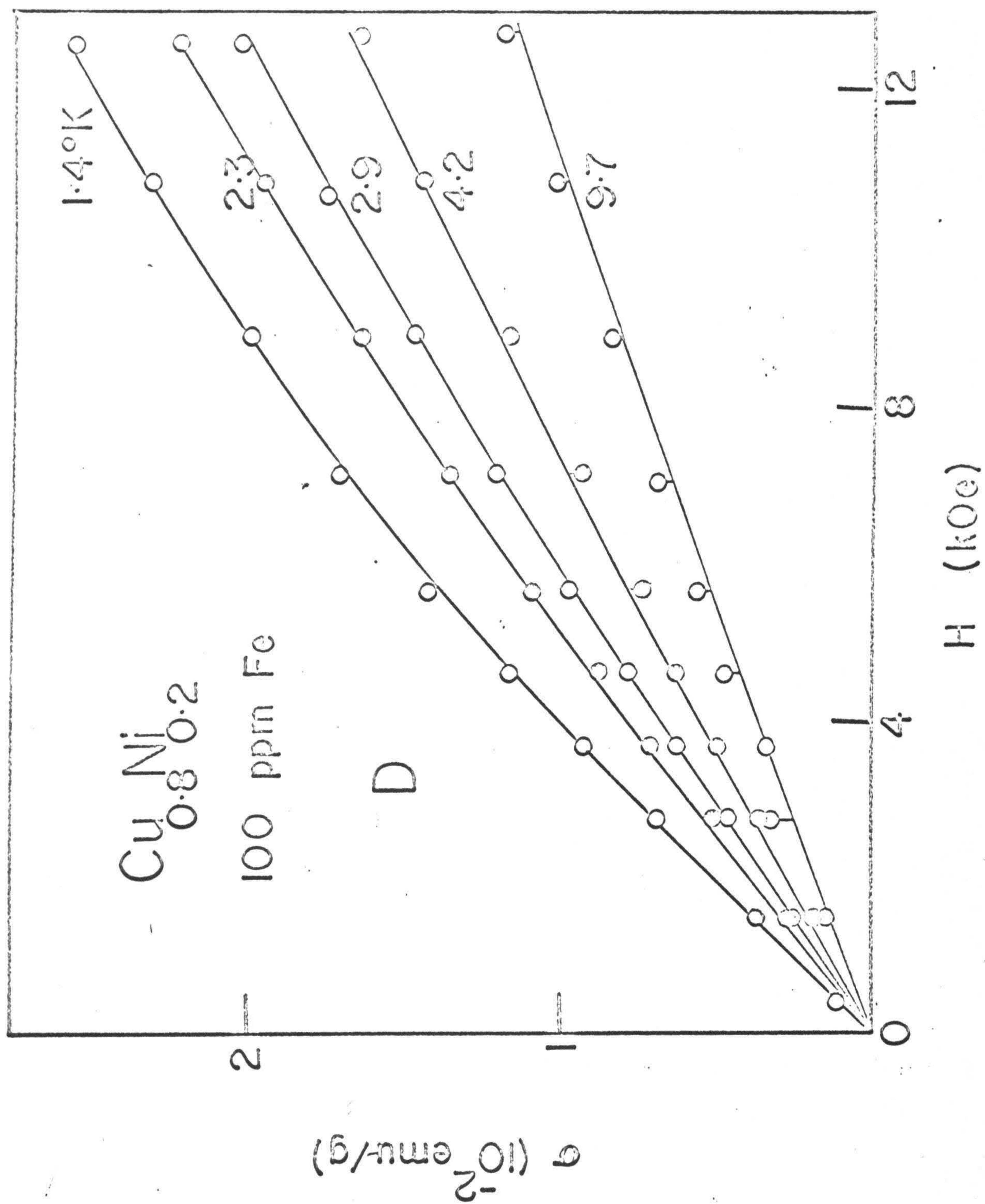




Figure 51. Magnetization vs. field for deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 500 ppm Fe. The empty and filled circles represent experimental data (Table 32). The dashed curve and the solid curves were calculated using parameter values (Table 41) obtained by least squares fitting of Eq. 13 to experimental data in the temperature range of  $3.1^\circ$  to  $\sim 300^\circ\text{K}$ .



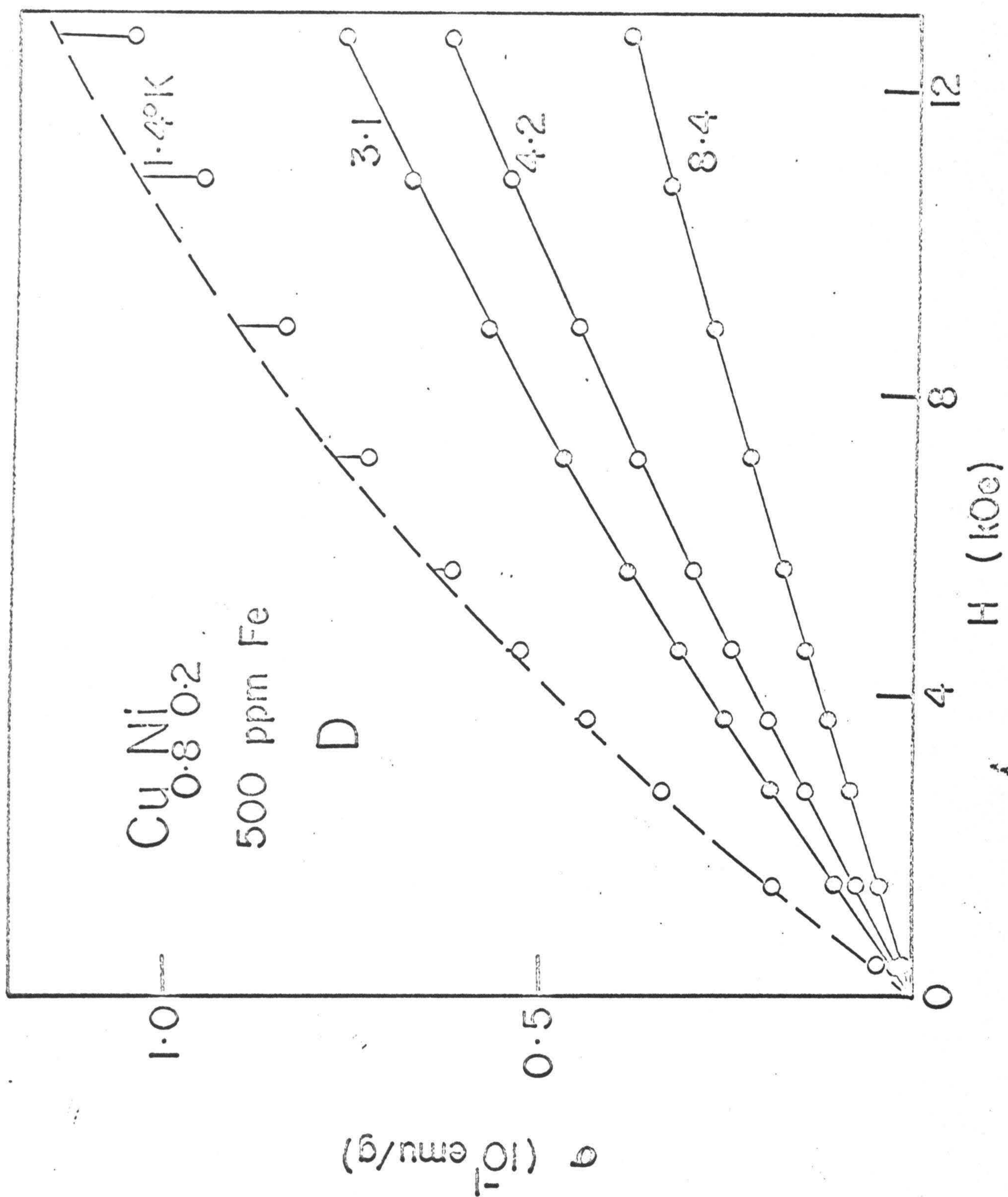




Figure 52. Magnetization vs. field for deformed  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 1000 ppm Fe. The empty and filled circles represent experimental data (Table 33). The solid curves were calculated using parameter values listed in Table 41.



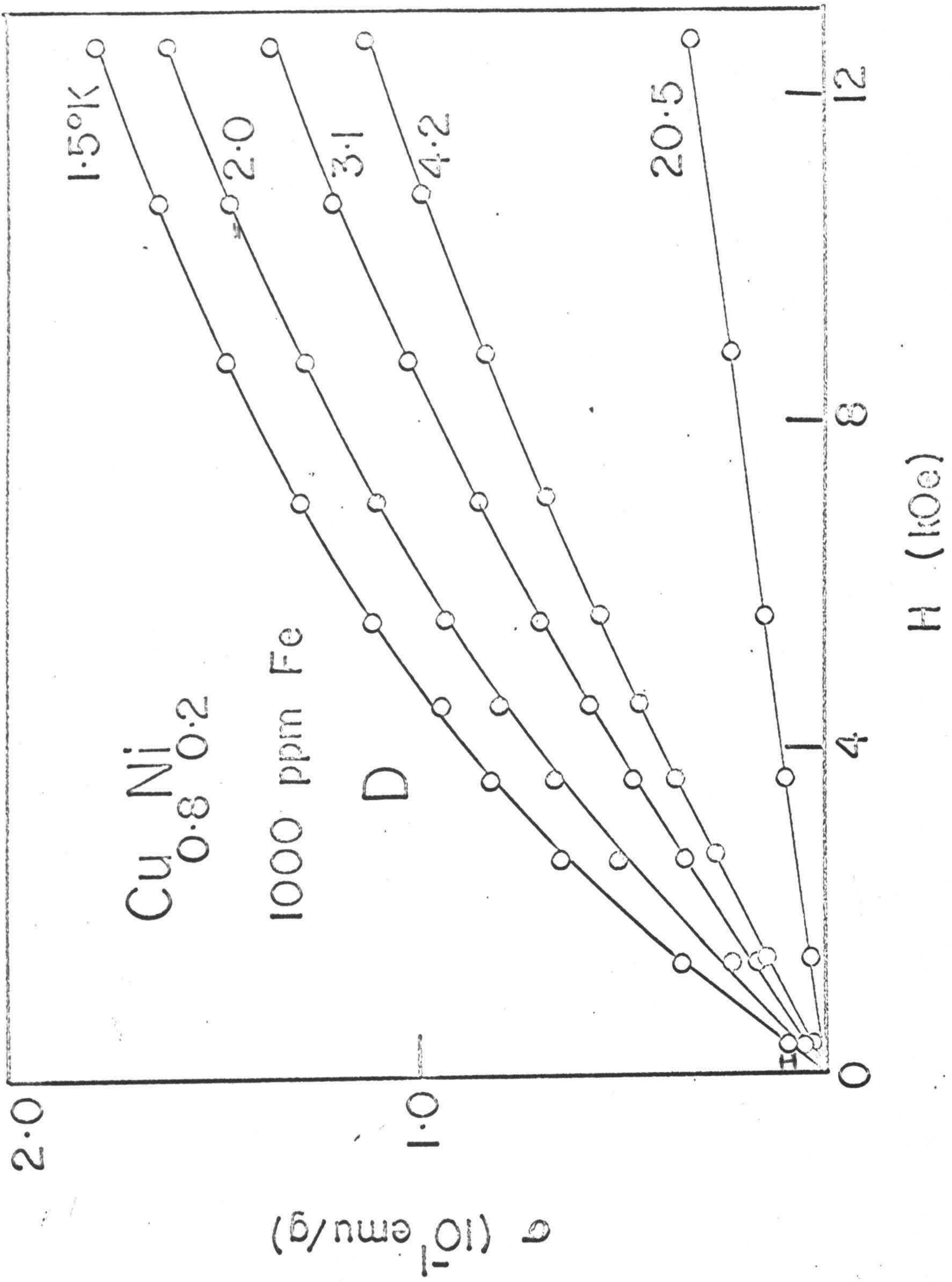




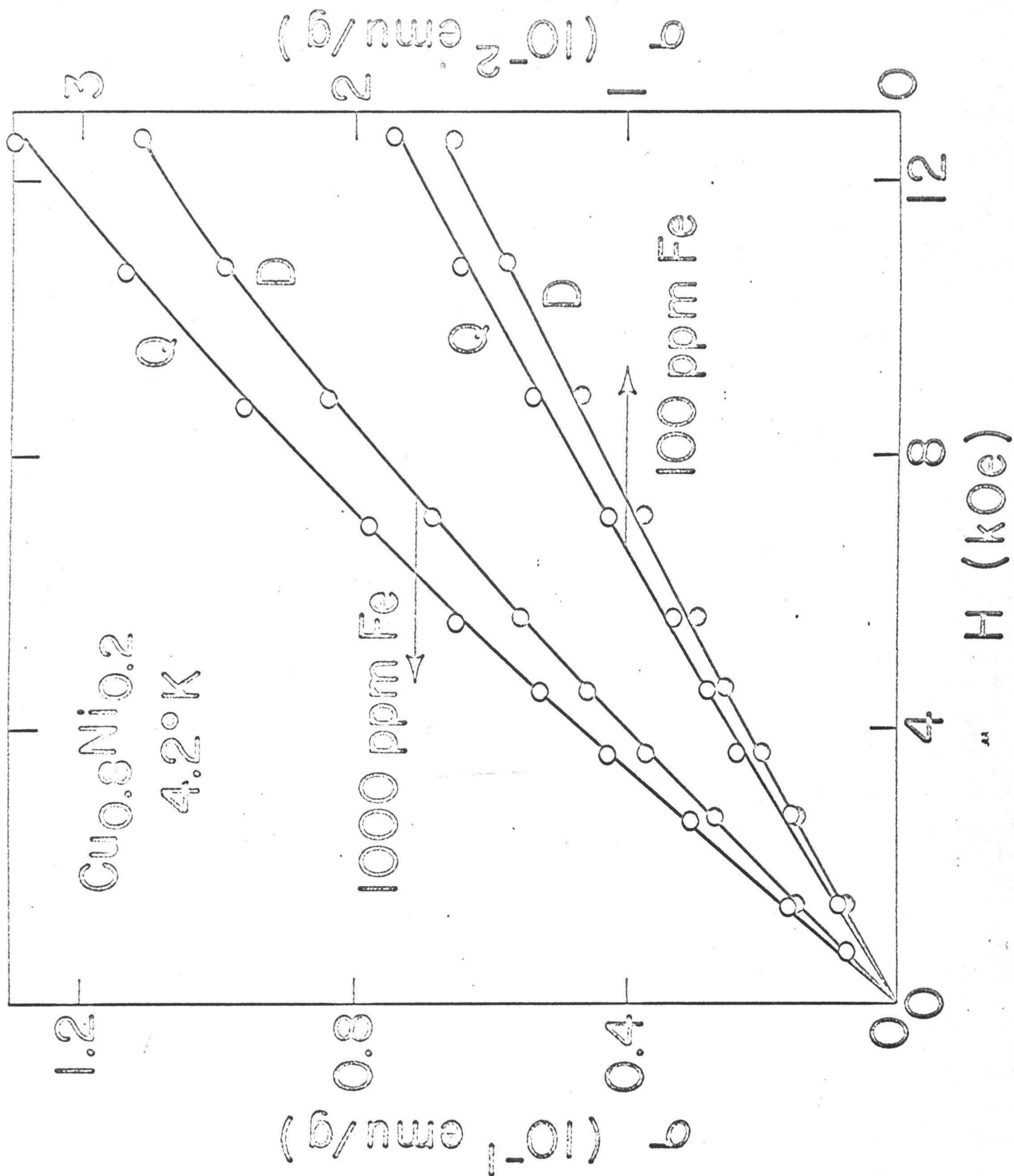
Table 42. Percentage decrease as a result of plastic deformation, of the magnetization of quenched alloys at 4.2°K in an applied field of  $\sim 12.6$  kOe.

| Alloy                                           | Magnetization<br>( $10^{-3}$ emu/g) |          | % Decrease |
|-------------------------------------------------|-------------------------------------|----------|------------|
|                                                 | Quenched                            | Deformed |            |
| 100 ppm Fe in $\text{Cu}_{0.9}\text{Ni}_{0.1}$  | 8.85                                | 7.78     | 12.1       |
| 500 ppm Fe in $\text{Cu}_{0.9}\text{Ni}_{0.1}$  | 37.95                               | 32.84    | 13.5       |
| 1000 ppm Fe in $\text{Cu}_{0.9}\text{Ni}_{0.1}$ | 76.06                               | 65.39    | 14.0       |
| 100 ppm Fe in $\text{Cu}_{0.8}\text{Ni}_{0.2}$  | 18.64                               | 16.47    | 11.6       |
| 500 ppm Fe in $\text{Cu}_{0.8}\text{Ni}_{0.2}$  | 68.65                               | 62.90    | 8.4        |
| 1000 ppm Fe in $\text{Cu}_{0.8}\text{Ni}_{0.2}$ | 129.80                              | 112.74   | 13.1       |



Figure 53. Effect of plastic deformation on the magnetization. Magnetization vs. field at 4.2°K for quenched (empty circles, Table 23) and deformed (filled circles, Table 31)  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 100 ppm Fe, and quenched (empty circles, Table 26) and deformed (filled circles, Table 33)  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  with 1000 ppm Fe.







For some of these alloys, in either the quenched or the deformed state, large systematic deviations were obtained for the data at the lowest temperature ( $\sim 1.5^\circ\text{K}$ ). In such cases deletion of these data from the fitting resulted in very satisfactory rmsd values and the deviations at higher temperatures could also be minimized. The parameter values in Tables 37 through 41 were obtained from these improved fits. A similar situation was encountered in the analysis of the data for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ . It is not unreasonable to assume that the interaction effects are large at  $T \approx 1.5^\circ\text{K}$ , so that the analysis in terms of Brillouin functions is not appropriate.

The accuracy with which the parameter values listed in Tables 37 through 41 were determined may be estimated to:  $\pm 5\%$  for  $\chi_0$  and  $\mu_1$ ,  $c_1$ ,  $\theta_1$ ;  $\pm 10\%$  for  $\mu_2$ ,  $c_2$ ,  $\theta_2$ ; and  $\pm 20\%$  for  $\mu_3$ ,  $c_3$ ,  $\theta_3$ .



## V. DISCUSSION

### A. Cu-Fe

The results of our analysis of the magnetization data for the Cu-Fe alloy with 108 ppm Fe<sup>6</sup> show (Table 36) that the magnetization of this alloy can be well described, in the temperature range of 1.3° to 32.5°K, in terms of isolated Fe, Fe pair, Fe triplet and Fe quadruplet moments. The value of  $\mu_1 = 2.44 \mu_B$  is very similar to the value of  $2.54 \mu_B$  reported by Tholence and Tournier;<sup>6</sup> it is also in excellent agreement with the results of Franz and Sellmyer,<sup>21</sup> who estimated  $\mu = 2.4 \pm 0.4 \mu_B$ , from Curie-Weiss analysis of initial susceptibility data above  $\sim 10^\circ\text{K}$ , for Cu-Fe alloys containing 447 and 842 ppm Fe. The value of  $\mu_2 = 4.86 \mu_B \approx 2\mu_1$  is not very far from the corresponding value ( $\sim 5.4 \mu_B$ ) reported by Tholence and Tournier<sup>6</sup> on the basis of the concentration dependence of the magnetization. The principal differences between the earlier<sup>6</sup> and the present interpretation of the data are the presence of dipoles with  $\mu_3 \approx 7.22 \mu_B$  attributable to groups of three Fe atoms and giant moments of the value of  $\mu_4 = 10.17 \mu_B$ , and in the values of  $\theta$  and  $c$  for the single and double Fe dipoles. It is worth noting that the fit is equally good in the entire temperature range (Fig. 32) without any indication of a decrease of  $\mu_1$  and  $\mu_2$ , either by spin compensation or by local spin fluctuations, at temperatures as



low as  $1.3^\circ\text{K}$  (i.e.,  $T < 10^{-1}T_K$  where  $T_K$ , the lowest Kondo temperature reported in literature,<sup>24,25</sup> is about  $15^\circ\text{K}$ ).

The present evaluation of the data of Hirschkoff et al.<sup>9</sup> in the lower temperature range of  $\sim 0.01^\circ\text{K}$  to  $\sim 0.04^\circ\text{K}$ , for a Cu-Fe alloy with 112 ppm Fe indicates the absence here of any appreciable concentration of single Fe dipoles giving rise to a corresponding temperature- and field-dependence of the magnetization expressed by a Brillouin function. Hirschkoff et al.<sup>9</sup> concluded on the basis of the concentration dependence of the magnetization that single Fe dipoles are absent. The least squares fitting of Eq. 13 shows that a Brillouin term corresponding to Fe pair dipoles is absent as well. The large values obtained from these data for  $\mu_1$ ,  $\mu_2$ , and  $\mu_3$  (Table 36) apparently represent averages for a distribution of magnetic clusters, each of which involves more than two Fe moments. Assuming each Fe moment in the clusters to be  $2.2 \mu_B$ , the concentration of all Fe atoms participating in dipoles and contributing to the temperature- and field-dependence of the magnetization described by Brillouin functions may be estimated as only about 1.7 ppm, i.e., less than 2% of the total Fe concentration in the alloy.

The question arises here whether the large majority of Fe atoms, which do not contribute to the temperature-dependent magnetization below  $0.4^\circ\text{K}$ , may be responsible for the large increase of the temperature independent susceptibility to  $\chi_0 = 8.7 \times 10^{-8}$  emu/g over the corresponding value of  $\chi_0 = 0.48 \times 10^{-8}$  emu/g for the higher temperature range (Table 36). One



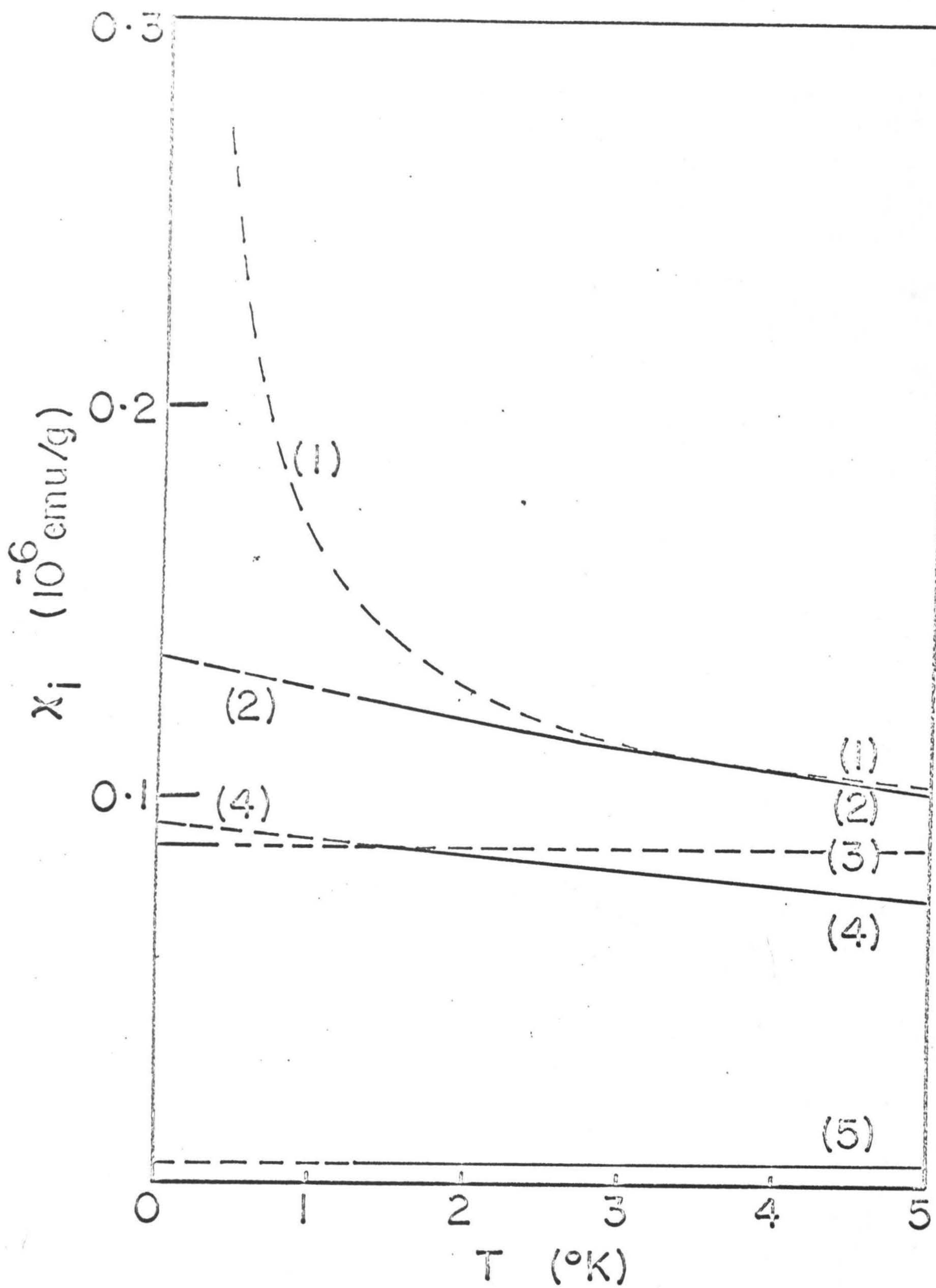
interpretation would be that the isolated Fe moments, present at and above 1.3°K, are fully compensated below 0.4°K. Some authors have suggested<sup>24,25</sup> that the susceptibility at 0°K for a spin compensated Kondo system is  $\sim \frac{p^2}{3kT_K}$  where  $p^2 = \mu_{\text{effective}}^2 = \mu(\mu+2)$ . Assuming  $T_K \sim 15^\circ\text{K}$   $\chi_0 \approx 8 \times 10^{-8}$  emu/g, in good agreement with the value of  $\chi_0$  in the lower temperature range. However an alternative explanation, not requiring the assumption of spin compensation, is also in good agreement with the data. As seen in Fig. 54 the magnitude of the increase in the field and temperature independent susceptibility,  $\Delta\chi_0 = 8.2 \times 10^{-8}$  emu/g, agrees quite well with the sum,  $8.6 \times 10^{-8}$  emu/g, of the initial susceptibilities due to the single Fe, the Fe pair and the triple Fe moments, extrapolated to 0.4°K from the higher temperature range. Because of the large negative values of the corresponding  $\theta_1$ ,  $\theta_2$  and  $\theta_3$  (see Table 36), these initial susceptibilities are practically temperature-independent below 0.4°K. At the low values of the external field used in the measurements,<sup>9</sup> they are nearly independent of the field as well, so that they are incorporated into  $\chi_0$  in the least squares fitting. Also, extrapolation of the remaining Brillouin term, corresponding to  $\mu_4 = 10.17 \mu_B$ , from the higher temperature range to 0.4°K gives a magnetization value in close agreement with the sum of the values at the same temperature of the three Brillouin terms obtained for the lower temperature range. Thus, one may conclude that the present interpretation of the available magnetic data for the copper alloys with approximately 110 ppm Fe



Figure 54.  $\chi_i$  vs.  $T$  for Cu-Fe with  $\sim 110$  ppm Fe:

- (1) Total initial susceptibility above  $0.4^\circ\text{K}$  as extrapolated from the data below  $0.4^\circ\text{K}$  of Hirschkoﬀ et al.<sup>9</sup>
- (2) Total  $\chi_i$  (dashed part is an extrapolation below  $1.3^\circ\text{K}$ ); data above  $1.3^\circ\text{K}$  from Tholence and Tournier.<sup>6</sup>
- (3) Temperature independent susceptibility  $\chi_0$  (dashed part is an extrapolation above  $0.4^\circ\text{K}$ ) as obtained from analysis of the data below  $0.4^\circ\text{K}$ , Hirschkoﬀ et al.<sup>9</sup>
- (4) The sum of the initial susceptibilities due to  $\mu_1 = 2.44$ ,  $\mu_2 = 4.86$  and  $\mu_3 = 7.22$ , and  $\chi_0 = 0.48 \times 10^{-8}$  emu/g, as obtained from the analysis of the data above  $1.3^\circ\text{K}$ , Tholence and Tournier<sup>6</sup> (dashed part is an extrapolation below  $1.3^\circ\text{K}$ ).
- (5) Temperature independent susceptibility  $\chi_0$  (dashed part is an extrapolation below  $1.3^\circ\text{K}$ ) from analysis of the data above  $1.3^\circ\text{K}$ , Tholence and Tournier.<sup>6</sup>







in the two temperature ranges is self consistent and that it does not require the loss of Fe moments by spin compensation or local spin fluctuation, even at temperatures as low as 0.012°K.

It is an interesting question whether the finding of Hirsch-koff et al.<sup>9</sup> that the susceptibility in the lower temperature range scales with the second power of the Fe concentration can be reconciled with the absence in the same temperature range of a Brillouin term corresponding to the Fe pair moment of about  $4.86 \mu_B$ . According to the interpretation outlined in the preceding paragraph, the dipoles with single Fe and with Fe pair moments are in fact present, but they contribute only to the temperature- and field-independent susceptibility  $\chi_0$ . Also, if the single Fe moments are compensated by the Kondo mechanism, their contribution to  $\chi_0$  will be essentially the same. The dependence of the total susceptibility on the Fe concentration represents an average of the concentration dependence of  $\chi_0$  and of the various Brillouin terms in Eq. 14. This average may approximately correspond to the square of the Fe concentration, provided that  $\chi_0$  itself is proportional to a lower than second power of the concentration, so that it can compensate the effect on the average of the Brillouin terms, which vary with a higher than second power of the Fe concentration. It is clearly apparent in Fig. 1 of Ref. 9 that the compensation is indeed approximately achieved at 0.4°K. One would not expect it to continue, however, as the temperature is decreased, since the Brillouin terms enter the average with a larger weight at lower temperatures. In fact, Fig. 1 of Ref. 9 shows that the graphs



representing the alloys with different Fe contents diverge. For instance, at  $T = 0.08^\circ\text{K}$  the susceptibility values would have to be divided by the 1.8th, rather than the 2nd, power of the respective Fe concentrations in order to bring about approximate superposition, analogous to that achieved at  $0.4^\circ\text{K}$  through division by the square of the concentration. Thus, the scaling of the susceptibility with the second power of the Fe-concentration, discovered by Hirschkoﬀ et al.,<sup>9</sup> clearly represents the average concentration dependence of the various susceptibility terms at  $0.4^\circ\text{K}$ . As pointed out above, such an average presupposes that  $\chi_0$  scales with a lower than second power of the concentration, i.e., that it comprises an appreciable contribution from either compensated or uncompensated single Fe moments, a contribution essentially linear in Fe-concentration. It may be, therefore concluded that the concentration-dependence of the susceptibility<sup>9</sup> does not contradict the analysis of its field-and-temperature-dependence given in the present work.

On the basis of their neutron magnetic scattering studies with a Cu-Fe alloy, Stassis and Shull<sup>26</sup> recently concluded that at  $4.2^\circ\text{K}$  there is absence of any large contribution to the total magnetization by field-induced polarization in the compensating conduction electron cloud. Window<sup>7</sup> concluded, through his Mössbauer effect study of the saturation hyperfine field at isolated Fe nuclei in Cu-Fe alloys, that even at temperatures as low as  $1.4^\circ\text{K}$  all the susceptibility can be accounted for by the localized Fe moments, with no contribution from the compensating spin cloud. In view of these findings, and of the results of Tholence



and Tournier,<sup>6</sup> based on the concentration dependence, it appears at present that neither spin compensation nor local spin fluctuations make any noticeable contribution to the magnetization at low temperatures. The present analysis of the field- and temperature-dependence of the magnetization values measured by Tholence and Tournier<sup>6</sup> for 108 ppm Fe in Cu, confirms that the single moments remain unchanged at least to 1.3°K.

In order to explain the high concentration of magnetically interacting pairs of Fe moments for a random alloy, it has been suggested<sup>6</sup> that the Fe atoms participating in a pair moment may not necessarily be nearest neighbors of one another, but that a long range magnetic coupling may be provided between them by the RKKY mechanism. On the other hand, more recent Mössbauer work<sup>7,8</sup> indicates the presence in dilute Cu-Fe alloys (with Fe contents as low as ~200 ppm<sup>8</sup>) of relatively large concentrations of Fe nearest neighbor pairs and of larger aggregates. It is therefore more plausible to assume that the Fe pair moments and the larger magnetic clusters revealed by the present analysis are associated with nearest neighbor Fe atoms.<sup>27</sup> For more concentrated Cu-Fe alloys (0.2 to 1.71 at. %) Svensson<sup>28</sup> had in fact concluded, from results of magnetic susceptibility measurements, that atomic clustering is present in quenched alloys and that on cold working there is a change in the magnetic structure from clusters to a statistical dispersion of Fe atoms. The ratio of the concentration of Fe-pair moments and of single-Fe moments derived in the present analysis (Table 36) from the



108 ppm Fe alloy data of Tholence and Tournier<sup>6</sup> requires a nearest-neighbor short range order parameter  $\text{Fe-Fe}^{\alpha}_1$  of  $\sim 0.017$ .

A maximum in the magnetization (Fig. 35) at approximately  $0.02^\circ\text{K}$  is observed in the 10 Oe data of Hirschkoff et al.<sup>9</sup> for a Cu-Fe alloy with 478 ppm Fe. A similar maximum is found at a lower temperature in their<sup>9</sup> data for the alloy with 380 ppm Fe; for the alloys with still lower Fe contents (e.g., 112 ppm Fe, Fig. 34) a clear-cut maximum is not indicated within the temperature range of the measurements. Such a maximum was found, in the present investigation, for the quenched  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  alloy at approximately  $4.3^\circ\text{K}$  (Fig. 29). At lower temperatures the magnetization values measured after cooling the specimen in a magnetic field are higher than those obtained after the specimen was cooled in zero field. Such thermomagnetic history effects, found in mictomagnetic alloys have been interpreted<sup>29, 30</sup> in terms of an interaction of magnetic clusters with the frozen spin-glass matrix in which they are dispersed. In the case of the  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  alloy the pronounced curvature in the  $\sigma$  vs.  $H$  graphs at low temperatures (Fig. 26) indicates the presence of large magnetic clusters. The freezing of the spin orientations at low temperatures in Cu-Fe alloys has been concluded from the occurrence of hyperfine splitting in the Mössbauer spectrum.<sup>7,10,11</sup> By interpolation from the Mössbauer ordering temperatures the freezing of the spin-glass matrix in the quenched  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  alloy may be estimated to take place at  $8 \pm 1^\circ\text{K}$ . That the maximum in the magnetization in Fig. 29 does not correspond to a



Néel temperature is shown by the fact that it does not coincide with the Mössbauer ordering temperature. The quenched  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  alloy has a remanence temperature of  $2.8^\circ \pm 1.4^\circ\text{K}$ . Franz and Sellmyer<sup>27</sup> observed remanence below  $3.5^\circ\text{K}$  for a Cu + 0.6% Fe alloy. That long range antiferromagnetic order is in fact absent from the frozen spin system in Cu-Fe alloys is strongly suggested by the close analogy of their magnetic properties, including the occurrence of remanence, with those of the mictomagnetic Cu-Mn alloys. In the latter the absence of long range antiferromagnetism has been demonstrated by neutron diffraction.<sup>31</sup>

The occurrence of a magnetization maximum suggests that Cu-Fe alloys containing as low an Fe level as 380 ppm may be mictomagnetic.

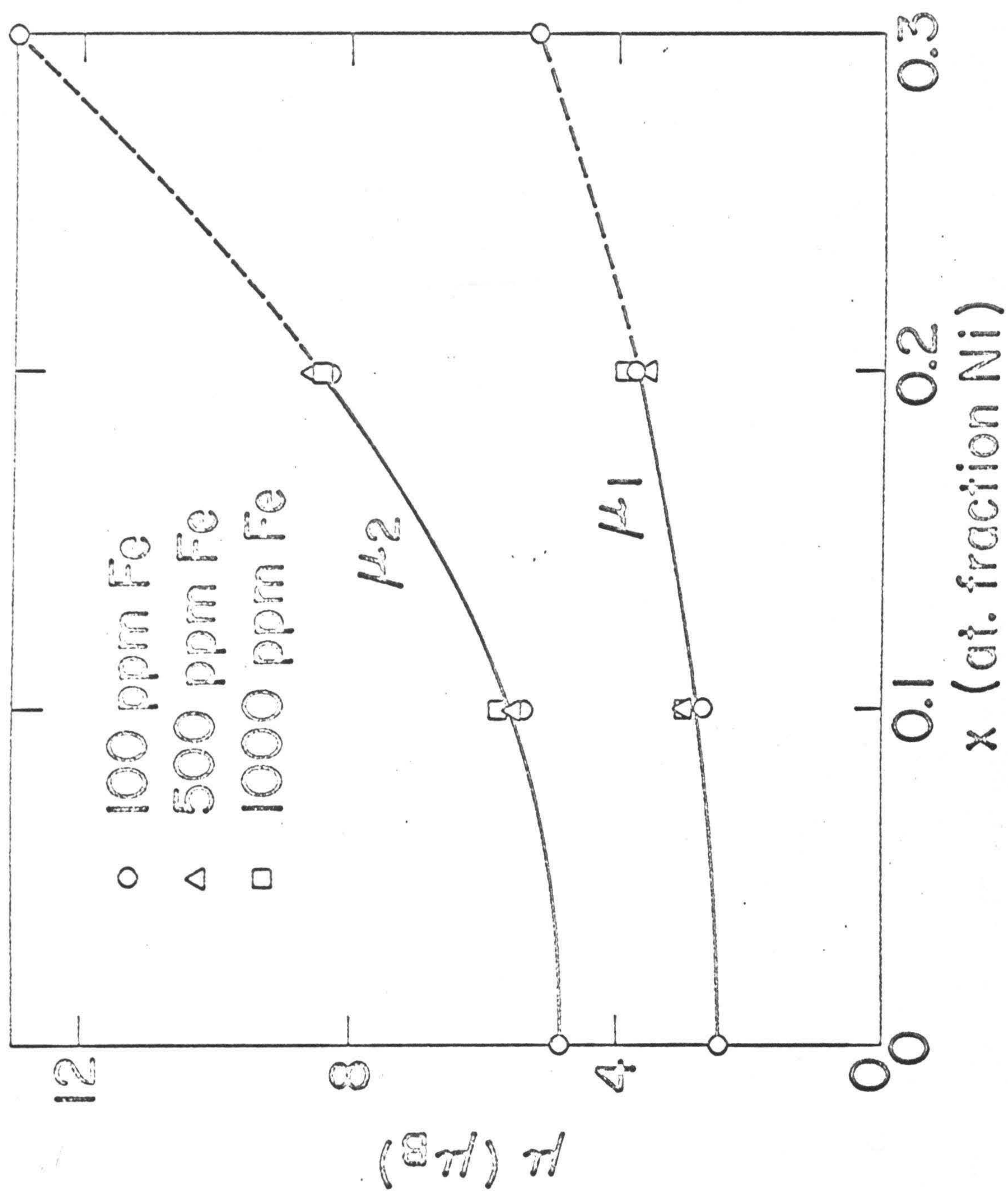
#### B. Cu-Ni-Fe

As seen in Figures 36, 40, and 44, Fe additions in amounts of 100 to 1000 ppm increase very much the temperature dependent susceptibility of  $\text{Cu}_{0.9}\text{Ni}_{0.1}$ ,  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  and  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloys. Analysis of the data for the quenched alloys (Tables 37, 38, and 39) indicate that the magnetization of most of these alloys can be well described in a very wide temperature range ( $\sim 2.5^\circ$  to  $250^\circ\text{K}$ , i.e., over two decades) in terms of magnetic clusters of three average sizes:  $\mu_1$ ,  $\mu_2$ , and  $\mu_3$ . Figure 55 shows that at a given Ni concentration, the  $\mu_1$  (and  $\mu_2$ ) values for different Fe contents agree very well. As a function of the Ni concentration  $\mu_1$  increases from  $2.44 \mu_B$  in pure Cu to  $5.2 \mu_B$  in



Figure 55.  $\mu_1$  and  $\mu_2$  for quenched Cu-Ni-Fe alloys as a function of Fe and Ni contents. The  $\mu_1$  and  $\mu_2$  values for 100 ppm Fe in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  may involve some error due to the clustering tendency in this alloy of the Ni atoms, giving rise to magnetic dipoles.<sup>1</sup>







$\text{Cu}_{0.7}\text{Ni}_{0.3}$  (Fig. 55); the corresponding increase in  $\mu_2$  is from  $4.86 \mu_B$  to  $12 \mu_B$ . In view of the fact that in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  the nickel atoms themselves tend to form magnetic clusters,<sup>1</sup> the values of  $\mu_1$  and  $\mu_2$  for  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  as shown in Fig. 53 may be slightly in error. The value of  $\mu_1 = 3.76 \mu_B$  for the quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloy with 100 ppm Fe is exactly the same as indicated in a preliminary report<sup>2</sup> for a quenched alloy of the same composition, on the basis of high field magnetization data at  $4.2^\circ\text{K}$  and of susceptibility data between  $4.2^\circ\text{K}$  and  $300^\circ\text{K}$ . The increase of  $\mu_1$  with the Ni content is qualitatively consistent with the results of Bennett *et al.*<sup>3</sup> for single Fe clusters. It is seen in Tables 37, 38, and 39 that for all alloys the ratio  $\mu_2/\mu_1$  roughly corresponds to  $\sim 2$  irrespective of the Fe and Ni concentrations. One may then conclude that  $\mu_1$  and  $\mu_2$  are indeed the moments associated with single Fe and Fe pair clusters. The value of  $\mu_3$  does not always correspond to  $\sim 3\mu_1$  (Tables 37, 38, and 39) and it may represent an average moment for all clusters containing three or more Fe atoms.

It may be noted in Tables 37, 38, and 39 that for each quenched alloy the best fit to the data is obtained when the ratio of the concentration of the single Fe moment to the concentration of Fe pair moments is such as to correspond to a finite positive value of  $\text{Fe-Fe}^{\alpha_1}$  suggesting that the Fe atoms in these alloys tend to cluster. On the other hand Bennett *et al.*<sup>4</sup> proposed that the concentrations of the single Fe and Fe pair moments can be explained, on the basis of a random alloy



model, in which two Fe moments may be coupled via nearest neighbor Ni moments. In order to compare this model with experimental results the concentration of isolated Fe and Fe pair moments may be calculated on the basis of the model in the following manner. Figure 56 shows the atomic sites near an Fe atom at the origin (Site 0) in a f.c.c. structure. According to the model of Bennett et al.<sup>4</sup> the moment on the Fe atom at site 0 can be magnetically coupled, for example, to another Fe moment at site 9, provided that sites 1 and 4 are occupied by Ni atoms, which in the model are assumed to have  $0.6 \mu_B$  each. The types of couplings by nearest neighbor sequences that are allowed are: Fe-Fe, Fe-Ni-Fe and Fe-Ni-Ni-Fe. This rules out the possibility of magnetic coupling when the second Fe atom is at site 8, or at 9b which is another type of 9<sup>th</sup>-nearest neighbor, or at any site more distant than the 9<sup>th</sup>-nearest neighbor, since in all these cases more than two intermediate Ni atoms would be required for "connection" by a nearest neighbor sequence. Table 43 lists the spatial co-ordinates of one site in each shell up to the 9th-nearest, and the number  $S_i$  of crystallographically equivalent sites on shell  $i$ , where  $i$  varies from 1 to 9. The total number of sites which can be connected to site 0, under the assumptions made, is 146. Also listed in Table 43 are the probabilities of connection for Fe atoms at the various sites, through at least one path of two or less nearest neighbor Ni atoms, as a function of the Ni concentration  $x$ . For a given value of  $i$ , that is for the second Fe atom in any one of the  $S_i$  equivalent sites, on



Figure 56. Some atomic sites in an f.c.c. structure.



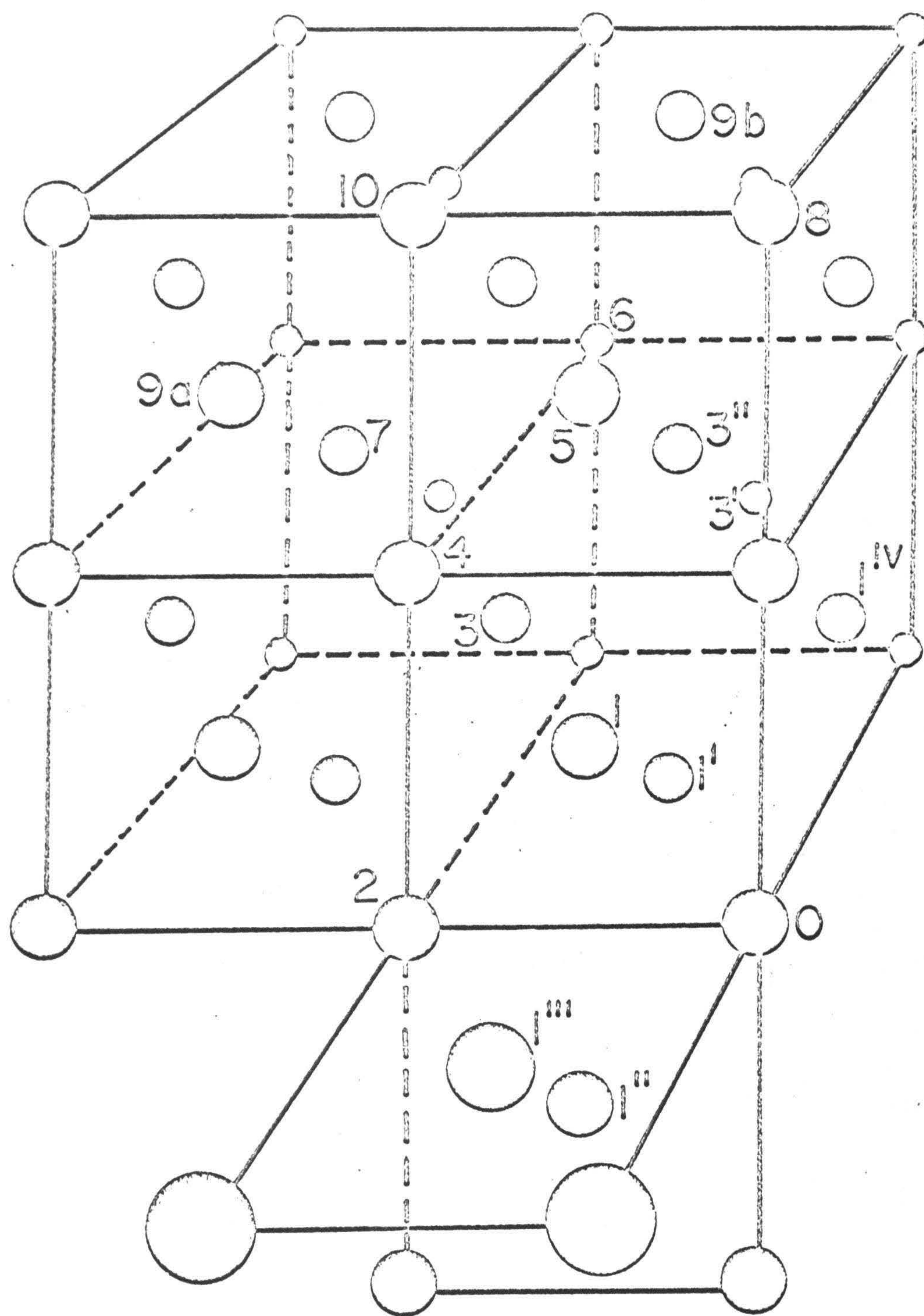




Table 43. Connection probabilities for random alloy.

| Shell No. | Location of atoms                               | No. of atoms in shell i | Probability of connection through at least one path of two or less nearest neighbor Ni atoms |
|-----------|-------------------------------------------------|-------------------------|----------------------------------------------------------------------------------------------|
| i         |                                                 | $S_i$                   | $P_i$                                                                                        |
| 1         | $\langle \frac{1}{2}, \frac{1}{2}, 0 \rangle$   | 12                      | 1                                                                                            |
| 2         | $\langle 1, 0, 0 \rangle$                       | 6                       | $1 - (1-x)^4$                                                                                |
| 3         | $\langle 1, \frac{1}{2}, \frac{1}{2} \rangle$   | 24                      | $1 - (1-x)^2 [1 - x\{1 - (1-x)^2\}]^2$                                                       |
| 4         | $\langle 1, 1, 0 \rangle$                       | 12                      | $1 - (1-x)(1-x^2)^4$                                                                         |
| 5         | $\langle 1\frac{1}{2}, \frac{1}{2}, 0 \rangle$  | 24                      | $6x^8 - 24x^7 + 35x^6 - 24x^5 + 15x^4 - 16x^3 + 9x^2$                                        |
| 6         | $\langle 1, 1, 1 \rangle$                       | 8                       | $-2x^6 + 6x^5 - 3x^4 - 6x^3 + 6x^2$                                                          |
| 7         | $\langle 1\frac{1}{2}, 1, \frac{1}{2} \rangle$  | 48                      | $3x^2 - 2x^3$                                                                                |
| 8         | $\langle 2, 0, 0 \rangle$                       | 6                       | 0                                                                                            |
| 9a        | $\langle 1\frac{1}{2}, 1\frac{1}{2}, 0 \rangle$ | 12                      | $x^2$                                                                                        |
| 9b        | $\langle 2, \frac{1}{2}, \frac{1}{2} \rangle$   | 24                      | 0                                                                                            |

Note: Total number of connectable sites: 146.



shell  $i$  of the first one, the connection probability  $P_i$  is the same. This rule, of course, breaks down for  $i=9$ , i.e., for the 9<sup>th</sup> nearest neighbor shell where we have two types of sites: 9a and 9b. The manner in which the probabilities  $P_i$  were derived may be illustrated by means of a few examples.

(1) The second Fe atom is at site 1: In this case, since the two Fe atoms are nearest neighbors of each other, they are coupled regardless of the Ni concentration and the probability of connection,  $P_1$ , is equal to 1.

(2) The second Fe atom is at site 2: Here the coupling can occur provided there is a Ni atom in site 1 or in any of the three alternative connecting sites ( $1'$ ,  $1''$ ,  $1'''$ ). The probability of finding a Ni atom at a given site is  $x$ , and that of a Cu atom is  $(1-x-z)$  where  $z$  is the Fe concentration. Since  $z$  is very small (1000 ppm or 0.001 at the maximum) compared to  $x$  (0.100 at the minimum), one may write the probability of finding a Cu atom at a given site as  $(1-x)$ . The probability that all four connecting sites under consideration are simultaneously occupied by Cu atoms is  $(1-x)^4$ ; the probability that not all of the four sites are occupied by Cu atoms, i.e., the probability that at least one of the four sites is occupied by a Ni atom is given by  $1-(1-x)^4$ . This is the probability,  $P_2$ , of an Fe atom in the second nearest shell being coupled to the Fe atom at the origin via a Ni intermediary.

(3) The second Fe atom is at site 3: In this case, the coupling may be achieved through one or two Ni atoms. Referring



to Fig. 56, the first type of coupling can occur only if there is a Ni atom at at least one of the sites 1 or 1'. The probability that both of these sites are occupied by Cu atoms is  $(1-x)^2$ . The second type of coupling may occur in either of the following two ways: (a) Given a Ni at  $1^{IV}$ , there should be another Ni atom at least at one of the two sites designated by 3' and 3''. The probability of such an event is  $1-(1-x)^2$ . The probability of connection through at least one path of two Ni atoms is  $\{1-(1-x)^2\}$ ; and  $1-x\{1-(1-x)^2\}$  is the probability that both of these alternative paths are being blocked by Cu atoms. (b) Given a Ni atom at 2, there should be a Ni atom at least at one of the sites 1'' or 1'''. The situation is identical with the one just discussed and so is the connection probability. Finally, one obtains the total probability of all the possible single Ni or double Ni paths being blocked by Cu atoms as equal to  $(1-x)^2 [1-x\{1-(1-x)^2\}]^2$ . Then the probability,  $P_3$ , of the Fe atom at site 3 being connected to the one at site 0, through at least one path of two or less nearest neighbor Ni atoms is  $1-(1-x)^2 [1-x\{1-(1-x)^2\}]^2$ . The connection probabilities  $P_4$ , and  $P_{9a}$  for Fe-sites in shells  $\underline{i} = 4$ , and 9a were derived in a similar fashion.

In the determination of the connection probability  $P_1$ , or  $P_2$ , or  $P_3$  above (or  $P_4$ , or  $P_{9a}$ ), the connecting paths in each case were independent of one another, i.e., each possible connecting path involved Ni sites not involved in any of the other possible connecting paths. Because of the independence of the



paths the calculation was fairly simple. The same results can also be obtained by a more direct but laborious approach by calculating first the probability of each possible arrangement of copper and nickel atoms at the connecting sites, then discarding those configurations which are identical, and finally adding up the probabilities of only those not-identical configurations which provide a "connecting path" through one or two Ni atoms. In the calculation of the connection probabilities  $P_5$ ,  $P_6$  and  $P_7$  such an approach had to be followed, since in these cases the different possible connecting paths are interlinked. Thus, to connect an Fe atom at a site marked 7 (i.e.,  $i = 7$ , Fig. 56) to the Fe atom at site 0, it is necessary to have Ni atoms (a) at sites 1' and 3; or (b) at sites 1 and 3, or (c) at sites 1 and 4. Clearly paths (a), (b) and (c) are not independent of one another.

Given an Fe atom A at site 0, the average number of Fe atoms in its  $i$ -shell is  $zS_i$ , and the probability of finding an Fe atom at a given site in the  $i^{\text{th}}$  shell, that is connected to the Fe atom at site 0, is  $zP_i$ . Then the probability,  $P_A$  that, if an Fe atom is located at site 0, it is not connected to another Fe atom at any site in shells  $i = 1$  through 9 is given by

$$P_A = \prod_{i=1}^9 (1 - zP_i)^{S_i} \quad (25a)$$

From Eq. 25a, the concentration of isolated single-Fe clusters is



$$c_1 = z \prod_{i=1}^9 (1-zP_i)^{S_i} \quad (25)$$

In calculating the concentration of Fe-pair clusters, one has to be careful not to count pairs which are parts of triplets or of larger configurations. The probability that an Fe atom A is connected to another Fe atom B located at any one of the  $S_i$  sites in its  $i$ -shell, but is not connected to any other Fe atom in any of the remaining  $(S_i-1)$  sites on its  $i$ -shell, or in any site on its shells  $\underline{j} = 1$  through 9 ( $j \neq i$ ), is

$$z P_i S_i (1-zP_i)^{S_i-1} \prod_{\substack{j=1 \\ j \neq i}}^9 (1-zP_j)^{S_j}. \quad (26a)$$

In calculating  ${}_i P_{AB}$ , the probability of a given Fe atom A being part of a doublet, with another Fe atom B in its  $i$ -shell, one also has to ensure that the Fe atom B, in its turn, is connected only to one Fe atom, namely A, which is in the  $i^{\text{th}}$  shell of B. Then  ${}_i P_{AB}$  is

$${}_i P_{AB} = \left[ z P_i S_i (1-zP_i)^{S_i-1} \prod_{\substack{j=1 \\ j \neq i}}^9 (1-zP_j)^{S_j} \right] \cdot \left[ (1-zP_i)^{(S_i-1)-{}_i S_i} \prod_{\substack{k=1 \\ k \neq i}}^9 (1-zP_k)^{S_k-{}_i S_k} \right] \quad (26)$$

where  $S_k$  is the co-ordination number of the  $k^{\text{th}}$  shell of B and  ${}_i S_k$  is the number of sites on the  $k^{\text{th}}$  shell of B that are located also on any of the  $1^{\text{st}}$  through  $9^{\text{th}}$  shell of A. The Fe



atom B has a total of 146 connectable sites; the atom A is occupying one of these. Of the remaining 145 sites there are  $\sum_{k=1}^9 i S_k$  sites which are among the 145 sites connectable to A. In the first factor in Eq. 26 the condition that none of these common connectable sites have an Fe atom is incorporated. Hence, in the second factor in Eq. 26 these sites were excluded from consideration. Equation 26 can be rewritten as follows:

$$\begin{aligned}
 {}_i P_{AB} &= \left[ z \prod_{i=1}^9 (1 - z P_i)^{S_i} \right] \left[ \frac{P_i S_i}{(1 - z P_i)^2} \prod_{k=1}^9 (1 - z P_k)^{S_k - i S_k} \right] \\
 &= \left[ z \prod_{j=1}^9 (1 - z P_j)^{S_j} \right] \left[ \frac{P_i S_i}{(1 - z P_i)^2} \prod_{k=1}^9 (1 - z P_k)^{S_k - i S_k} \right] \quad (27)
 \end{aligned}$$

It may be noted that only the second factor in Eq. 27 depends on the value of  $i$ . Now, summing over all nine shells, the fraction of Fe atoms in doublets is:

$$\begin{aligned}
 P_{\text{Fe-Fe}} &= \sum_{i=1}^9 {}_i P_{AB} = \left[ z \prod_{j=1}^9 (1 - z P_j)^{S_j} \right] \cdot \\
 &\quad \sum_{i=1}^9 \left[ \frac{P_i S_i}{(1 - z P_i)^2} \prod_{k=1}^9 (1 - z P_k)^{S_k - i S_k} \right] \quad (28)
 \end{aligned}$$

The concentration of Fe-pair clusters is



$$c_2 = \frac{1}{2} z \left[ z \prod_{j=1}^9 (1-zP_j)^{S_j} \right] \sum_{i=1}^9 \left[ \frac{P_i S_i}{(1-zP_i)^2} \prod_{k=1}^9 (1-zP_k)^{S_k - i S_k} \right] \quad (29)$$

The ratio of the concentrations of Fe-pair clusters to single-Fe clusters, from Eq. 29 and Eq. 25, is then:

$$\frac{c_2}{c_1} = \frac{1}{2} z \sum_{i=1}^9 \left[ \frac{P_i S_i}{(1-zP_i)^2} \prod_{k=1}^9 (1-zP_k)^{S_k - i S_k} \right] \quad (30)$$

With the help of a computer program (Appendix B) the numbers  $i S_k$  were determined for  $k=1$  through 9 for each value of  $i=1$  through 9. These numbers are listed in Table 44. The ratio  $c_2/c_1$  was computed from Eq. 30 with the aid of another program (Appendix C) for different values of the Fe concentration,  $z$ , and of the Ni concentration,  $x$ . Figure 57(a) shows the calculated values of  $c_2/c_1$  as compared with the experimental values derived from the analysis of magnetization data (Tables 36 through 41). As described in the section on Data Analysis, the  $c_2$  and  $c_1$  values for quenched alloys were estimated assuming that the ratio  $c_2/c_1$  is a function of a single parameter  $\text{Fe-Fe}^{\alpha_1}$  expressing the clustering tendency of Fe atoms. The  $c_2$  and  $c_1$  values for deformed alloys were derived without making the above assumption; i.e.,  $c_1$  and  $c_2$  were set to be independent of each other. For both quenched and deformed alloys the experimental  $c_2/c_1$  ratios are much higher than the values calculated from Eq. 30, i.e., on the basis of the random alloy model of Bennett et al.<sup>4</sup> The  $c_2/c_1$  ratios for the quenched alloys are systematically



Table 44. The number  $iS_k$  of sites on the  $k^{\text{th}}$  shell of atom B, which are shared with the 1<sup>st</sup> through 9th shells of atom A.

| $i \backslash k$ | 1  | 2 | 3  | 4  | 5  | 6 | 7  | 8 | 9 | 9a | $\sum_k iS_k$ |
|------------------|----|---|----|----|----|---|----|---|---|----|---------------|
| 1                | 11 | 6 | 24 | 12 | 22 | 6 | 32 | 4 | 5 | 10 | 132           |
| 2                | 12 | 5 | 24 | 8  | 20 | 4 | 24 | 1 | 4 | 12 | 114           |
| 3                | 12 | 6 | 18 | 9  | 14 | 5 | 22 | 3 | 5 | 10 | 104           |
| 4                | 12 | 4 | 18 | 6  | 12 | 2 | 24 | 2 | 5 | 10 | 95            |
| 5                | 11 | 5 | 14 | 6  | 10 | 4 | 20 | 2 | 4 | 6  | 82            |
| 6                | 9  | 3 | 15 | 3  | 12 | 3 | 18 | 3 | 3 | 9  | 78            |
| 7                | 8  | 3 | 11 | 6  | 10 | 3 | 15 | 2 | 3 | 7  | 68            |
| 8                | 8  | 1 | 12 | 4  | 8  | 4 | 16 | 0 | 4 | 4  | 61            |
| 9                | 5  | 2 | 10 | 5  | 8  | 2 | 12 | 2 | 4 | 8  | 58            |
| 9a               | 5  | 3 | 10 | 5  | 6  | 3 | 14 | 1 | 4 | 5  | 56            |

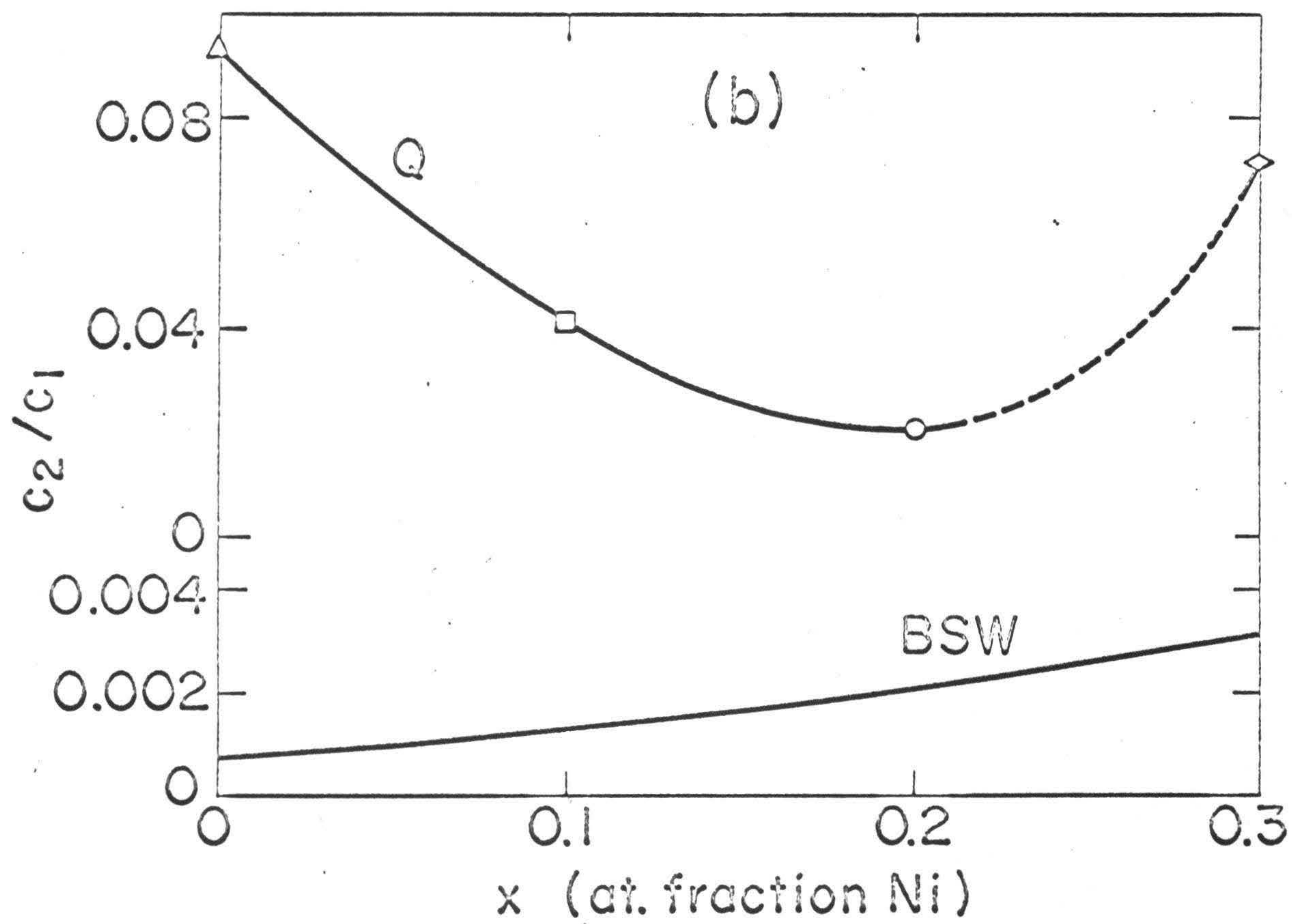
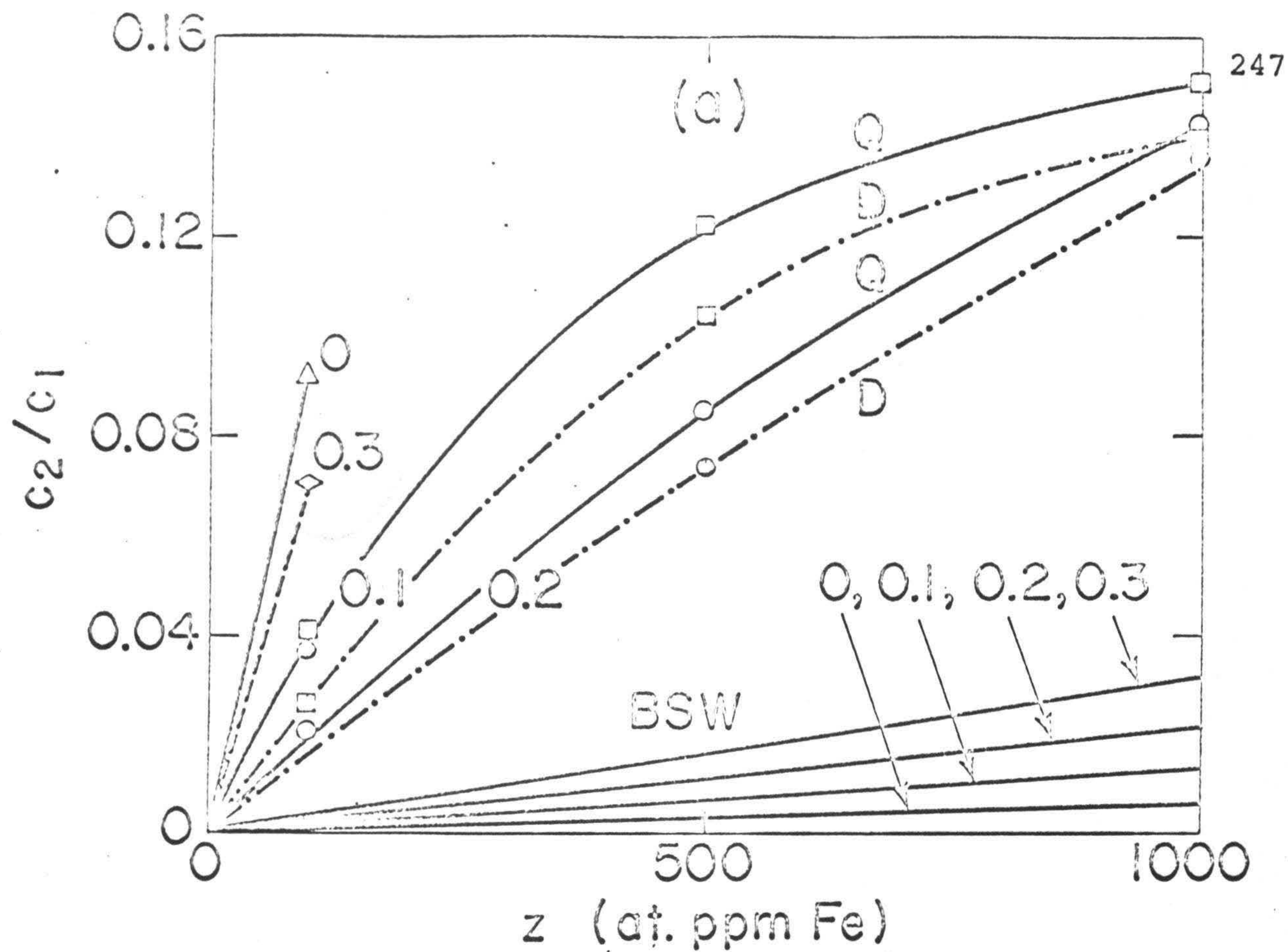


Figure 57. Experimental and calculated (on the basis of random alloy model) values of  $c_2/c_1$ .

- (a) The values of  $c_2/c_1$  estimated in the present work for quenched (Q) and deformed (D) alloys as a function of Fe and Ni content ( $x = 0.1, 0.2, 0.3$ ) as compared to values calculated using Eq. 30 (BSW).
- (b)  $c_2/c_1$  values estimated in the present work for quenched alloys with  $\sim 100$  ppm Fe cross plotted from Fig. 57(a), as compared to values calculated using Eq. 30 (BSW).

Note: The experimental value of  $c_2/c_1$  for 100 ppm Fe in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  may involve some error due to the clustering tendency in this alloy of the Ni atoms, giving rise to magnetic dipoles.<sup>1</sup>







higher than the corresponding ratios for deformed alloys, suggesting that quenched alloys have more clustering than deformed alloys, although the latter are certainly not random either.

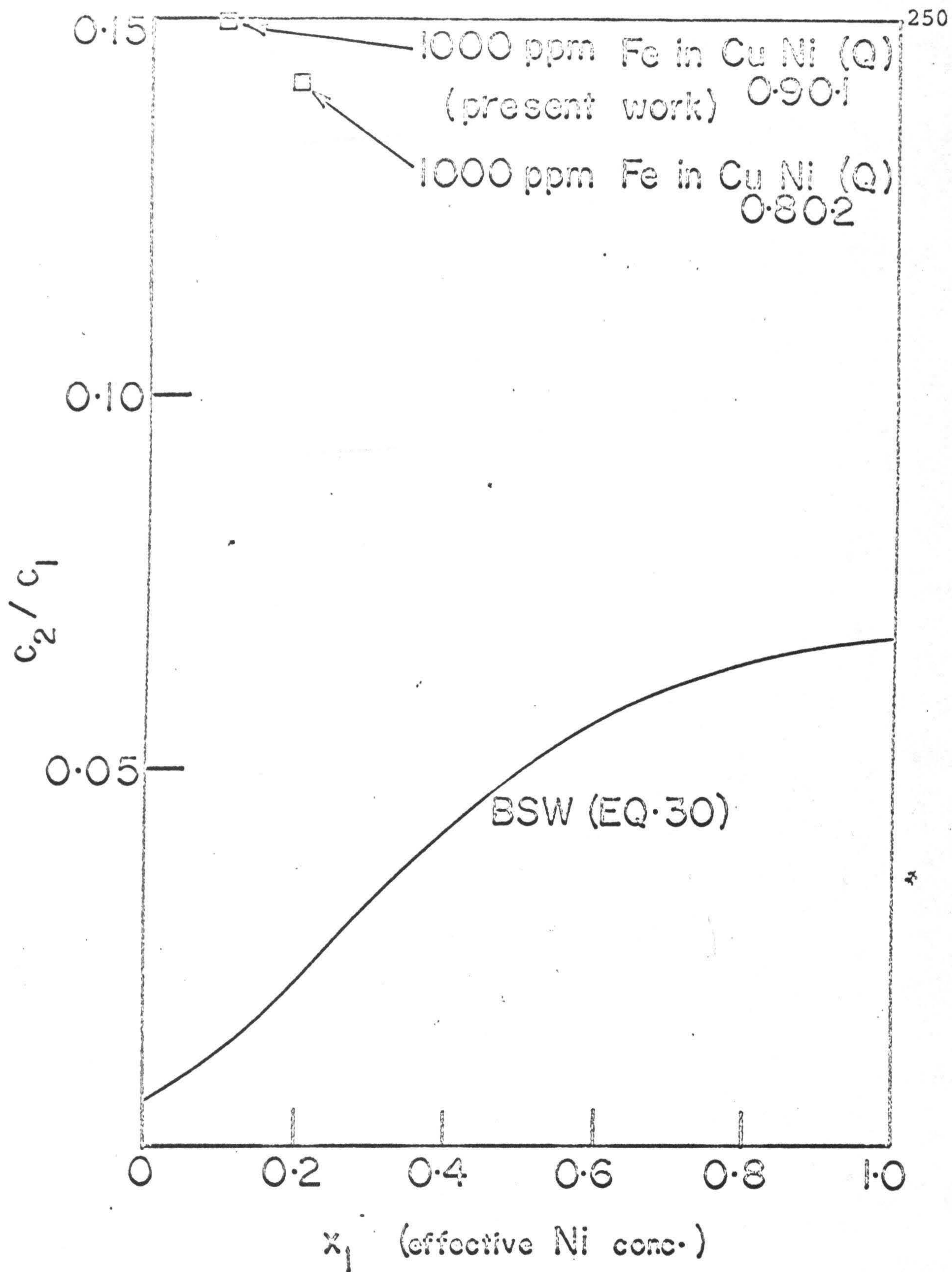
The connection probabilities and hence the Fe pair concentration and thus the ratio  $c_2/c_1$  can be increased by assuming that, while the Fe atoms are randomly distributed, there is a tendency for the Ni atoms to cluster around the Fe atoms, i.e.,  $x_1$ , the effective Ni concentration in the nearest neighbor shell of all Fe atoms is higher than  $x$ , the overall Ni concentration in the alloy. Figure 58 shows that the assumption of the highest possible value of  $x_1$ , namely 1, is not sufficient to bring about agreement of the calculated  $c_2/c_1$  values with those experimentally evaluated for the quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing 1000 ppm Fe. This is also true for all the other alloys containing 100 or 500 ppm Fe.

An interesting feature of the random alloy model of Bennett et al.<sup>4</sup> is that it predicts that, for a given Fe concentration, the  $c_2/c_1$  ratio should increase with the Ni concentration. In Fig. 57(b) one finds that for an Fe concentration of about 100 ppm the  $c_2/c_1$  ratio for quenched alloys, as estimated from experimental data, decreases with increasing Ni content up to 20 at. % Ni. The increase in the estimated value of  $c_2/c_1$  between 20 at. % Ni and 30 At. % Ni may not be real; the situation is complicated by the presence of Ni-rich magnetic clusters.<sup>1</sup> In any case, at least up to 20 at. % Ni the dependence of the  $c_2/c_1$  ratio on the Ni concentration as predicted by the random



Figure 58.  $c_2/c_1$  vs.  $x_1$ . The assumption of a value of  $x_1$  (the effective Ni concentration in the nearest neighbor shells of all Fe atoms) even as high as 1 is seen not to be sufficient to give high enough  $c_2/c_1$  ratios from calculations based on Eq. 30 to be comparable to the experimentally evaluated values for quenched  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  and  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  alloys containing 1000 ppm Fe.







alloy model of Bennett et al.<sup>4</sup> is the opposite of that obtained from the analysis of the experimental data.

One may conclude that in quenched Cu-Ni-Fe alloys there is a tendency for the Fe atoms to cluster. The  $c_2/c_1$  ratios are then well represented by the  $_{\text{Fe-Fe}}\alpha_1$  values listed in Tables 37, 38, and 39. It has already been pointed out that for Cu-Fe alloys there is Mössbauer spectroscopic evidence, based on the interpretation of isomer shift and line shape data,<sup>7,8</sup> that Fe atoms tend to form Fe-Fe pairs or larger atomic clusters with nearest neighbor Fe atoms. Window et al.<sup>5</sup> have concluded from isomer shift and quadrupole splitting in the Mössbauer spectra of dilute  $^{57}\text{Fe}$  in copper-rich Cu-Ni alloys, that here, too, the Fe atoms have a tendency to cluster. The results of the present investigation are consistent with the finding of Window et al.<sup>5</sup> The values of the short range order parameter  $_{\text{Fe-Fe}}\alpha_1$ , as evaluated in the present work as a function of Fe and Ni contents, are shown in Fig. 59(a).  $_{\text{Fe-Fe}}\alpha_1$  increases with the Fe concentration but decreases with the Ni concentration, at least up to 20 at. % Ni. We define a parameter D by the following equation:

$$D = \frac{z_1}{z} \quad (31)$$

D represents the degree of nonrandomness of the Fe atoms and expresses the increase in the Fe concentration in the nearest neighbor shells of all Fe atoms, over the overall Fe content of the alloy. For a truly random solution  $z_1 = z$  and  $D = 1$ . As seen in Fig. 59(b), for a given Ni concentration D decreases

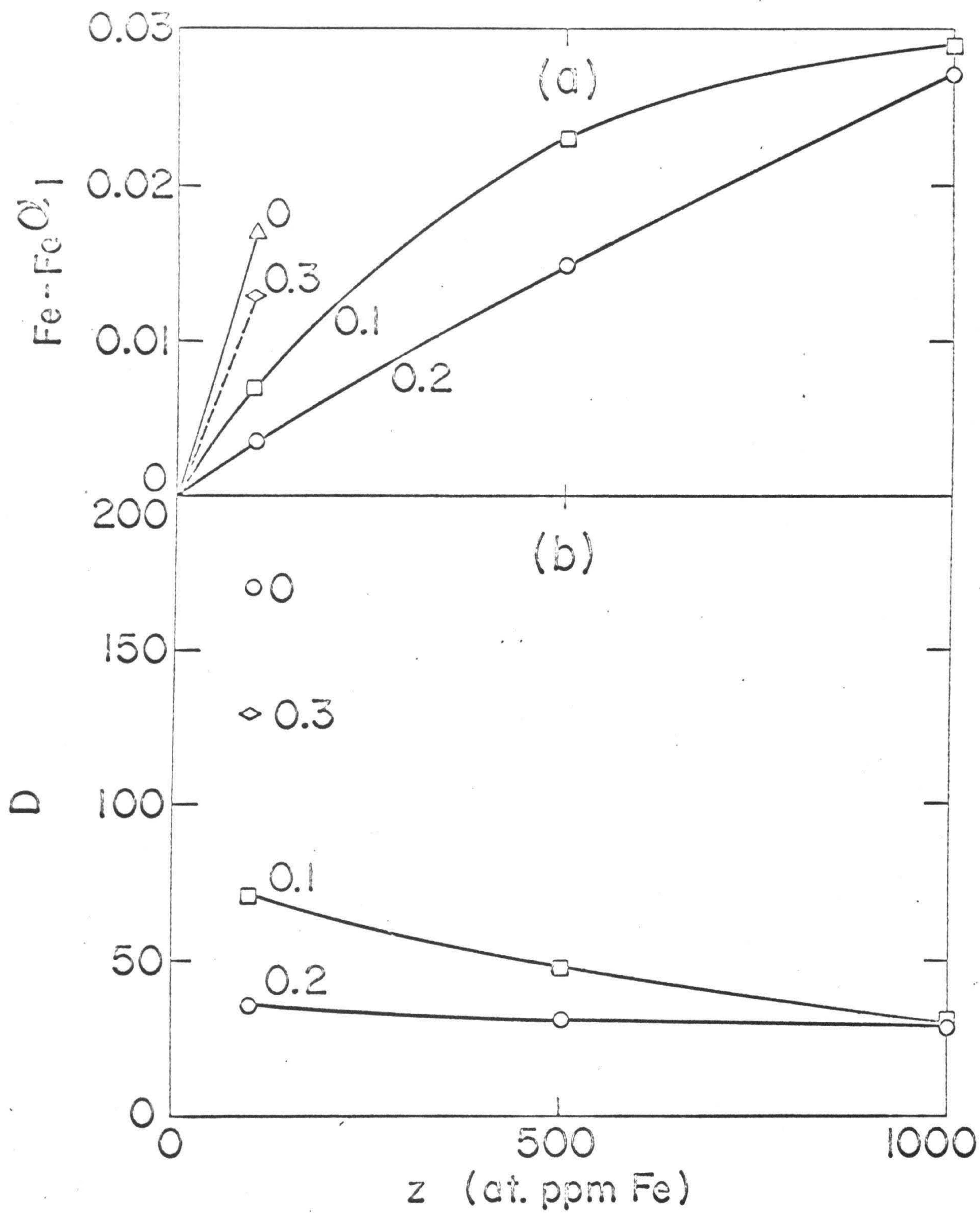


Figure 59.  $\text{Fe-Fe}^{\alpha_1}$  and D vs. z.

- (a)  $\text{Fe-Fe}^{\alpha_1}$  for quenched alloys as a function of Fe and Ni content ( $x = 0, 0.1, 0.2, 0.3$ ) from magnetic data.
- (b) D for quenched alloys as a function of Fe and Ni content, evaluated from magnetic data.

Note: The  $\text{Fe-Fe}^{\alpha_1}$  and D values for 100 ppm Fe in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  may involve some error due to the clustering tendency in this alloy of Ni atoms, giving rise to magnetic dipoles.<sup>1</sup>







with increasing Fe content, i.e., the alloys approach randomness. Thus the most dilute solid solutions of Fe in copper-rich Cu-Ni alloys are the most nonrandom as far as the distribution of the Fe atoms is concerned. This very interesting feature has also been observed in deformed Cu-Fe alloys by Campbell et al.<sup>8</sup>

It has already been shown that for quenched alloys the average value of  $\mu_1$ , the single-Fe cluster moment, increases (Fig. 55) from  $2.44 \mu_B$  in pure Cu to  $5.2 \mu_B$  in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ . Fe is known to have a moment of  $3.1 \mu_B$  in pure Ni.<sup>32</sup> Hence on a weighted average basis the moment on an Fe atom may be expected to change from  $2.44 \mu_B$  in Cu to  $\sim 2.61 \mu_B$  in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ . Clearly the  $\mu_1$  values can not be interpreted as the moment of Fe alone. A simple interpretation would be that those Ni atoms which are nearest neighbors to an Fe atom, have moments and that the moment on the Fe atom and the adjacent Ni moments are aligned with one another, forming a magnetic cluster.<sup>3,2</sup> Two interesting questions that follow are: (a) How much does each Ni contribute to the cluster moment? (b) How many nearest neighbor Ni atoms are there on the average around each Fe? Making a simple assumption that the moment  $\mu_0$  on a Ni atom nearest neighbor to an Fe atom is independent of the number of Ni atoms in its own (i.e., of the Ni atom in question) nearest and second nearest neighbor shells, the cluster moment  $\mu_1$  can be expressed in the following way:

$$\mu_1(x) = \mu_{\text{Fe}}(x_1) + 12 \mu_0 x_1 \quad (32)$$



where  $\mu_{\text{Fe}}(x_1)$  is the moment on the Fe atom, which depends upon the concentration  $x_1$  of Ni atoms in its nearest neighbor shell. On a weighted average basis,

$$\mu_{\text{Fe}}(x_1) = 2.44 + (3.1 - 2.44)x_1 \quad (33)$$

If one assumes further that  $x_1$  is a simple function of  $x$ , the overall Ni concentration in the alloy, i.e.,

$$x_1 = x(1+ax^n) \quad (34)$$

then Eq. 32 can be rewritten as:

$$\mu_1(x) = 2.44 + (0.66 + 12\mu_0)(1+ax^n) \quad (35)$$

The parameter values  $\mu_0$ ,  $a$ , and  $n$  were estimated by fitting Eq. 35 to the  $\mu_1$  values for quenched alloys (Fig. 55). The parameter values obtained are:  $\mu_0 = 0.225 \mu_B$ ,  $a = 11.52$ , and  $n = 1.57$ . The Fe-Ni nearest neighbor short range order parameter  $\text{Fe-Ni}^{\alpha_1}$  may then be estimated from the relation:

$$x_1 = x + (1-x) \text{Fe-Ni}^{\alpha_1} \quad (36)$$

The values of  $\text{Fe-Ni}^{\alpha_1}$  for different alloys are listed in Table 45 and shown in Fig. 60. The results indicate that  $\text{Fe-Ni}^{\alpha_1}$  increases with the Ni content. For the 10 and 20 at. % Ni alloys the  $\text{Fe-Ni}^{\alpha_1}$  values as a function of the Fe content show some scatter which is however seen to be random and not systematic. The positive average value of  $\text{Fe-Ni}^{\alpha_1}$  for a given Ni content suggests clustering of Ni around Fe, consistent with the



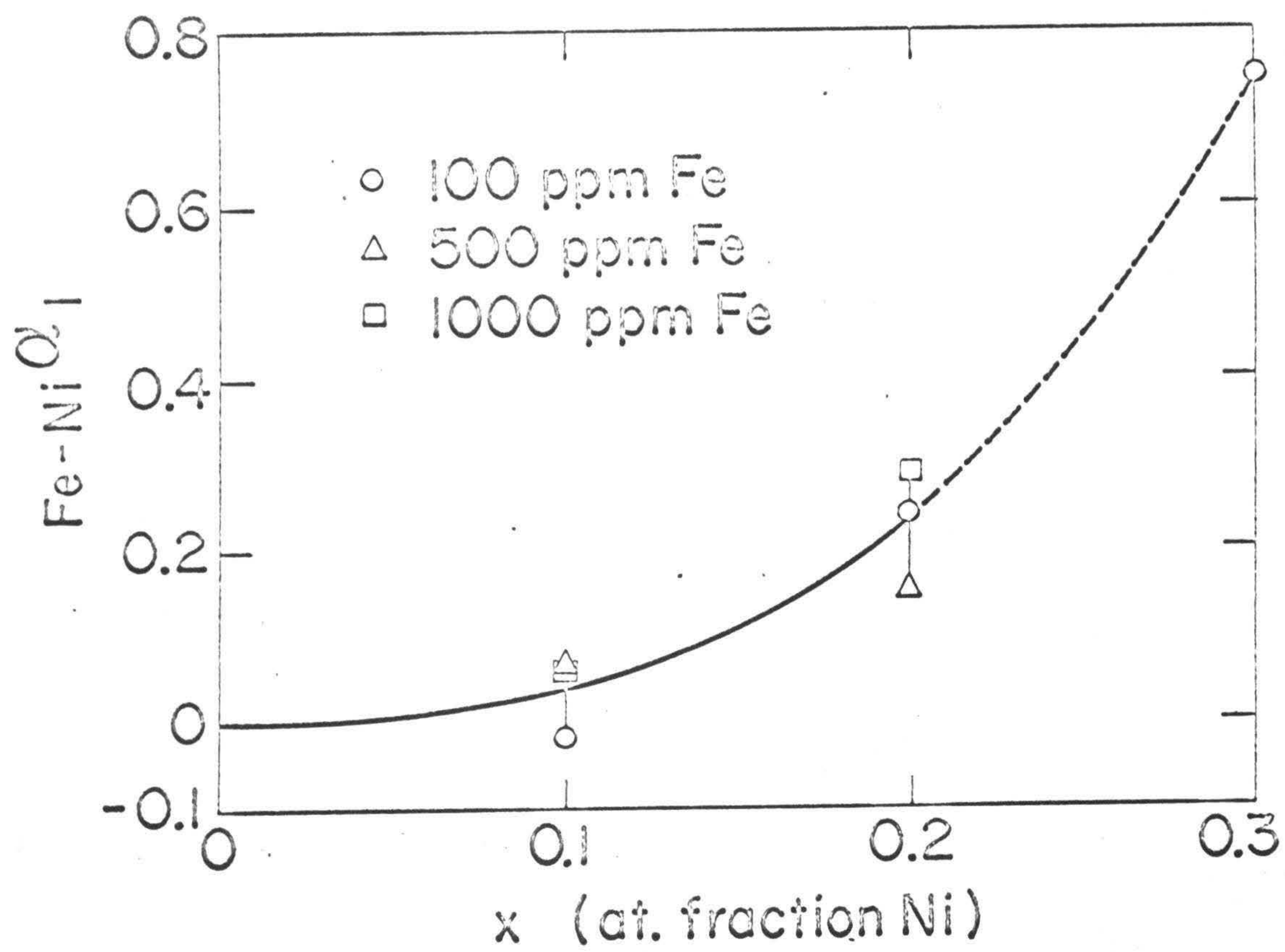
Table 45. Results for quenched alloys for the effective concentration,  $x_1$ , of Ni atoms in the nearest neighbor shells of isolated Fe atoms, and the Fe-Ni short range order parameter  $\text{Fe-Ni}^{\alpha_1}$ . See Figure 59.

| $x$<br>(at. fraction Ni) | $z$<br>(at. ppm Fe) | $x_1$<br>(at. fraction Ni) | $\text{Fe-Ni}^{\alpha_1}$ |
|--------------------------|---------------------|----------------------------|---------------------------|
| 0.1                      | 100                 | 0.077                      | -0.025                    |
| 0.1                      | 500                 | 0.161                      | 0.067                     |
| 0.1                      | 1000                | 0.155                      | 0.061                     |
| 0.2                      | 100                 | 0.393                      | 0.241                     |
| 0.2                      | 500                 | 0.321                      | 0.152                     |
| 0.2                      | 1000                | 0.431                      | 0.289                     |
| 0.3                      | 100                 | 0.821                      | 0.745                     |



Figure 60.  $\text{Fe-Ni}\alpha_1$  as a function of Fe and Ni content (see Table 45) for quenched alloys. The value of  $\text{Fe-Ni}\alpha_1$  for 100 ppm Fe in  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  may involve some error due to the clustering tendency in this alloy of the Ni atoms, giving rise to magnetic dipoles.<sup>1</sup>







conclusions of Window et al.<sup>5</sup> Clearly the random alloy model of Bennett et al.<sup>4</sup> is inappropriate for quenched Cu-Ni-Fe alloys.

The effect of deformation is to decrease the magnetization (e.g., Fig. 53). In Table 42 it is seen that the magnitude of the percent decrease in the magnetization, at 4.2°K in an applied field of  $\sim 12.6$  kOe, does not vary systematically with the composition. One of the principal reasons is that in the present work no attempt was made to deform the various specimens to exactly the same degree. In any case, as seen in Fig. 57 deformation of quenched alloys tends to partially randomize the Fe-Fe clustering, as evidenced by the systematic decrease in the  $c_2/c_1$  ratios. Another semiquantitative observation that may be made with respect to the effect of deformation is that the  $\mu_1$  values systematically decrease (Tables 37 through 41), suggesting a partial randomization of the Fe-Ni clustering as well. Both results are consistent with the conclusions of Window et al.<sup>5</sup> Window et al.<sup>5</sup> also concluded that even in heavily rolled samples there remained some degree of Fe-Ni clustering. Thus, it is difficult to obtain a truly random Cu-Ni-Fe alloy. The results of Bennett et al.<sup>4</sup> indicated that the single Fe cluster moment  $\mu_1$  for a  $\text{Cu}_{0.79}\text{Ni}_{0.21}$  alloy is the same ( $\sim 4.2 \mu_B$ ) in both quenched and deformed (cold rolled to  $\sim 10\%$  of the original thickness, i.e.,  $\sim 90\%$  reduction of area) conditions. This is inconsistent with the results of the present work and with those of Window et al.<sup>5</sup> Bennett et al.<sup>4</sup> found that for 0.5% Fe in  $\text{Cu}_{0.79}\text{Ni}_{0.21}$  the  $c_2/c_1$  ratio decreased



by ~50% on deformation. This need not be inconsistent with the smaller change in the  $c_2/c_1$  ratios (Fig. 57) obtained in the present work, since (a) the Fe concentration used by Bennett et al.<sup>4</sup> was five times higher than the maximum in the present investigation and it is expected that there were present in the quenched alloy larger clusters, containing more than three or four Fe atoms, which would have been easier to break up, and (b) the amount of deformation given to the specimens was much higher. It should be noted that the large change in the  $c_2/c_1$  ratio observed by Bennett et al.<sup>4</sup> would be very difficult to explain on the basis of their own random alloy model.<sup>4</sup>

Window et al.<sup>5</sup> concluded, from the hyperfine splitting in the Mössbauer spectra that  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$  and  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  alloys are magnetically ordered at 1.4°K; the ordering temperature lies between 3 and 4.2°K in the as rolled state, and increases to above 4.2°K for annealed specimens. Bennett et al.<sup>11</sup> claimed that the above two alloys are ferromagnetically ordered with ordering temperatures of 6.2°K and 5.8°K respectively. Results of the present investigation indicate a remanence temperature  $T_r$  of ~2.1°K (Fig. 24) for quenched  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$ , much lower than the Mössbauer ordering temperature.<sup>11</sup> Another result of the present work that is important in evaluating the above conclusions is that below 4.2°K the magnetization vs. temperature graph (Fig. 30) shows thermomagnetic history effects. Thus the quenched  $(\text{Cu}_{0.9}\text{Ni}_{0.1})_{0.99}\text{Fe}_{0.01}$  alloy is evidently mictomagnetic. The quenched  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  alloy shows no remanence



(Fig. 25) even at 1.57°K, a temperature quite low compared to the reported Mössbauer ordering temperature.<sup>11</sup> This suggests that the  $(\text{Cu}_{0.8}\text{Ni}_{0.2})_{0.99}\text{Fe}_{0.01}$  alloy is also micromagnetic. Though no thermomagnetic history effect was observed for this alloy in a 1000 Oe field (Fig. 31) it may be expected that such effects would be observable at a lower applied field,<sup>13</sup> and, particularly, at temperatures lower than 1.57°K.

### C. Cu-Ni

For the quenched  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy the value of the average permanent moment  $\bar{\mu} = 0.00036 \mu_B$  agrees well with the results of Cornut et al.<sup>33</sup>

For  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ , the magnetization values and susceptibilities below 160°K are higher in the aged than in the as-quenched condition (Figs. 17 through 20). Analogous increases in the magnetization as a result of aging have previously been reported.<sup>16,34</sup> Comparing the parameter values for the  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy (Table 35) in the as-quenched and the aged condition, one notes that the most important change on aging is the increase in the average moment of the large magnetic clusters from  $\sim 23$  to  $29 \mu_B$ . The average moment of the small magnetic clusters does not change perceptibly on aging. Robbins et al.<sup>16</sup> pointed out that in Cu-Ni alloys Ni-rich atomic clusters give rise to magnetic clusters which are responsible for the observed superparamagnetism,<sup>35,36</sup> the low temperature specific heat anomaly,<sup>37,16</sup> and the changes in the magnetization upon low



temperature aging and plastic deformation.<sup>16</sup> Low temperature aging allows the atomic (and, hence, of the magnetic) clusters to grow in size. The present results for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  are totally consistent with such an interpretation. The considerable increase of the average moment of the large clusters on aging implies a substantial increase in the short range order parameter  $\text{Ni-Ni}\alpha_1$ . There is no reason to assume that in 3 days the short range order parameter has already attained its equilibrium value on aging at  $300^\circ \text{C}$ . It is even possible that in true equilibrium at  $300^\circ \text{C}$  the alloy  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  would consist of two phases.

Although the physical significance of the bimodal distribution of cluster moments in the  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy is as yet not clearly understood, it seems quite possible that it is related to a higher degree of atomic clustering at grain boundaries than within the grains, because the grain boundary diffusion rate is higher. This explanation is consistent with the observation that aging at  $300^\circ \text{C}$  increases the larger moments much more than the smaller ones. The proposed explanation could be tested by magnetic measurements with a single crystal specimen of the same alloy.

For the quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy the average moment value of  $\sim 5.3 \mu_B$  for the small clusters is smaller and that of  $\sim 23 \mu_B$  for the large clusters is larger than the average moment of about  $10 \mu_B$  reported by Hicks et al.<sup>38</sup> from neutron scattering study of weakly ferromagnetic Cu-Ni alloys (46 to 50 at. % Ni) and by Kouvel and Comly<sup>22</sup> on the basis of magnetization



measurements for paramagnetic Cu-Ni alloys containing 32 to 44 at. % Ni. (For quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  a single moment Brillouin analysis of the magnetization data yields an average moment of  $\sim 17 \mu_B$ , substantially higher than  $\sim 10 \mu_B$ .) The method of analysis used by Kouvel and Comly<sup>22</sup> precluded the possibility of noticing a bimodal moment distribution. The present results for a  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy show that the average moment per cluster in the quenched state is about  $\sim 2.8 \mu_B$ . These results suggest that the interpretation of their bulk magnetization data by Kouvel and Comly<sup>22</sup> in terms of an average cluster moment, that remains constant at about  $\sim 10 \mu_B$  from 32 to 44 at. % Ni may be incorrect. Cornut et al.<sup>33</sup> also concluded that the giant moments in Cu-Ni alloys are concentration dependent. Earlier magnetization results of Van Elst et al.<sup>35</sup> indicated a large moment of  $\sim 60 \mu_B$  for a  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy. However this alloy, as evidenced by the appearance of remanence in the liquid helium temperature range, may have contained a considerable level of Fe impurity (spectroscopic analysis of a specimen of their  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy, kindly made available to us by Prof. Van Den Berg, indicated an Fe level of  $\sim 121$  ppm). The more recent magnetization results of Acker and Huguenin<sup>34</sup> for  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  have been interpreted in terms of magnetic clusters with average sizes of  $\sim 8 \mu_B$  and  $\sim 40 \mu_B$ . Qualitatively the present results may be considered to be in agreement with theirs, particularly since the magnetization data used by Acker and Huguenin<sup>34</sup> were limited to a relatively narrow temperature range.



In Fig. 61 the values of  $\chi_0$ , the temperature- and field-independent susceptibility, are shown as a function of the Ni concentration. There is good agreement with the results of Pugh et al.<sup>36</sup>  $\chi_0$  may be interpreted as the band susceptibility of the matrix. From Fig. 60 it is seen that  $\chi_0$  increases monotonically with increasing Ni content. Conversely the magnitude of  $\chi_0$  is a very good index of the Ni content of the matrix. However, when the Ni concentration is greater than ~20 at. %, Ni-rich clusters are formed, so that the Ni content of the matrix is lower than the average Ni content of the alloy as a whole. Thus the value of  $\chi_0 = 1.61 \times 10^{-6}$  emu/g (Table 35[b]) for quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  represents a matrix with less than 40 at. % Ni, and the decrease in the value of  $\chi_0$  to  $1.15 \times 10^{-6}$  emu/g on aging (Table 35[b]) suggests a further reduction in the Ni content of the matrix due to the increase in the size and the concentration of the Ni-rich clusters. In a simplified picture, the decrease in  $\chi_0$  on aging directly corresponds to the increase in the average moment per atom from  $\bar{\mu} = 0.0097 \mu_B$  in the quenched condition to  $0.0115 \mu_B$  in the aged condition. If one assumes that the average moment  $\bar{\mu}_{\text{Ni}}$  per Ni atom in a cluster is the same for both the quenched and the aged specimen of  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ , then

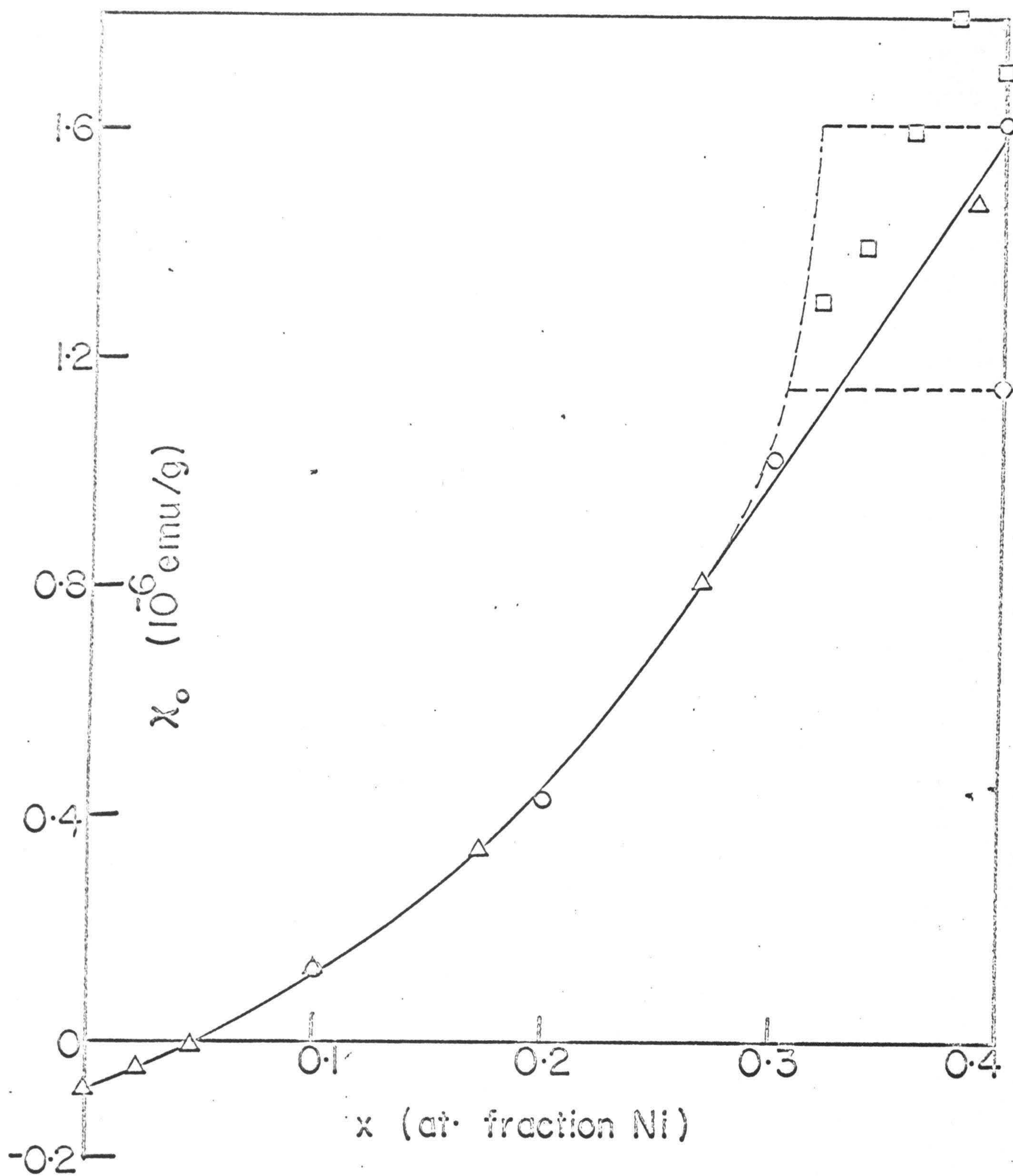
$$\bar{\mu}_{\text{Ni}} = \frac{0.0097}{0.4 - x_q} = \frac{0.0115}{0.4 - x_a} \quad (37)$$

where  $x_q$  represents the Ni concentration in the matrix of quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ , and  $x_a$  represents that of the aged alloy.



Figure 61.  $\chi_0$  vs. at. fraction Ni. Open circles: present data for quenched alloys; filled circle: present result for an aged  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  alloy; triangles: Pugh et al.; <sup>36</sup> squares: Kouvel and Comly.<sup>22</sup> The dashed line represents suggested variation of  $\chi_0$  as a function of the Ni content of the matrix.







There are many possible solutions of Eq. 37. However, to obtain a physically meaningful solution, one may assume (a)  $\bar{\mu}_{\text{Ni}}$  is less than  $0.6 \mu_B$ , the moment on a Ni atom in pure Ni, (b)  $x_a$  is greater than 0.3 since  $\chi_0$  for the  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy, where only a small fraction of the Ni atoms may be in clusters, is lower than that for aged  $\text{Cu}_{0.6}\text{Ni}_{0.4}$ , and (c) the  $x_q$  and  $x_a$  values must be such that when plotted against the experimental  $\chi_0$  values, the points should lie on a reasonable extrapolation of the  $\chi_0$  vs.  $x$  curve (Fig. 61) for lower Ni concentrations. These conditions are satisfied for a choice of  $x_q = 0.32$  and  $x_a = 0.305$ . The dashed curve in Fig. 61 then represents  $\chi_0$  versus Ni concentration in the matrix.

One may assume that the temperature- and field-independent susceptibility is

$$\chi_0 = \chi_p + \chi_v + \chi_L + \chi_c \quad (38)$$

where  $\chi_p$  and  $\chi_v$  are the Pauli (spin) and Van Vleck (orbital) components of the paramagnetic susceptibility and  $\chi_L$  and  $\chi_c$  represent the Landau (spin) and ion-core diamagnetic susceptibilities. The value of  $\chi_p$  (in emu/g) can be calculated from the electronic specific heat coefficient  $\gamma$  (in  $10^{-4}$  cal/mole-°K<sup>2</sup>),

$$\chi_p = \frac{3\mu_B^2 \gamma \beta}{\pi^2 k^2 M(1+\lambda)} \quad (39)$$

where  $\beta = 4.184 \times 10^3$  ergs/cal, and  $(1+\lambda)$  is the electron-phonon enhancement factor for the electronic specific heat. Assuming the electron-phonon enhancement factor to be equal to 1,  $\chi_p$  was



computed for copper-rich Cu-Ni alloys from the corresponding  $\gamma$  values reported in the literature<sup>39</sup> and is presented in Fig. 62(a). For pure Cu the measured value of  $\chi_o$  is  $-0.088 \times 10^{-6}$  emu/g<sup>36</sup> and the value of  $\chi_p$  (calculated from  $\gamma$ ) is  $0.151 \times 10^{-6}$  emu/g. Assuming  $\chi_v \approx 0$  and  $\lambda = 0$ , the total diamagnetic susceptibility, i.e.,  $(\chi_L + \chi_C)$  for pure Cu is  $-0.239 \times 10^{-6}$  emu/g. If one further assumes that the diamagnetic component does not change with the addition of Ni to Cu,<sup>36</sup>  $\chi_p$  for Cu-Ni alloys can also be estimated from the experimentally determined  $\chi_o$  values, using Eq. 38. The  $\chi_p$  values so obtained from the susceptibility data are seen in Fig. 62(a) to be systematically higher than the corresponding values obtained from specific heat results. The Stoner enhancement (S) of the susceptibility<sup>40</sup> for Cu-Ni alloys was estimated from the relation:

$$S = \frac{\chi_p \text{ (from susceptibility data)}}{\chi_p \text{ (from specific heat data)}} \quad (40)$$

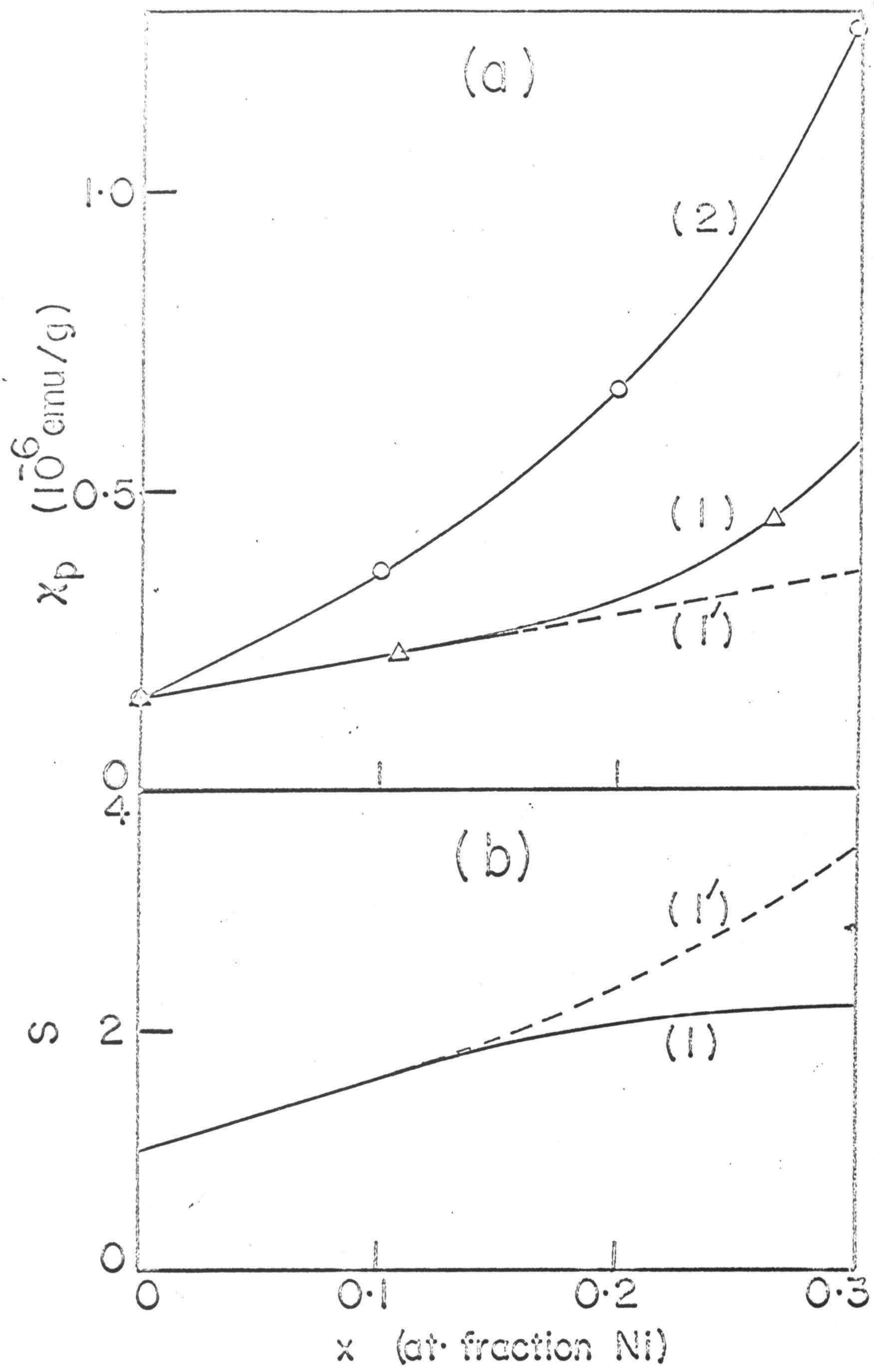
The Stoner enhancement factor is presented in Fig. 62(b) as a function of the Ni concentration and is seen to increase with the Ni content. One may postulate that for Ni concentrations higher than 15 at. % the  $\gamma$  values (and the  $\chi_p$  values derived from them) might have been increased due to a magnetic contribution<sup>41</sup> due to the interaction of the magnetic moment on some Ni atoms<sup>1,2</sup> with a very weak ambient field as described by Marshall for dilute alloys.<sup>42</sup> One may assume that, under such conditions a linear extrapolation of the  $\chi_p$  values (from specific heat data) from below 15 at. % Ni to higher concentrations



Figure 62.  $\chi_p$  and S vs. at. fraction Ni.

- (a) The Pauli susceptibility  $\chi_p$ , as calculated from the electronic specific heat coefficient  $\gamma$  <sup>39</sup> (1), and as estimated from the susceptibility data (2). The dashed line (1') is a linear extrapolation to higher Ni concentrations of the  $\chi_p$  values at and below  $\sim 0.1$  at. fraction Ni.
- (b) The stoner enhancement factor S; as calculated from curves (1) and (2) in Fig. 62(a).







(line (1') in Fig. 62[a]) may represent more accurately the variation of  $\chi_p$  with the Ni content than the  $\chi_p$  calculated directly from the measured  $\gamma$  values (Line [1] in Fig. 62[a]). The corresponding higher rate of increase of the Stoner enhancement factor than the rate of addition of Ni to Cu is shown in Fig. 62(b) by line (1').

For Cu-Ni alloys the average permanent moment  $\bar{\mu}$  per alloy atom can be estimated from the model of Robbins et al.<sup>16</sup> in which the moment  $\mu_{n,m}$  on a Ni atom is a function of the number  $n$  of the nearest, and number  $m$  of the second-nearest Ni neighbors:

$$\bar{\mu}(x) = x \sum_{n,m} P_{n,m} \mu_{n,m} \quad (41)$$

where  $P_{n,m}$  is the probability a for a given Ni atom to have  $n$  Ni nearest neighbors and  $m$  second-nearest neighbors. If  $y_1 = x + \text{Ni-Ni}^{\alpha_1}(1-x)$  and  $y_2 = x + \text{Ni-Ni}^{\alpha_2}(1-x)$  represent the effective concentration of Ni in the nearest and second-nearest neighbor shells of all Ni atoms in the alloy, then from the usual binomial distribution theorem,

$$P_{n,m} = \frac{12!6!}{(12-n)!(6-m)!n!m!} y_1^n (1-y_1)^{12-n} y_2^m (1-y_2)^{6-m} \quad (42)$$

12 and 6 being the co-ordination numbers of the nearest and second-nearest neighbor shell of a given site in an fcc lattice. Assuming  $\text{Ni-Ni}^{\alpha_1} = 0.121$  and  $\text{Ni-Ni}^{\alpha_2} = 0$ , the short range order parameters obtained for a furnace cooled  $\text{Cu}_{0.525}\text{Ni}_{0.475}$  alloy by Mozer, Keating and Moss,<sup>23</sup> the average



permanent moment per alloy atom for quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  may be calculated to be  $\bar{\mu}' = 0.0129 \mu_B$ ; this calculation overestimates the experimental value by about 33%. The model of Robbins et al. is also inaccurate in the weakly ferromagnetic composition range, i.e., around 50 at. % (Fig. 1, Reference 16); for Ni concentrations lower than 50 at. % Ni the model predicts larger  $\bar{\mu}$  values than experimentally observed, thus indicating that perhaps smaller (than 0.121)  $\text{Ni-Ni}^{\alpha_1}$  values should be assumed for these alloys.

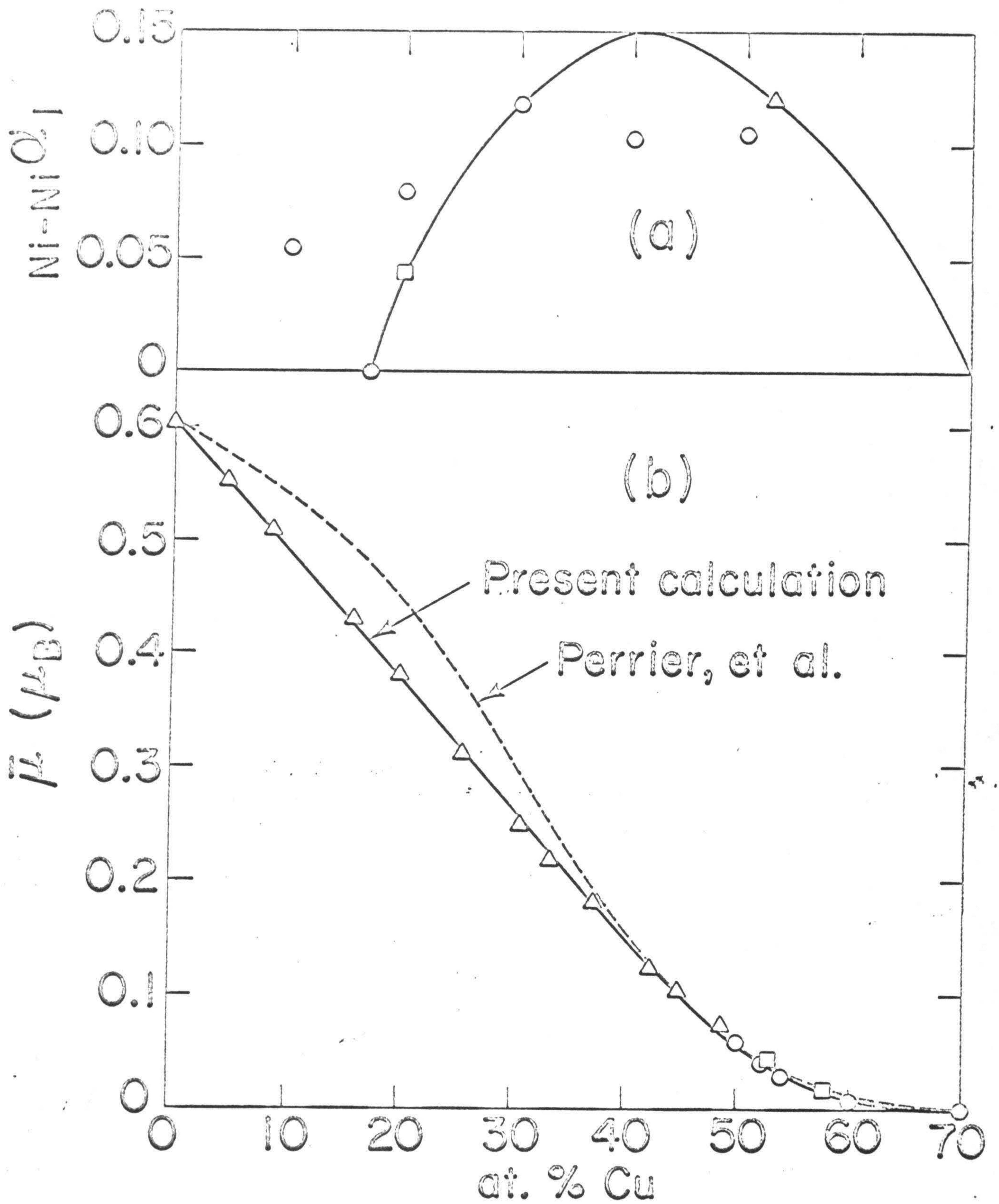
On the basis of the model of Perrier et al.<sup>43</sup> for Cu-Ni alloys of nearly equiatomic composition, which makes the assumption that the quenched alloys are atomically random and that Ni atoms with 8 or more nearest neighbors have a moment of  $0.6 \mu_B$  (moment of Ni in pure nickel), while the Ni atoms with fewer Ni nearest neighbors have zero moment, the average moment per alloy atom calculated for quenched  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  is  $\bar{\mu}'' = 0.0145 \mu_B$ ; this calculation overestimates the average moment by nearly 50%. In fact as may be seen in Fig. 63(b) the model of Perrier et al.<sup>43</sup> predicts, for all alloys containing more than 55 at. % Ni, much larger  $\bar{\mu}$  values than those measured. This indicates that much too large moment values (i.e.,  $0.6 \mu_B$ ) were assigned to the Ni atoms with 8, 9, 10 and 11 Ni nearest-neighbors. The assumption of Perrier et al.<sup>43</sup> that quenched Cu-Ni alloys are atomically random is also questionable in view of the recent neutron diffuse scattering work of Aldred et al.<sup>44</sup> who obtained, for a  $\text{Cu}_{0.5}\text{Ni}_{0.5}$  alloy quenched from 1000° C, a value of 0.106



Figure 63.  $\text{Ni-Ni}^{\alpha_1}$  and  $\bar{\mu}$  vs. at. % Cu.

- (a)  $\text{Ni-Ni}^{\alpha_1}$  as a function of the Ni content:  
 $\Delta$ , Mozer et al.;<sup>23</sup>  $\square$ , Cable et al.;<sup>45</sup>  
 $\circ$ , Aldred et al.;<sup>44</sup>  $\bullet$ , Dekhtyar et al.<sup>46</sup>  
 The solid curve drawn shows the assumed variation of the short range order parameter.
- (b)  $\bar{\mu}$  as a function of Ni content:  $\circ$  and  $\bullet$ , present work;  $\Delta$ , Ahern et al.;<sup>47</sup>  $\square$ , Perrier et al.<sup>43</sup> The dashed curve represents calculated values based on the model of Perrier et al.<sup>43</sup> The full curve represents calculated values from a modified moment assignment scheme (Fig. 64) and assuming  $\text{Ni-Ni}^{\alpha_1}$  varies as shown in Fig. 63(a).







for  $\text{Ni-Ni}^{\alpha_1}$ , in fair agreement with the very accurate results of Mozer et al.<sup>23</sup> for a near equi-atomic furnace cooled alloy. The values of the atomic short range order parameter for a number of Cu-Ni alloys, quenched from  $\sim 1000^\circ \text{C}$ , as obtained by Aldred et al.<sup>44</sup> and by Cable et al.,<sup>45</sup> are shown in Fig. 63(a). Dekhtyar and Chudakov<sup>46</sup> did not find any effect of plastic deformation on the magnetization of a  $\text{Cu}_{0.83}\text{Ni}_{0.17}$  alloy; one may assume that this is an indication of the absence of Ni-rich atomic clusters, i.e.,  $\text{Ni-Ni}^{\alpha_1} = 0$ .

A revised moment assignment scheme was constructed for Cu-Ni alloys along the lines of the model of Robbins et al.<sup>16</sup> The short range order parameter was assumed to vary with the Ni concentration in the manner shown in Fig. 63(a), taking into full consideration the results of Dekhtyar and Chudakov<sup>46</sup> and the accurate values of  $\text{Ni-Ni}^{\alpha_1}$  determined by Mozer et al.<sup>23</sup> and Cable et al.<sup>45</sup> With the  $\mu_{n,m}$  values listed in Table 46 and presented in Fig. 64, good agreement was obtained in the entire ferromagnetic composition range between experimental and calculated values of  $\bar{\mu}$ , the average moment per alloy atom. As seen in Fig. 63(b) the fit is equally good also for superparamagnetic ( $\text{Cu}_{0.6}\text{Ni}_{0.4}$  and  $\text{Cu}_{0.7}\text{Ni}_{0.3}$ ) alloys.

In a recent paper Garland and Gonis<sup>48</sup> pointed out that one may obtain a good fit to the experimental average moment ( $\bar{\mu}$ ) by using either second nearest neighbor effects<sup>16</sup> or by using cooperative effects in which case the moment on a Ni atom would depend not only on the number of nearest neighbor Ni atoms, but



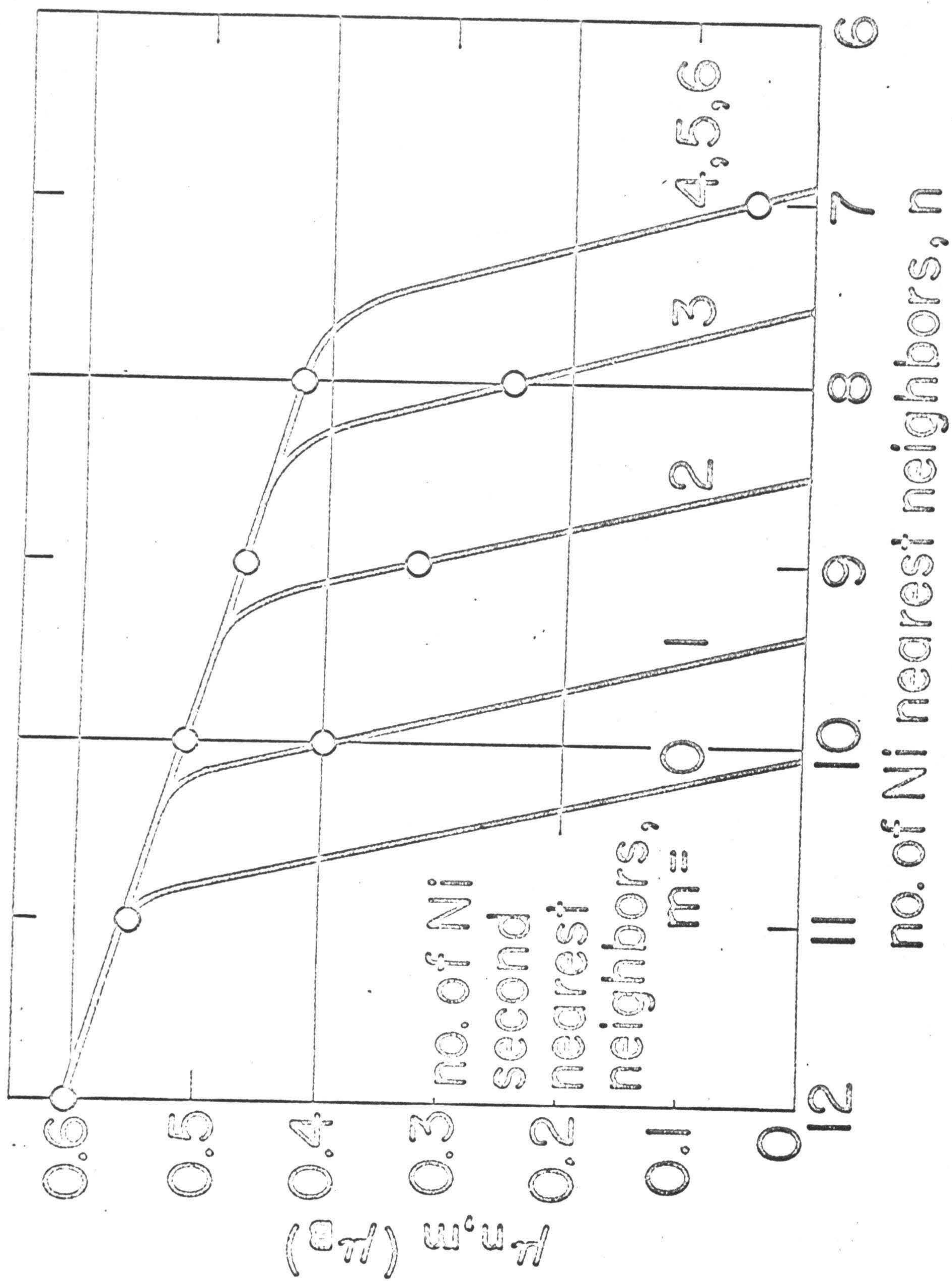
Table 46. Moment assignments,  $\mu_{n,m}$  in  $\mu_B$ , in Cu-Ni alloys for Ni atoms with  $n$  nearest and  $m$  second nearest neighbor Ni atoms.

| $m \backslash n$ | 6-0 | 7    | 8     | 9     | 10    | 11    | 12    |
|------------------|-----|------|-------|-------|-------|-------|-------|
| 0                | 0   | 0    | 0     | 0     | 0     | 0.556 | 0.606 |
| 1                | 0   | 0    | 0     | 0     | 0.400 | 0.556 | 0.606 |
| 2                | 0   | 0    | 0     | 0.325 | 0.512 | 0.556 | 0.606 |
| 3                | 0   | 0    | 0.250 | 0.468 | 0.512 | 0.556 | 0.606 |
| 4                | 0   | 0.05 | 0.424 | 0.468 | 0.512 | 0.556 | 0.606 |
| 5                | 0   | 0.05 | 0.424 | 0.468 | 0.512 | 0.556 | 0.606 |
| 6                | 0   | 0.05 | 0.424 | 0.468 | 0.512 | 0.556 | 0.606 |



Figure 64. A modified moment assignment scheme for Cu-Ni alloys.  $\mu_{n,m}$  is the moment on a Ni atom with n nearest and m second nearest neighbor Ni atoms. This is slightly different from the moment assignment scheme of Robbins et al.<sup>16</sup>







also on the moment carried by each of these nearest neighbor Ni atoms.<sup>22</sup> Garland and Gonis<sup>48</sup> contend that no purely chemical model can yield a magnetic moment per cluster that is independent of the Ni composition.<sup>22</sup> However, as has been shown in the present work the magnetic moment per cluster does in fact depend on the Ni composition. Garland and Gonis<sup>48</sup> have claimed that the model of Robbins et al. predicts: (a) magnetic clusters of smaller spatial extent than that observed by Hicks et al.,<sup>38</sup> (b) a concentration of magnetic clusters in the superparamagnetic regime much greater than that found by Kouvel et al.,<sup>22</sup> and (c) a much too rapid decrease of the magnetic cluster size with increasing copper concentration, e.g., for  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  a magnetic moment per cluster that is substantially smaller than  $3 \mu_B$ .<sup>1</sup> So far no numerically workable model for Cu-Ni alloys has been put forth, which takes into account the co-operative effects. The model of Robbins et al.<sup>16</sup> at least has the virtue that it fits very well all the available information on the average moment per alloy atom over a wide composition range. It should also be pointed out that in their model,<sup>16</sup> since the moment  $\mu_{n,m}$  on a Ni atom depends upon the number  $m$  of second nearest neighbor Ni atoms, which in turn influence the moment on the  $n$  nearest neighbor Ni atoms, co-operative effects of the type suggested by Kouvel and Comly<sup>22</sup> and Garland and Gonis<sup>48</sup> are at least partially accounted for.



## VI. SUMMARY

The magnetization of quenched  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys containing 100 to 1000 ppm Fe can be quantitatively accounted for in terms of magnetic clusters associated with 1, 2, and 3 or more Fe atoms. The ratio of the concentration of the Fe pair clusters to that of single Fe clusters is at all Ni and Fe concentrations much higher than the corresponding ratio calculated on the basis of a random alloy model which assumes long range interaction between Fe moments. Hence Fe-Fe clusters have to be postulated. The nearest-neighbor short range order parameter, corresponding to experimental concentration ratios, increases with the Fe concentration but decreases with the Ni concentration. The dipole moment connected with the single Fe clusters is larger than that expected for Fe alone, and increases with the Ni content. These findings can be accounted for if a contribution to the cluster moment from nearest neighbor Ni atoms is assumed.

The temperature dependence of the magnetic susceptibility of the iron-free binary  $\text{Cu}_{0.9}\text{Ni}_{0.1}$  and  $\text{Cu}_{0.8}\text{Ni}_{0.2}$  alloys is very small, indicating the absence of a measurable concentration of magnetic moments. The magnetization of the  $\text{Cu}_{0.7}\text{Ni}_{0.3}$  alloy can be interpreted in terms of a low but measurable concentration of small nickel-rich magnetic dipoles. For  $\text{Cu}_{0.6}\text{Ni}_{0.4}$  a bimodal distribution of magnetic clusters seems to be appropriate. The



average magnetic moment of ferromagnetic and superparamagnetic Cu-Ni alloys can be described in terms of a local atomic environment model making use of published short range order parameter values.

Analysis of the available magnetic data for Cu-Fe alloys with ~110 ppm Fe indicates the presence of giant moments in addition to single Fe and Fe pair moments. Down to 1.3°K the results exclude any measurable loss of Fe moments as a result of spin compensation or local spin fluctuation, which might be expected in view of published Kondo temperatures.

The ratio of the concentration of the Fe pair moments to that of the single Fe moments suggests clustering of Fe atoms. Each of the copper alloys containing 380 and 478 ppm Fe, and 1% Fe has a maximum in the magnetization and the temperature of the maximum increases with the Fe content. The  $\text{Cu}_{0.99}\text{Fe}_{0.01}$  alloy is shown to be micromagnetic.



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## APPENDIX A

SIGMA-5 COMPUTER PROGRAM FOR FITTING OF EQ. 9  
(OR 11, 13, OR 14) TO MAGNETIZATION DATA

This program makes use of a variational method where the parameters are varied successively till a best fit, characterized by a minimum rmsd is obtained.

Program Steps

Steps 65 through 100, and 195 through 960.

Input Parameters

K is the total number of data points.

K1 is the number by which the mean square deviation should be divided ( $K1 > K$  if some of the data points were weighted preferentially).

K2 is the number of that data point starting from which all the data points (i.e., from K2 to K) are weighted.

K3 is the weighting constant.

K4 is the dividing factor for the data, in case the data points were premultiplied by a constant factor for convenience.

K5 is the number up to which (from 1 to K4) the data points are to be eliminated from the final stages of the fitting.



K6 is the number after which (K6 to K) the data points are to be eliminated from the final stages of the fitting.

K7 and K8 represent the numbers between which (i.e., K7 to K8) the data points are to be eliminated from the final stages of the fitting.

G is the average gram-atomic weight of the alloy.

N1, N2, and N3 are the starting values of the cluster moments  $\mu_1$ ,  $\mu_2$ , and  $\mu_3$  respectively, in Bohr magnetons.

C1, C2, and C3 are the starting values of the cluster concentrations  $c_1$ ,  $c_2$ , and  $c_3$  respectively, in atomic fraction.

S1, S2, and S3 are the starting values of the interaction temperatures  $\theta_1$ ,  $\theta_2$ , and  $\theta_3$  respectively, in °K.

X1 is the temperature and field independent susceptibility  $\chi_0$  (in emu/g).

$$X = \Delta\chi_0 \text{ (emu/g)}$$

$$Z_1 = \Delta\theta_1 \text{ (°K)}$$

$$Z_2 = \Delta\theta_2 \text{ (°K)}$$

$$Z_3 = \Delta\theta_3 \text{ (°K)}$$

$R_1$  is the factor for varying the moment.

$R_2$  is the factor for varying the concentration.

### Input Data

The data are stored in steps 101 through 194. The magnetization M is in emu/g, the field H in Oersteds, and the temperature T in °K (e.g., step 101).



Print Out

rmsd

 $\chi_0$  $c_1$  $\mu_1$  $\theta_1$  $c_2$  $\mu_2$  $\theta_2$  $c_3$  $\mu_3$  $\theta_3$ Additional Operations

(a) To Print out data only,

Step 212 GOTO 900

(b) To Print out data and rmsd and deviations for a given set  
of parameters,

Step 212 GOTO 800

Step 337 PRINT T(I),H(I),M(I),M,D



```

1K1=45
2K2=45
3K3=1
4K4=10
5K5=1
6K6=45
7K7=1
8K8=1
9K=45
10G=42.845
11N1=.3015
12N2=.856884
13N3=4.5108
20Z7=.5
21C1=5.72076E-4
22C2=1.00122E-4
23C3=1.947E-5
31S1=-1.75
32S2=-1.6
33S3=-.2
40X=1E-9
41X1=1.6E-7
51Z1=.01
52Z2=.01
53Z3=.01
61R1=1.002
62R2=1.002
63Z3=.01
65PRINT"-----"
70PRINT
71PRINT"DEFORMED 1000 PPM IRON IN 20%NICKEL-80%COOPER"
72PRINT"-----"
73PRINT"TRIPLE MOMENT FIT"
74PRINT
75PRINT"FOLOWING ARE STARTING PARAMETERS"
80PRINT
81PRINTZ7
82PRINT
84PRINTG,K,K1,K2,K3
85PRINTK4,K5,K6,K7,K8
86PRINT
87PRINTC1,N1,S1
88PRINTC2,N2,S2
89PRINTC3,N3,S3
90PRINTX1,X
91PRINTZ1,Z2,Z3
92PRINTR1,R2
93PRINT
101M(1)=.17829,H(1)=12582,T(1)=1.47
195PRINT"CALCULATION BEGINS"
196FORI=1TOKSTEP1
197M(I)=M(I)/K4

```



```

1000PRINT
1001PRINT
2000F=0
2001A=1,V1=C1,W1=S1
2002B=1,V2=C2,W2=S2,U3=N3,V3=C3,W3=S3
2003H(K(0)),C(0),S(0),X(1)
2004H1=Z1,H2=Z2,H3=Z3
2005L=0
2006PRINT
2007DIMX(100),H(100),T(100)
210X(1)=X1
211A,B,P,Q,A1,B1,P1,Q1=0
215N(1)=N1,C(1)=C1,S(1)=S1
220N(2)=N2,C(2)=C2,S(2)=S2
225N(3)=N3,C(3)=C3,S(3)=S3
230GOSUB700
235L=L+1
236PRINTL,F
237PRINTA1;B1;P1;Q1
254PRINT
255IF F=0 THEN 260
256IFY5<(Y7+Y7*1E-3) THEN 350
260IF L=1 THEN 270
265GOTO 274
270Y6=Y7,U1=N1,V1=C1,W1=S1,H1=Z1
271N1=N2,C1=C2,S1=S2,Z1=Z2
272N2=U1,C2=V1,S2=W1,Z2=H1
273GOTO 210
274IFY6<(Y7+Y7*1E-6) THEN 351
276Y6=Y7,U1=N1,V1=C1,W1=S1
277U2=N2,V2=C2,W2=S2,H1=Z1,H2=Z2
279N1=N2,C1=C2,S1=S2,Z1=Z2
280N2=U1,C2=V1,S2=W1,Z2=H1
285GOTO 210
300Y=0
305FOR I=K5 TO K6 STEP 1
306GOTO 950
310M=X(1)*H(1)
311FOR J=1 TO 3 STEP 1
312IF (T(1)-S(J))=0 THEN 363
316M1=2*6.72E-5*H(1)/(T(1)-S(J))
317IF M1<0 THEN 361
318M2=M1*(N(J)+1)
319IF M2<100 THEN 322
320M2=N(J)+1
321GOTO 323
322M2=(N(J)+1)*(EXP(M2)+1)/(EXP(M2)-1)
323IF M1<170 THEN 326
324M3=1
325GOTO 327
326M3=(EXP(M1)+1)/(EXP(M1)-1)
327E(J)=5581*C(J)*(M2-M3)/G
328M=M+E(J)

```



```

3300=0
3301=-H*(K1)
3400=D+2
3401=F1<=XCCST6345
3402=D-43
343GCT6345
346Y=Y+D
350EXTI
355Y=Y/X1
359Y=SCR(Y)
360GCT6365
361PRINT"T(I)-S(J) NEGATIVE"
362STOP
363PRINT"T(I)-S(J)=0"
364STOP
365RETURN
400C(1)=C1
401GOSUB300
402Y1=Y
403A=0
405C(1)=C1*R2
410A=A+1
411IFA=20THEN430
412IFA>A1THEN414
413GCT6415
414A1=A
415GOSUB300
420IFY1<(Y+Y*1E-3)THEN435
425Y1=Y,C1=C(1)
430GCT6405
435IFA=1THEN450
440GCT6475
450C(1)=C1/R2
451A=A+1
452IFA=20THEN480
453IFA<A1THEN455
454A1=A
455GOSUB300
460IFY1<(Y+Y*1E-3)THEN475
465Y1=Y,C1=C(1)
470GCT6450
475RETURN
480PRINTA,B,P,Q
486PRINT"INCREASE R2"
487GCT6550
500GOSUB400
505Y9=Y1,C9=C1
510B=0
515N(1)=N1*R1
520B=B+1
521IFB=40THEN590
522IFB>B1THEN524
523GCT6525

```



```

53500000
53500000
53500000<(Y1+Y1*1E-3) THEN 545
53500000=Y1, C9=C1, N1=N(1)
54000000
54500000=1 THEN 554
55000000
55400000=C9
55500000=N1/R1
55600000=E+1
55700000=40 THEN 590
55800000=B1 THEN 560
55900000=E
56000000
56500000<(Y1+Y1*1E-3) THEN 580
57000000=Y1, C9=C1, N1=N(1)
57500000
58000000=N1, C1=C9
58500000 RETURN
59000000 PRINT A; B; P; Q
59500000 PRINT "INCREASE R1"
59700000
60000000
60500000=Y9, C8=C9, N8=N1
61000000
61500000=S1+Z1
62000000=P+1
62100000=10 THEN 690
62200000>P1 THEN 624
62300000
62400000=P
62500000
63000000<(Y9+Y9*1E-3) THEN 645
63500000=Y9, C8=C9, N8=N1, S1=S(1)
64000000
64500000=1 THEN 654
65000000
65400000=C8, N(1)=N8
65500000=S1-Z1
65600000=P+1
65700000=10 THEN 690
65800000<P1 THEN 660
65900000=P
66000000
66500000<(Y9+Y9*1E-3) THEN 680
67000000=Y9, C8=C9, N8=N1, S1=S(1)
67500000
68000000=S1, C1=C8, N(1)=N8, N1=N8
68500000 RETURN
69000000 PRINT A; B; P; Q
69500000 PRINT "INCREASE Z1"
69600000
70000000

```



```

705Y7=Y8,C7=C8,N7=N8,S7=S1
710C=C
715X(1)=X1+X
716PRINT"X1CHANGED",Y7,X1
717PRINTC7,N7,S7
718PRINTC2,N2,S2
719PRINTC3,N3,S3
720C=C+1
721IFC=10THEN790
722IFC>Q1THEN724
723GOTO725
724Q1=Q
725GOSUB600
730IFY7<(Y8+Y8*1E-3)THEN745
735Y7=Y8,C7=C8,N7=N8,S7=S1,X1=X(1)
740GOTO715
745IFQ=1THEN754
750GOTO730
754Q1=C7,N(1)=N7,S(1)=S7
755X(1)=X1-X
756PRINT"X1CHANGEDDOWN",Y7,X1
757PRINTC7,N7,S7
758PRINTC2,N2,S2
759PRINTC3,N3,S3
760Q=Q+1
761IFQ=10THEN790
762IFQ<Q1THEN764
763Q1=Q
764GOSUB600
765IFY7<(Y8+Y8*1E-3)THEN780
770Y7=Y8,C7=C8,N7=N8,S7=S1,X1=X(1)
775GOTO755
780C1=C7,N(1)=N7,S(1)=S7,N1=N7,X(1)=X1,S1=S7
785RETURN
790PRINTA;B;P;Q
791PRINT"INCREASE X1"
792GOTO850
800N(1)=U1,C(1)=V1,S(1)=W1
805N(2)=U2,C(2)=V2,S(2)=W2
806N(3)=U3,C(3)=V3,S(3)=W3
810GOSUB300
815PRINT
820PRINTY
821PRINTX1
822PRINTC1,N1,S1
823PRINTC2,N2,S2
824PRINTC3,N3,S3
825STOP
830END
850STOP
851IFF=0THEN860
855IFY5<(Y6+Y6*1E-3)THEN885
860Y5=Y6

```



```
333W3=X1, C3=C1, S3=S1, Z3=Z1
370X1=U3, C1=V3, S1=W3, Z1=X3
373Y=Y+1
380GOTO 4201
383STOP
900FTRI=170KSTEP1
905PRINTI, X(1), T(1), M(1)
910NEXTI
915STOP
950IFI<=K7THEN310
955IFI>=K8THEN310
960GOTO 350
>
```



## APPENDIX B

SIGMA-5 COMPUTER PROGRAM FOR THE  
DETERMINATION OF  $iS_k$ 

$iS_k$  is the number of sites in an f.c.c. structure which are common to the  $k^{\text{th}}$  shell of an atom B, that is in the  $i^{\text{th}}$  shell of an atom A, and the shells 1 through 9 of the atom A.

The program is divided into two main parts: the K Program (steps 95 to 600) and the J Program (steps 649 to 1315). In the J program all the lattice points in the K shell of atom B are generated successively; as each point is generated, the K Program is used to generate all the lattice points in shells 1 through 9 of atom A and a comparison is made to determine if there is an overlap.

The position of the atom B with respect to atom A is represented by a translation vector  $I$ . The lattice sites in the  $k$  shell of atom B are generated by first generating the lattice sites in the  $k$ -shell of A and then applying to each of these sites a lattice translation with the vector  $I$ .

The lattice sites in a given shell of atom A are generated by finding out all the crystallographically equivalent sites, in space, of a single site (whose spatial coordinates are known) in that shell.



InputStep 690       $U(=i)$ Step 700       $G(=k)$ Print Out

| I | i | k | $iS_k$ |
|---|---|---|--------|
|---|---|---|--------|



```
1PRINT
2PRINT
3PRINT
81I(1),J(1),K(1)=515150
82I(2),J(2),K(2)=525050
83I(3),J(3),K(3)=525151
84I(4),J(4),K(4)=525250
85I(5),J(5),K(5)=535150
86I(6),J(6),K(6)=525252
87I(7),J(7),K(7)=535251
88I(8),J(8),K(8)=545050
89I(9),J(9),K(9)=535350
90I(10),J(10),K(10)=545151
94GOTO649
95PRINT"KPROGRAM"
100REMKPROGRAM
160FORL=1TO10STEP1
170K=K(L)
180W=0
181DIMN(4,6)
185MATN=ZER(4,6)
190GOSUB200
191GOTO300
200P=1
205Q=1
206GOSUB2500
210IFK1=N(P,Q)THEN285
215IFN(P,Q)=0THEN250
220P=P+1
225IFP<5THEN210
230P=P-4,Q=Q+1
235IFQ<7THEN210
240GOTO270
250N(P,Q)=K1
270IFK1=JTHEN280
275GOTO285
280N=N+1
285RETURN
300K=K-500000
310GOSUB200
320K=K-5000
330GOSUB200
340K=K-50
350GOSUB200
360K=K+5000
370GOSUB200
380K=K+500000
390GOSUB200
400K=K-5000
410GOSUB200
420K=K+50
430GOSUB200
440K=K+5000
```



```
445G0SUB450
446G0T0480
450E1=K/100
455F1=INT(E1)
460G1=E1-F1
465H1=INT(G1*10*6+.1)
470K=H1+F1
475RETURN
480W=W+1
490IFW/3-INT(W/3)=0THEN510
500G0T0190
510G0SUB520
511G0T0570
520A2=K/100
525B2=INT(A2)
530C2=A2-B2
535C2=C2*100
540B2=B2/100
545D2=INT(B2)
550B2=B2-D2
560K=INT(B2*10*6+D2*100+C2+.1)
565RETURN
570IFW=>6THEN580
575G0T0190
580REMM1CALCULATION
590NEXTL
600RETURN
649N=0
650V1=0
690U=10
700F0RG=1T010STEP1
710DIMM(4,6)
720MATM=ZER(4,6)
730T=0
735Y=J(G)
736G0SUB2000
740G0SUB750
741G0T0830
750R=1
755S=1
756Y5=INT(Y5+.1)
760IFY5=M(R,S)THEN805
765IFM(R,S)=0THEN795
770R=R+1
775IFR<5THEN760
780R=R-4,S=(S+1)
785IFS<7THEN760
790G0T0800
795M(R,S)=Y5
800G0T0810
805Y1=Y5
810RETURN
830IFY1=Y5THEN1005
```



```
835G0SUB840
836G0T01000
840U1=I(U)
841Y7=Y5
842G0SUB845
843G0T0900
845Y2=Y7/100
850Y3,Y7=INT(Y2)
855Y4=Y2-Y3
860IFY4>=.5THEN892
865U2=U1/100
870U3,U1=INT(U2+.1)
875U4=U2-U3
880U5=U4-.5
885IFU5-Y4>0THEN894
890U6=ABS(U5-Y4)
891G0T0895
892G0SUB910
893G0T0895
894G0SUB945
895RETURN
900G0T0960
901PRINT"WE ARE ADDING I VECTOR"
910Y5=Y4-.5
915U2=U1/100
920U3,U1=INT(U2+.1)
925U4=U2-U3
930U6=Y5+U4
940RETURN
945U6=.5+U5-Y4
950RETURN
960U7=(U6)*100
965G0SUB845
970U7=U7+(U6)*10+4
975G0SUB845
980J=INT(U7+U6*10+6+.1)
981G0SUB1500
990RETURN
1000G0SUB 100
1005Y=Y-500000
1007G0SUB2000
1010G0SUB750
1015IFY1=Y5THEN1030
1020G0SUB840
1025G0SUB100
1030Y=Y-5000
1032G0SUB2000
1035G0SUB750
1040IFY1=Y5THEN1055
1045G0SUB840
1050G0SUB100
1055Y=Y-50
1057G0SUB2000
```



```
1060G0SUB3750
1065IF Y1=Y5THEN1080
1070G0SUB840
1075G0SUB100
1080Y=Y+5000
1082G0SUB2000
1085G0SUB750
1090IF Y1=Y5THEN1105
1095G0SUB840
1100G0SUB100
1105Y=Y+500000
1106G0SUB2000
1110G0SUB750
1115IF Y1=Y5THEN1130
1120G0SUB840
1125G0SUB100
1130Y=Y-5000
1131G0SUB2000
1135G0SUB750
1140IF Y1=Y5THEN1155
1145G0SUB840
1150G0SUB100
1155Y=Y+50
1156G0SUB2000
1160G0SUB750
1165IF Y1=Y5THEN1180
1170G0SUB840
1175G0SUB100
1180Y=Y+5000
1185G0SUB1190
1186G0T01220
1190E5=Y/100
1195F5=INT(E5)
1200G5=E5-F5
1202G5=G5*100
1204G5=INT(G5+.2)
1206H5=G5*10+4
1210Y=H5+F5
1215RETURN
1220T=T+1
1225IFT/3-INT(T/3)=0THEN1235
1230G0T0736
1235G0SUB1240
1236G0T01285
1240A7=Y/100
1245B7=INT(A7)
1250C7=A7-B7
1255D7=(C7)*100
1260E7=(B7)/100
1265F7=INT(E7)
1270G7=E7-F7
1275Y=G7*10+6+(F7)*100+D7
1280RETURN
```



```
1285 IF T >= 6 THEN 1295
1290 GOTO 736
1295 M1 = N - V1
1296 PRINT I(U), U, G, M1
1297 V1 = N
1299 PRINT
1300 NEXT G
1304 PRINT
1305 PRINT "TOTAL N FOR ALL J", I(U), U, N
1315 END
1500 J = INT(J + .1)
1501 A9 = J / 100
1505 B9 = INT(A9)
1510 C9 = A9 - B9
1515 D9 = C9 * 100
1520 IF D9 = 0 THEN 1560
1525 E9 = B9 / 100
1530 F9 = INT(E9 + .1)
1535 G9 = E9 - F9
1540 H9 = G9 * 100
1545 IF F9 = 0 THEN 1570
1550 IF H9 = 0 THEN 1580
1555 GOTO 1585
1560 D9 = D9 + 50
1565 GOTO 1525
1570 F9 = F9 + 50
1575 GOTO 1550
1580 H9 = H9 + 50
1585 J = INT(F9 * 10000 + H9 * 100 + D9 + .1)
1590 RETURN
2000 Y = INT(Y + .1)
2001 A9 = Y / 100
2005 B9 = INT(A9)
2010 C9 = A9 - B9
2015 D9 = C9 * 100
2020 IF D9 = 0 THEN 2060
2025 E9 = B9 / 100
2030 F9 = INT(E9)
2035 G9 = E9 - F9
2040 H9 = INT(G9 * 100 + .1)
2045 IF F9 = 0 THEN 2070
2050 IF H9 = 0 THEN 2080
2055 GOTO 2085
2060 D9 = D9 + 50
2065 GOTO 2025
2070 F9 = F9 + 50
2075 GOTO 2050
2080 H9 = H9 + 50
2085 Y5 = F9 * 10000 + H9 * 100 + D9
2090 RETURN
2500 K = INT(K + .1)
2501 A9 = K / 100
2505 B9 = INT(A9)
```



```
2510C9=A9-B9
2515D9=C9*100
2520IFD9=0THEN2560
2525E9=B9/100
2530F9=INT(E9)
2535G9=E9-F9
2540H9=INT(G9*100+.1)
2545IFF9=0THEN2570
2550IFH9=0THEN2580
2555GOTO2585
2560D9=D9+50
2565GOTO2525
2570F9=F9+50
2575GOTO2550
2580H9=H9+50
2585K1=INT(F9*10000+H9*100+D9+.1)
2590RETURN
```

&gt;



## APPENDIX C

SIGMA-5 COMPUTER PROGRAM FOR CALCULATING THE RATIO  
 $c_2/c_1$  ON THE BASIS OF THE RANDOM ALLOY  
MODEL,<sup>4</sup> FROM EQ. 30

Input

- Step 1      $x$  (= Ni concentration in at. fraction)  
Step 2      $z$  (= Fe concentration in at. fraction)

Print Out

|                    |                     |
|--------------------|---------------------|
| $x$                | $z$                 |
| $c_1$              | $c_2$               |
| $c_2/c_1$          | % Fe atoms in pairs |
| $(z - c_1 - 2c_2)$ |                     |



```
IX=.2
ZE=1000E-6
SPRINT
6PRINT
10DIMS(S,8)
11S(1,1)=11
12S(1,2)=6
13S(1,3)=24
14S(1,4)=12
15S(1,5)=22
16S(1,6)=6
17S(1,7)=32
18S(1,8)=5
21S(2,1)=12
22S(2,2)=5
23S(2,3)=24
24S(2,4)=8
25S(2,5)=20
26S(2,6)=4
27S(2,7)=24
28S(2,8)=4
31S(3,1)=12
32S(3,2)=6
33S(3,3)=18
34S(3,4)=9
35S(3,5)=14
36S(3,6)=5
37S(3,7)=22
38S(3,8)=5
41S(4,1)=12
42S(4,2)=4
43S(4,3)=18
44S(4,4)=6
45S(4,5)=12
46S(4,6)=2
47S(4,7)=24
48S(4,8)=5
51S(5,1)=11
52S(5,2)=5
53S(5,3)=14
54S(5,4)=6
55S(5,5)=10
56S(5,6)=4
57S(5,7)=20
58S(5,8)=4
61S(6,1)=9
62S(6,2)=3
63S(6,3)=15
64S(6,4)=3
65S(6,5)=12
66S(6,6)=3
67S(6,7)=18
```



```

68S(6,8)=3
71S(7,1)=8
72S(7,2)=3
73S(7,3)=11
74S(7,4)=6
75S(7,5)=10
76S(7,6)=3
77S(7,7)=15
78S(7,8)=3
81S(8,1)=5
82S(8,2)=2
83S(8,3)=10
84S(8,4)=5
85S(8,5)=8
86S(8,6)=2
87S(8,7)=12
88S(8,8)=4
100DIMR(8)
101R(1)=12
102R(2)=6
103R(3)=24
104R(4)=12
105R(5)=24
106R(6)=8
107R(7)=48
108R(8)=12
110A=1-X
111B=1-X*X
112C=1-A*A
113D=1-X*C
114E=1-X*(1-A*A*A)
115F=1-X*(1-A*A*A*A)
121P(1)=1
122P(2)=1-A^4
123P(3)=1-(A*A*D*D)
124P(4)=1-A*B^4
125P(5)=6*X^8-24*X^7+35*X^6-24*X^5+15*X^4-16*X^3+9*X^2
126P(6)=-2*X^6+6*X^5-3*X^4-6*X^3+6*X^2
127P(7)=3*X^2-2*X^3
128P(8)=X*X
300Y1=Z
305F0RJ=1T08STEP1
310Y2=(1-Z*P(J))^R(J)
315Y1=Y1*Y2
320NEXTJ
325C1=Y1
330Y3=.5*Z*C1
400Y6=0
405F0RI=1T08STEP1
410Y4=(P(I)*R(I))/((1-Z*P(I))^2)
415F0RK=1T08STEP1
420Y5=(1-Z*P(K))^R(K)-S(I,K)
425Y4=Y4*Y5

```



```
430NEXTK
435Y6=Y4+Y6
440NEXTI
445C2=Y3*Y6
450PRINTX,Z
455PRINTC1,C2
456PRINTC2/C1,(100*2*C2)/Z
457PRINT(Z-C1-2*C2)
460PRINT
465STOP
470ENDPROGRAM
```



## VITA

Sanak Mishra was born on December 18, 1945 in Berhampur, India to Harihar and Indumati Misra. He graduated from the Queen of the Missions High School, Berhampur in 1961. On the basis of his performance he was awarded a gold medal by the State Board of Education, and also a Government of India National Merit Scholarship which he held until August, 1968. He entered the Utkal University in 1961 and received the Bachelor of Science Honours degree in Physics in 1965. The same year he joined the Indian Institute of Science, Bangalore, and in 1965 obtained the Bachelor of Engineering degree in Metallurgy. In September, 1968 he began graduate work at the Department of Metallurgy, University of Illinois and received his M.S. degree in August, 1970. The title of his master's thesis was: Paramagnetism in Copper-Rich Copper Nickel Solid Solutions, Effect of Small Iron Additions. In September, 1970 he began studies toward a Ph.D. degree. He is the author of two publications.